

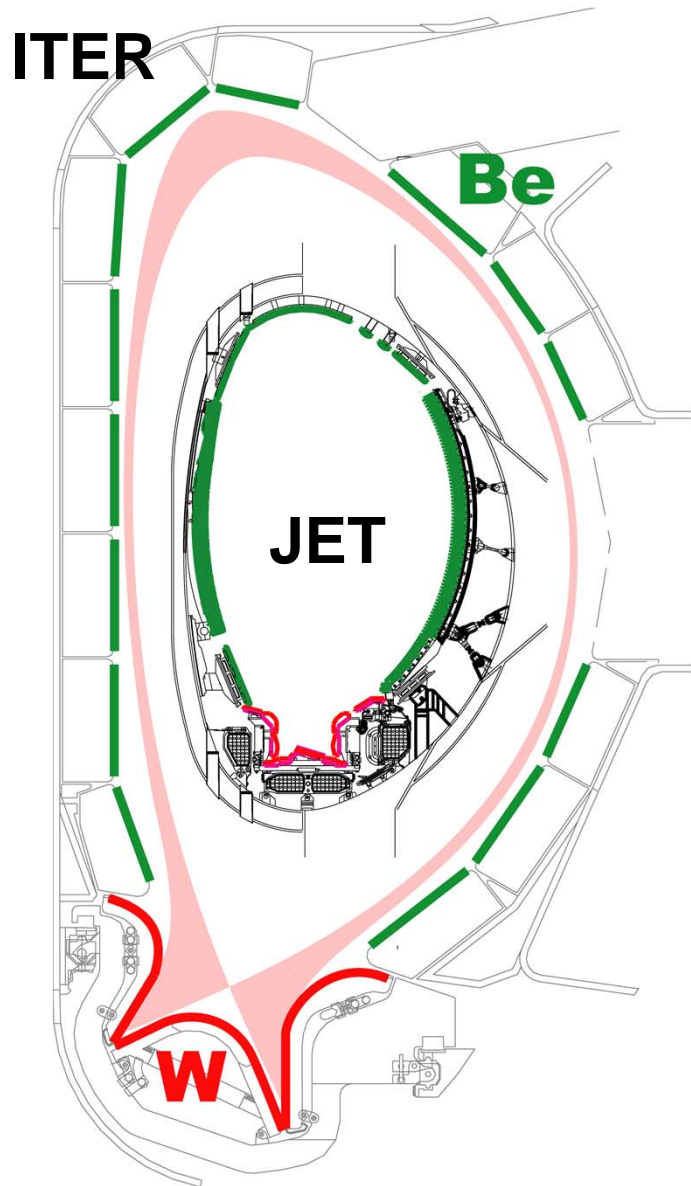


**PSI Investigations
in the JET full W divertor
(ITER-Like Wall)**

S. Brezinsek

for TFE, E1, E2, S1 and JET EFDA contributors

- **ITER-Like Wall at JET**
- Operational space of ILW components
- Strategy of preparatory work
 - Development of compatibility tools to control heat loads and transients
 - Reference plasmas for direct comparison of graphite and metallic wall
- Plans for ILW exploitation



Be wall and W divertor in JET

- Material combination for the first time used
 - Replacement of the wall in one shutdown
-
- “Carbon-free” environment
 - Reduced material migration to rem. areas
 - Reduced tritium retention
 - Loss of carbon as main radiator
-
- Change in operational space
 - Need for better plasma control
 - Need for heat load mitigation schemes

NBI upgrade in JET

- Parallel upgrade of neutral beam system
 - Maximum power from 20 to 34 MW
 - Maximum duration from 10 to 20 s

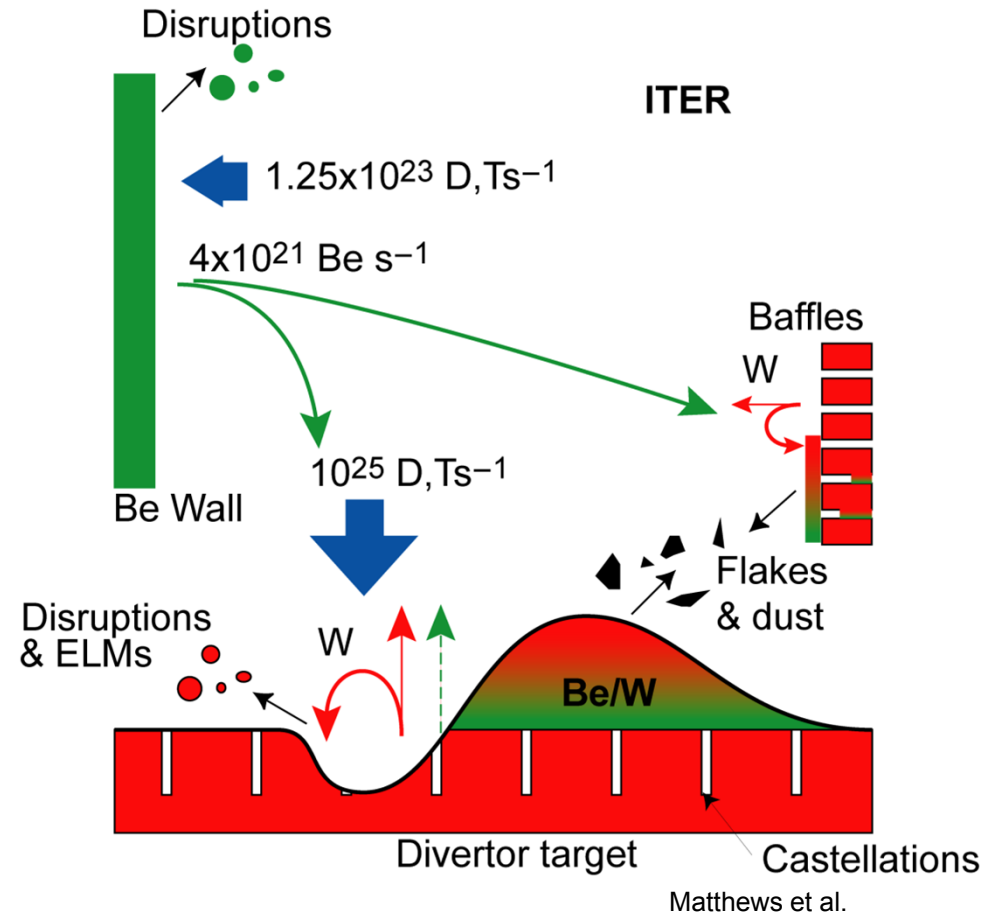
Important PWI questions for ITER will be addressed in JET with the ILW

Steady-state operation

- Be wall erosion and transport
- W erosion and prompt deposition
- Be-W material mixing
- Be:D layer formation
- Fuel retention
- Re-erosion of (mixed) layers
- Material Transport to remote areas

Transients

- Be/W Melt layer motion, loss and stability
- Metallic dust formation



Role of remaining impurities: residual C and O

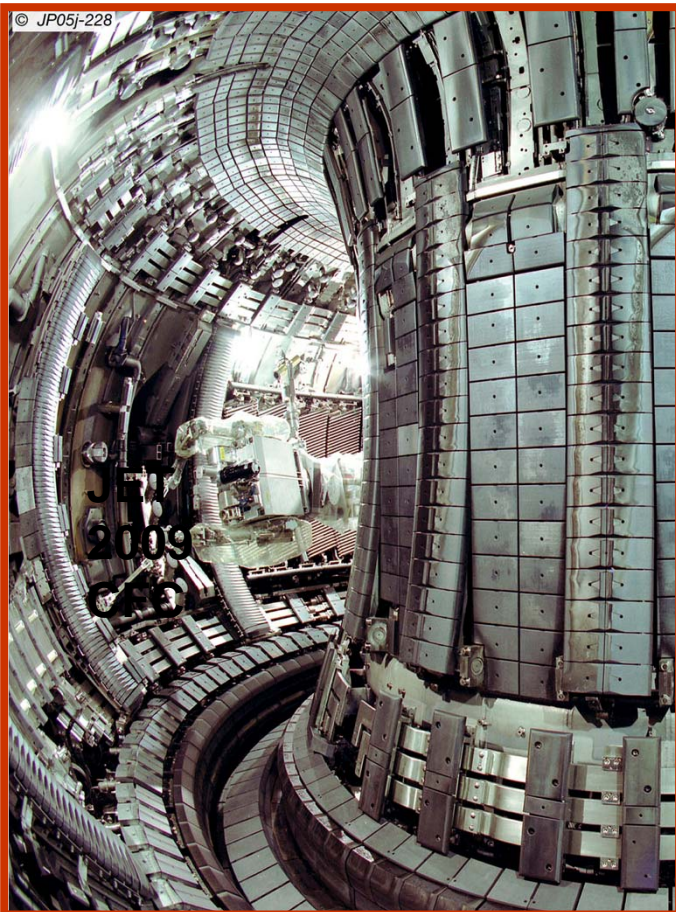
Strong link between plasma wall interaction and scenario compatibility

- Adaption of magnetic shape – use of bulk W divertor
- Neutral beam shine-through – high density operation needed
- W impurity production – low plasma temperature in divertor necessary
- W sputtering by ELMs – ELM control to reduce sputtering (and flushing)
- W accumulation in core region – need for central heating (ICRH)

=> High recycling or semi-detached divertor operation favourable/needed
=> Impact on confinement and plasma energy content

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JET (2009)
CFC and
Be layer
(evapor.)



ILW main chamber

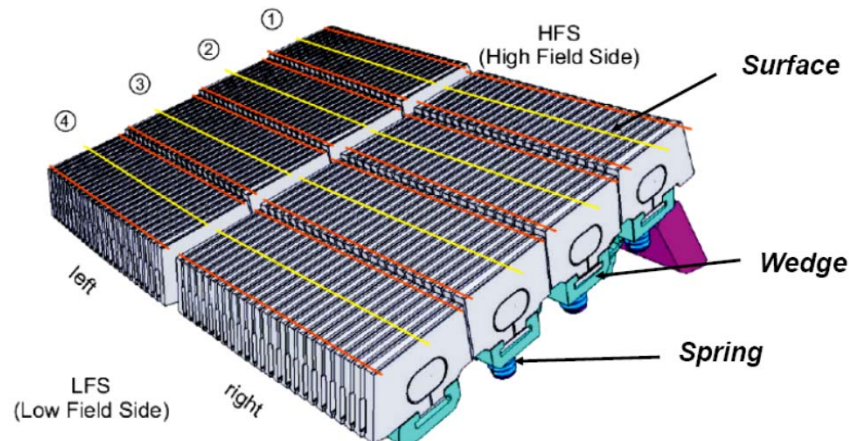
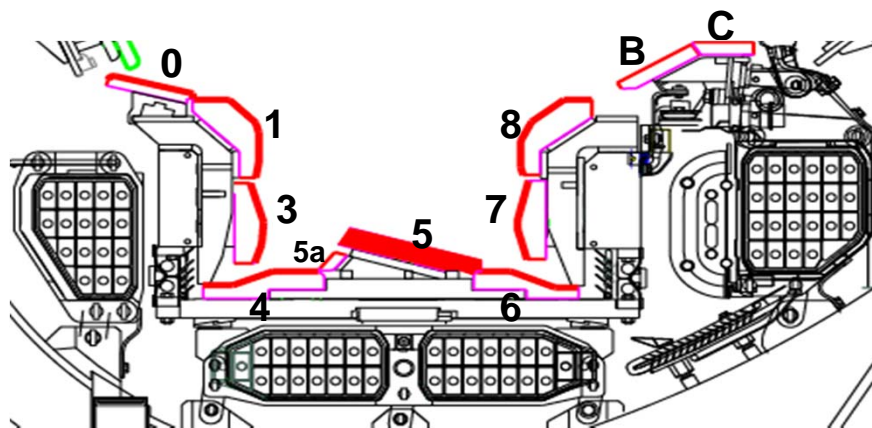
JET (2011)
Be first wall
W divertor



ILW divertor

- Massive Be tiles on main chamber limiters
- Be-coating on Inconel recessed areas
- W-coating on CFC in NBI shine-through area

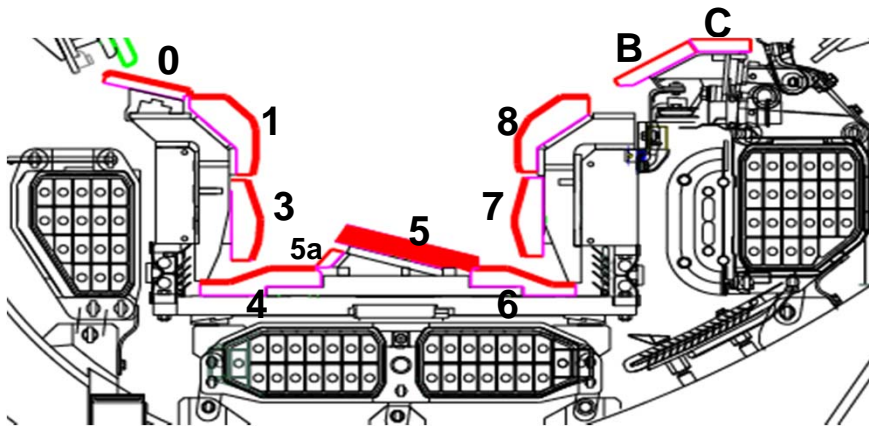
- W-coated CFC tiles in the divertor
- Bulk W tile with lamella structure used as outer divertor target plate



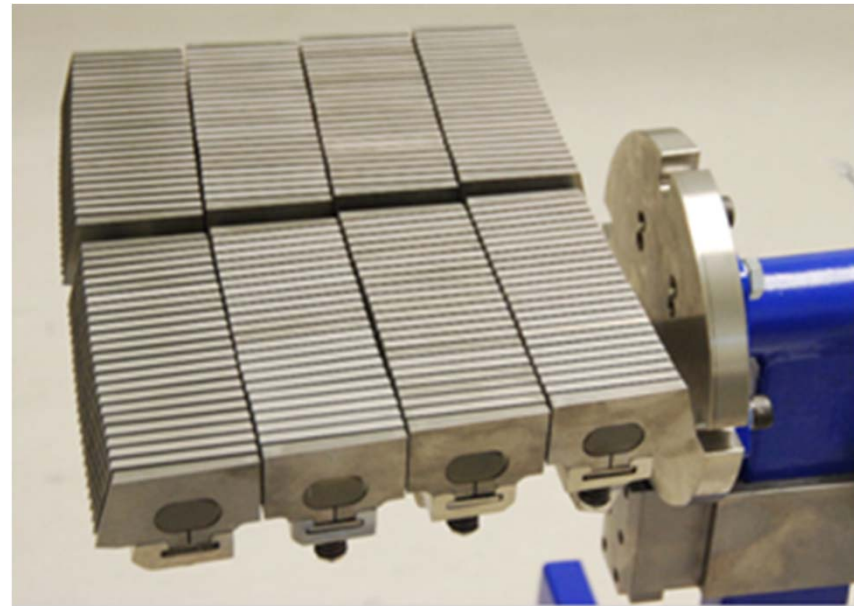
CPM Ph. Mertens

Bulk W tile (tile 5) – design and realisation by FZJ

- “Shape” pre-defined from CFC divertor tile 5. No active cooling!
- Bulk W tile for outer divertor segmented in 4 stacks with 24 lamellae each
- Energy limit per stack of ~60MJ determined by substructure
 - limit depends on wetted fraction area => configuration dependent!
- Power limit of the surface temperature => W recrystallisation
phase 1: 1200°C and final phase: 2200°C
- Cool-down time important => Reduction of plasma repetition rate
- Complex operational instructions to avoid melting of substructure



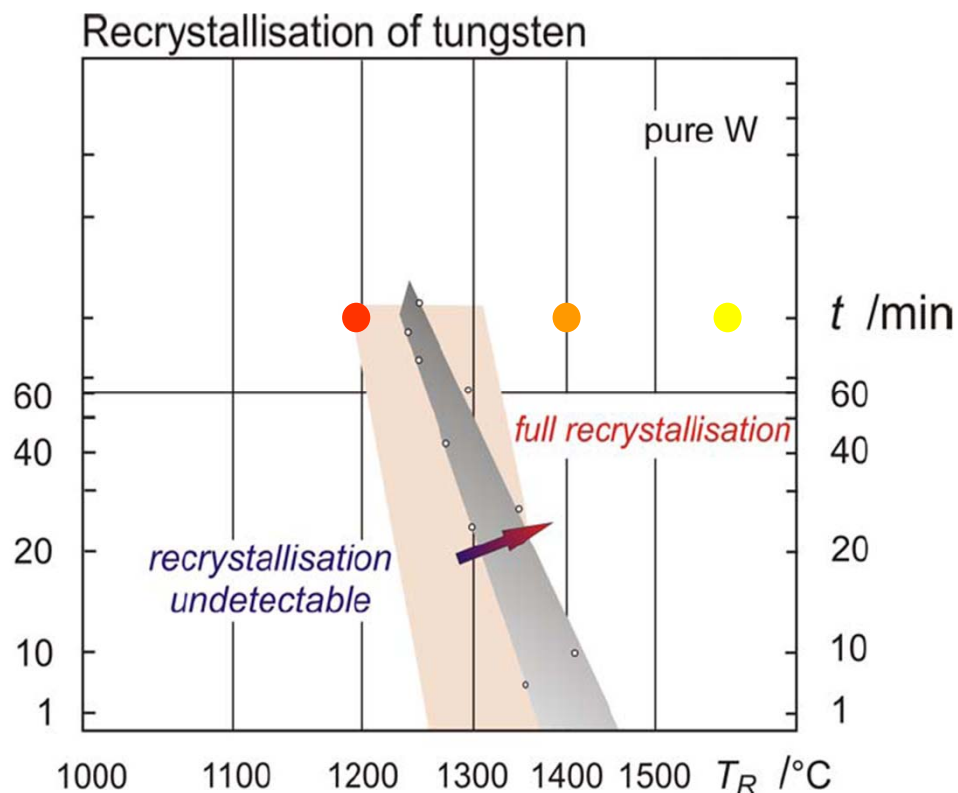
CPM Ph. Mertens



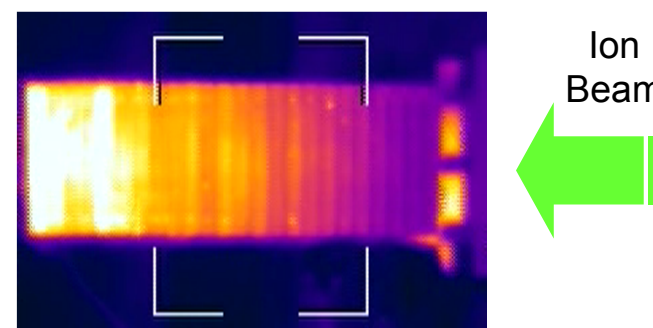
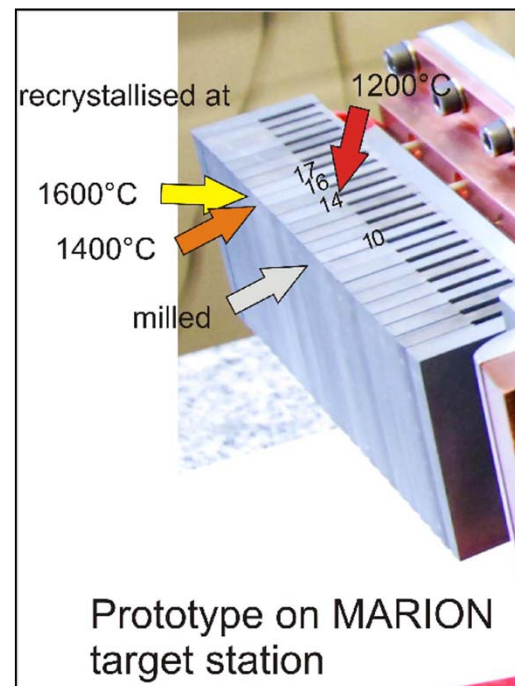
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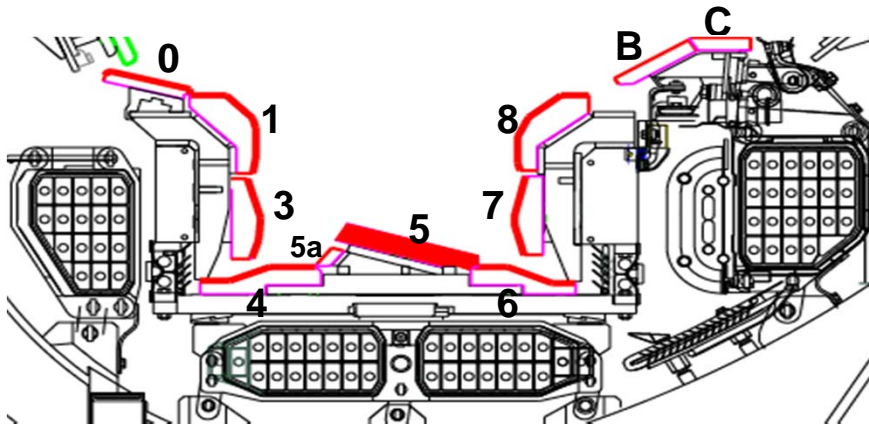
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MARION - Testing at 60MJ for steady-state operation in ion beam facility



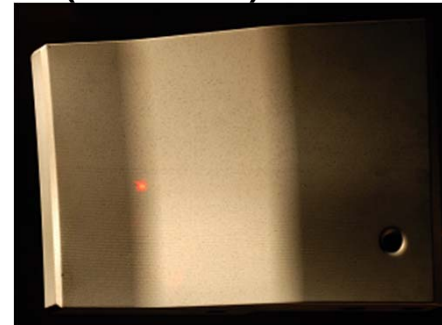
Recrystallisation is not expected to be a limitation!





CPM H. Maier

Tile 4 in GLADIS
(ion beam)



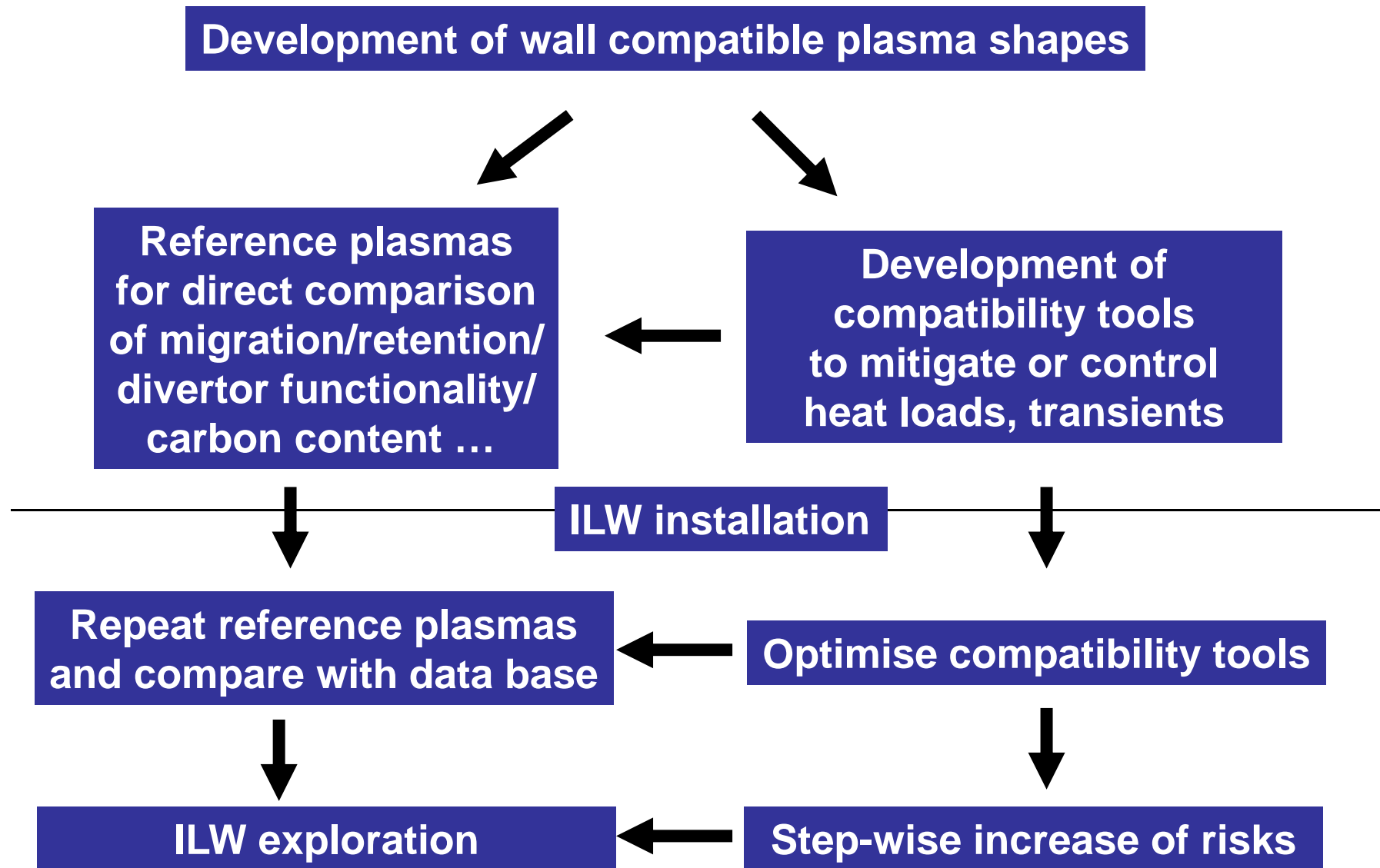
No damage in cycling
up to 1600°C



W-coated CFC tiles – test and qualification IPP

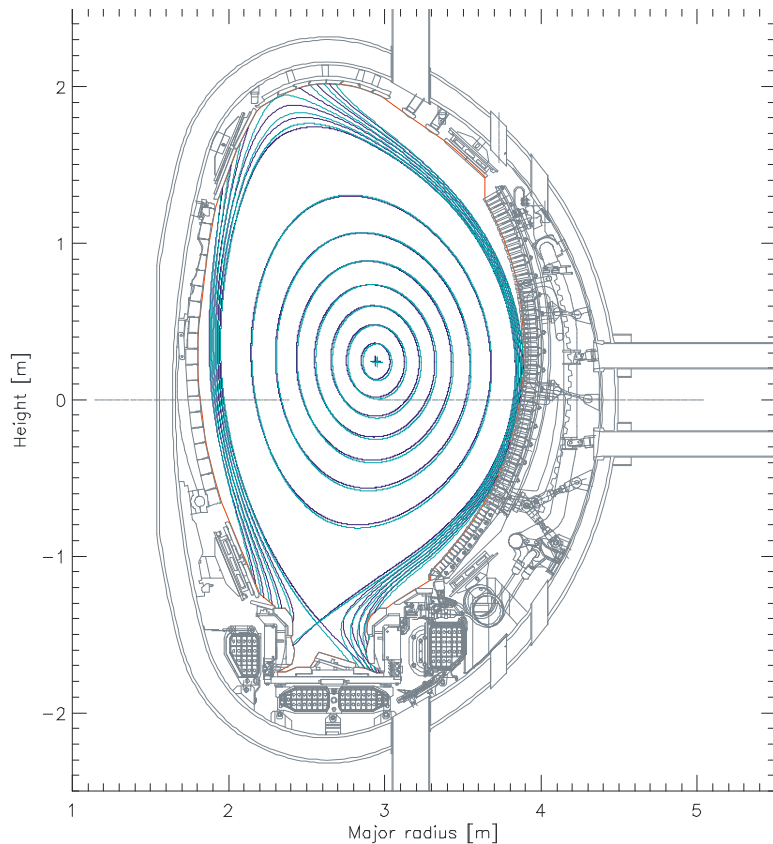
- W coating on standard 2D Dunlop CFC at JET (project requirement)
- No active cooling!
- Expected lifetime of 25µm W-coating for tile 6&7 ~100000s
extrapolation from test coatings of 3 µm thickness in previous campaigns
- (Additional) limitations by carbidisation and inhomogeneous erosion
- Energy limit of W-coated CFC tiles is 90 MJ/m²
- Power limit of W-coated tiles - phase 1: 1200°C, phase 2: 1600°C
- Limitations with respect to multiple ELM energy load: ~125kJ/m² (?)
but depends on starting value (preliminary)

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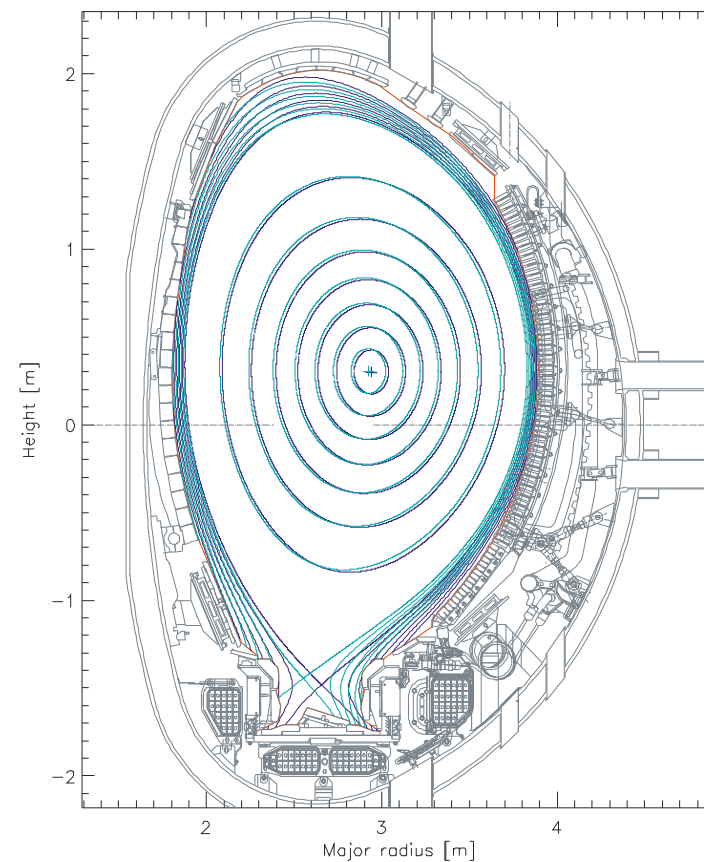


- Shift of the outer-strike point from tile 6 to tile 5 (bulk W with ILW)
- Change in pumping capability / proximity inner strike point and tile 1

high triangularity ($\delta=0.42$)



low triangularity ($\delta=0.27$)



Baseline scenario: P. Lomas, I. Nunes et al.

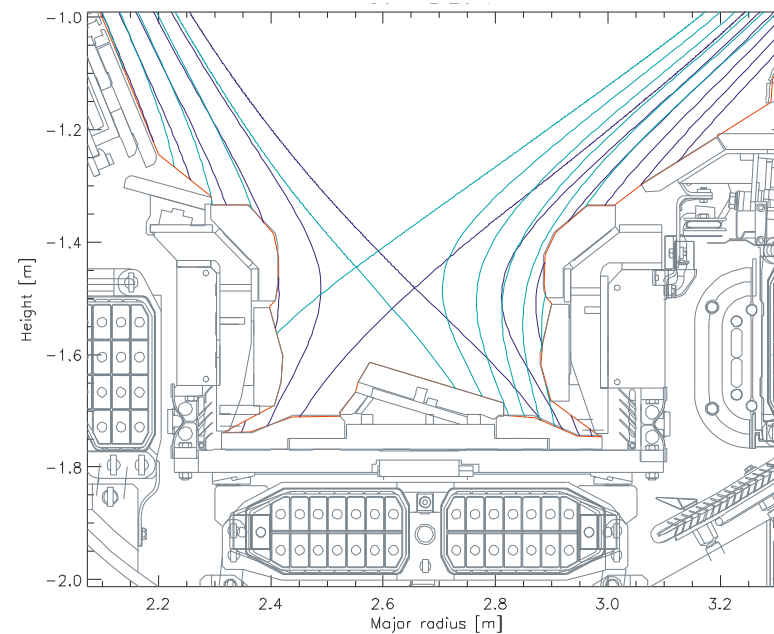
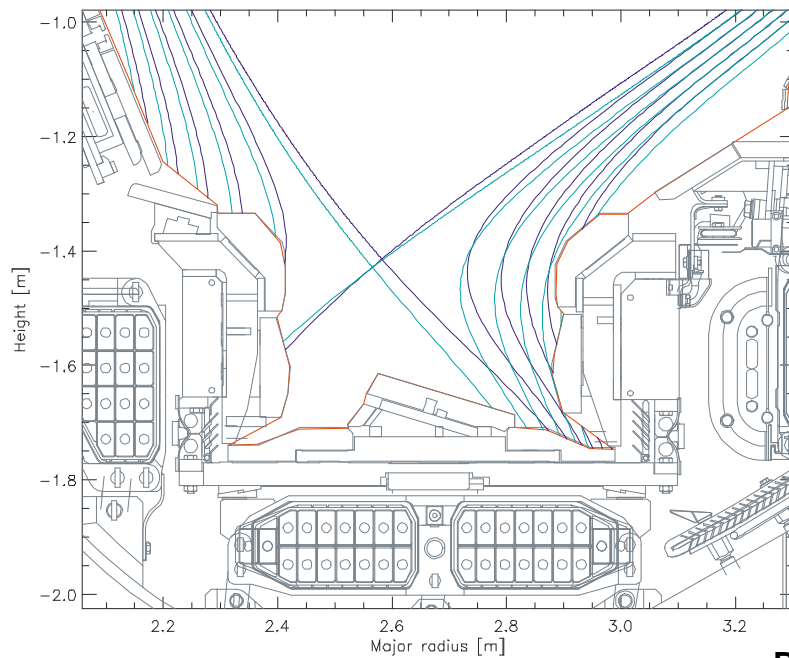
- Majority of preparatory experiments and reference plasmas in similar shapes

Plasma shape

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high triangularity ($\delta=0.42$)

low triangularity ($\delta=0.27$)

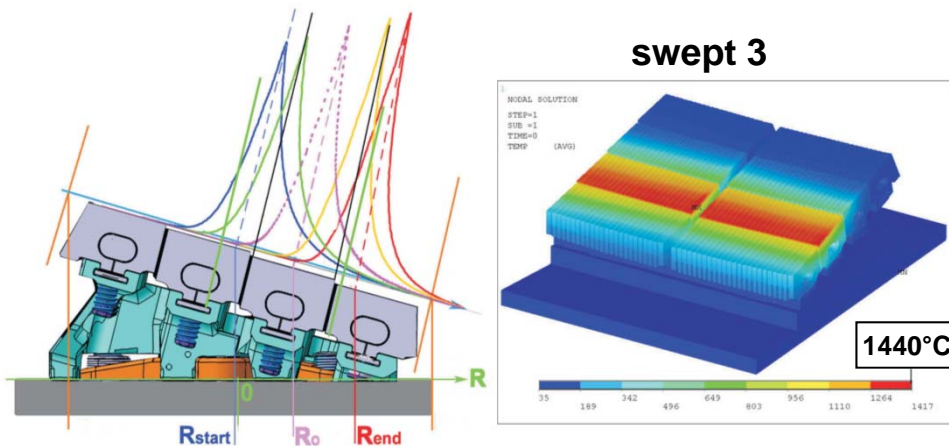


Baseline scenario: P. Lomas, I. Nunes et al.

- Majority of preparatory experiments and reference plasmas in similar shapes

- Development of tools to control heat loads, transients and erosion
 - Techniques to reduce Inter-ELM heat load
 - Techniques to reduce ELM heat load
 - Techniques to reduce W erosion
 - Techniques to mitigate disruptions
- All techniques developed in the first step independent from each other, but combinations have been applied in the later phase of preparation.

- Thermal modelling of energy load

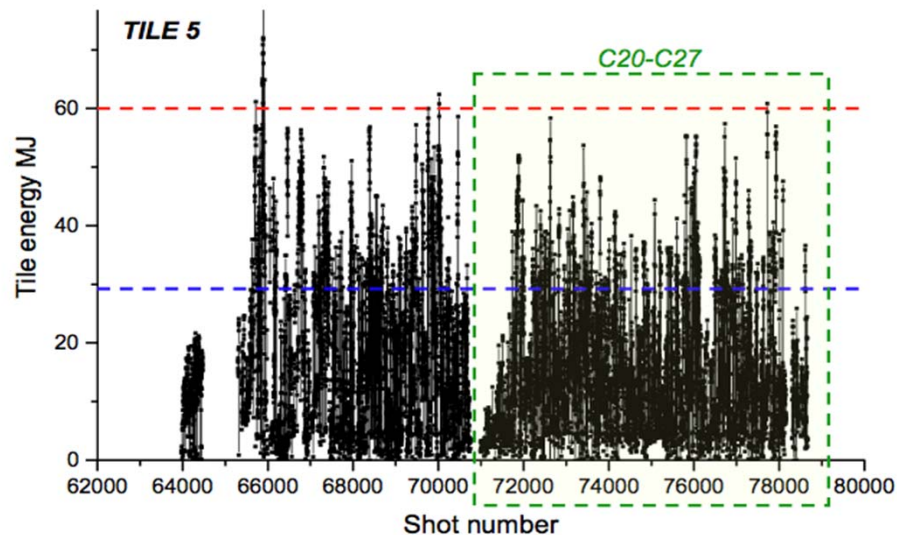


Scenario	Maximal Energy (MJ) deposited over						Temperature (W) <i>T_{surf} max.</i> <i>(approx., 1st pulse)</i>
	stack 1 (HFS)	stack 2	stack 3	stack 4 (LFS)	tile 6	total	
uniform 3	0.0	0.0	60.0	0.0	0.0	60.0	1330°C
static 3	0.0	0.3	60.0	14.4	0.2	74.9	1890°C
swept 3	0.0	9.3	60.0	32.3	1.9	103.5	1440°C
swept 2+3+4	0.4	30.0	60.0	53.8	5.8	150.0	1400°C

Ph. Mertens PSI

- Modelling inline with ion beam tests on real W stacks for ILW

- Tile 5 energy load in 2006-2009

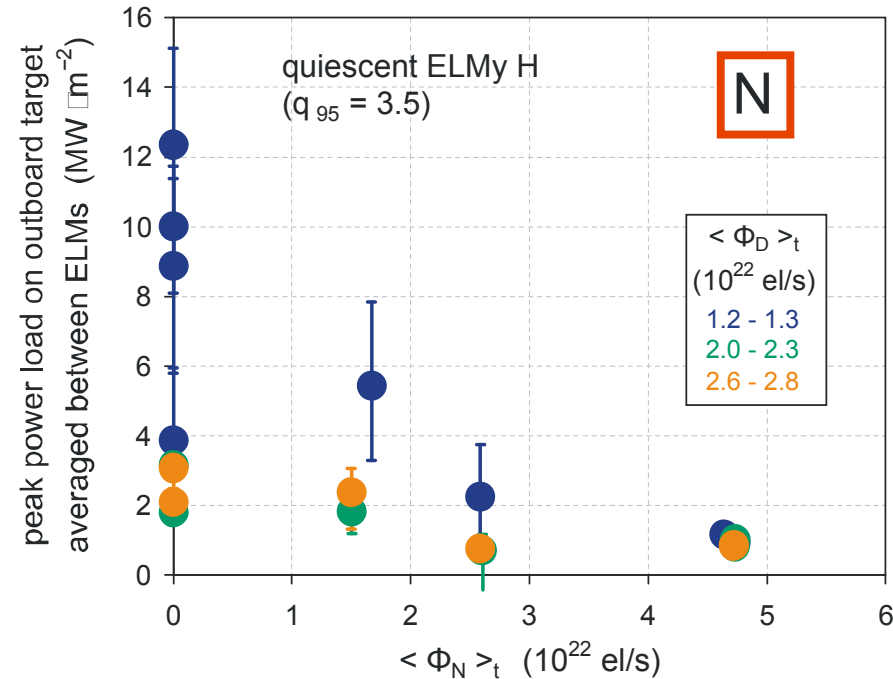
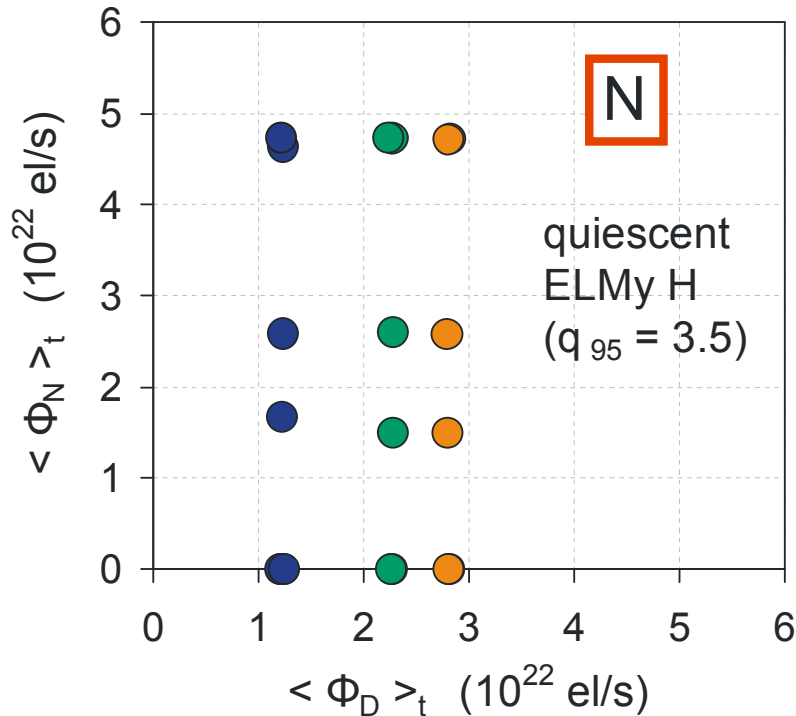


Energy (MJ)	# pulses (%)
0-30	3797 (64%)
30-60	1997 (33%)
>60	169 (3%)
Total	5963

↓ need for sweeping

- Sweeping required for highest input powers

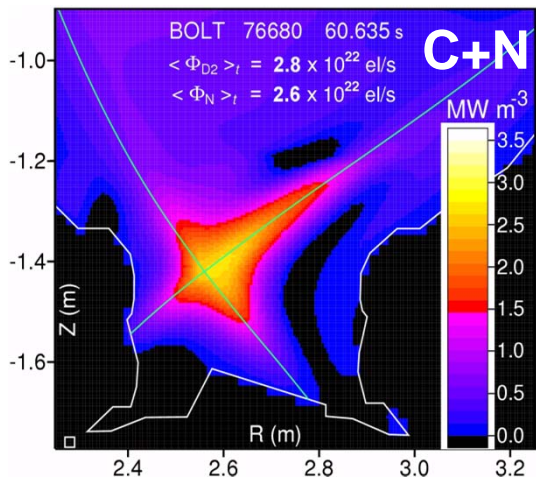
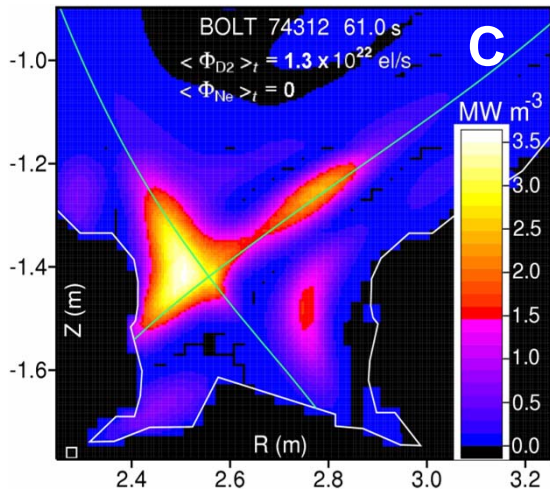
- Impurity seeding for radiation cooling and steady-state heat load mitigation



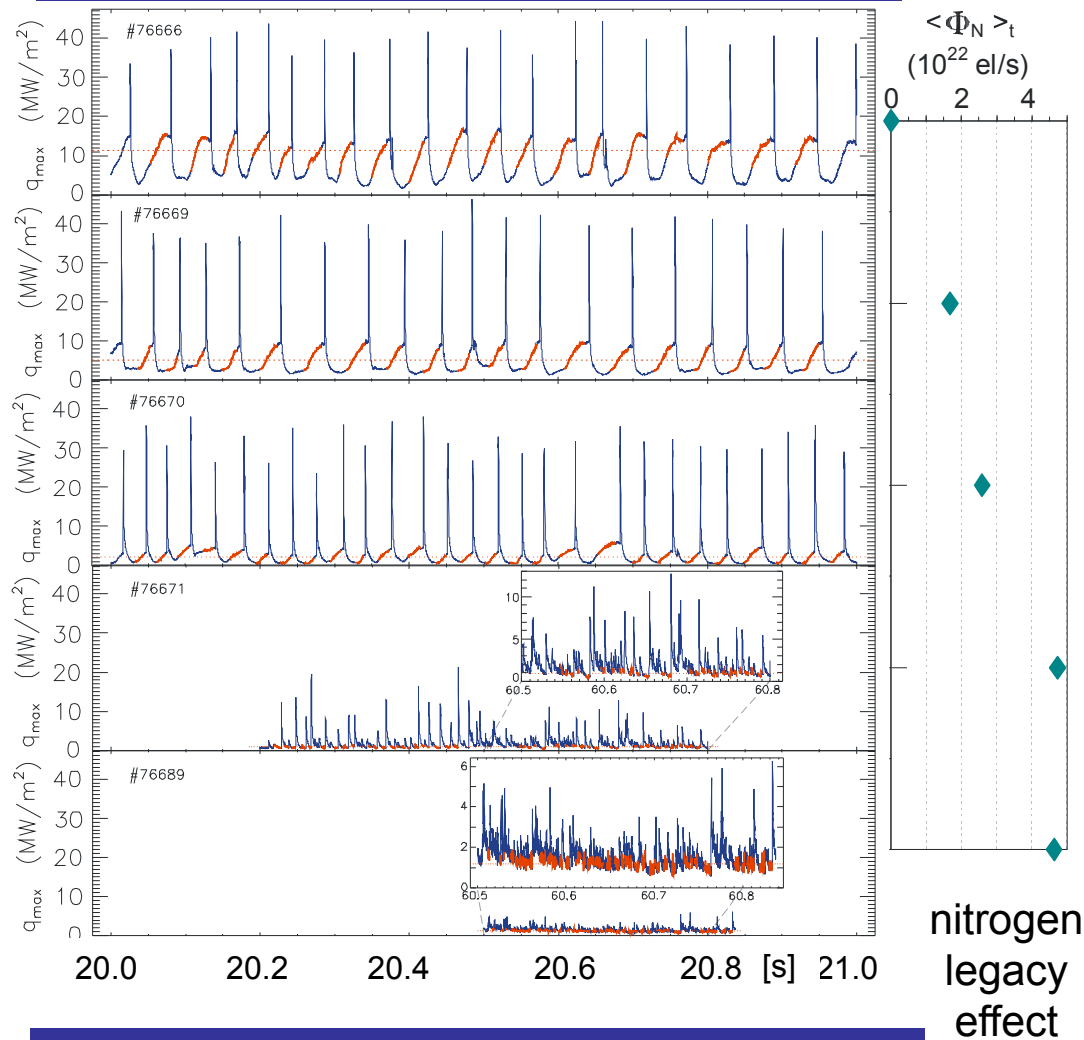
G.P. Maddison PSI

- Matrix scans in D fuelling and N (Ne) seeding
- D fuelling tends to raise plasma density, while seeding generally lowers it
- Outboard inter-ELM peak heat load declines substantially
- Clear shot-to-shot legacy effect of nitrogen

Radiation distribution in the divertor



Impact of nitrogen seeding on ELMs

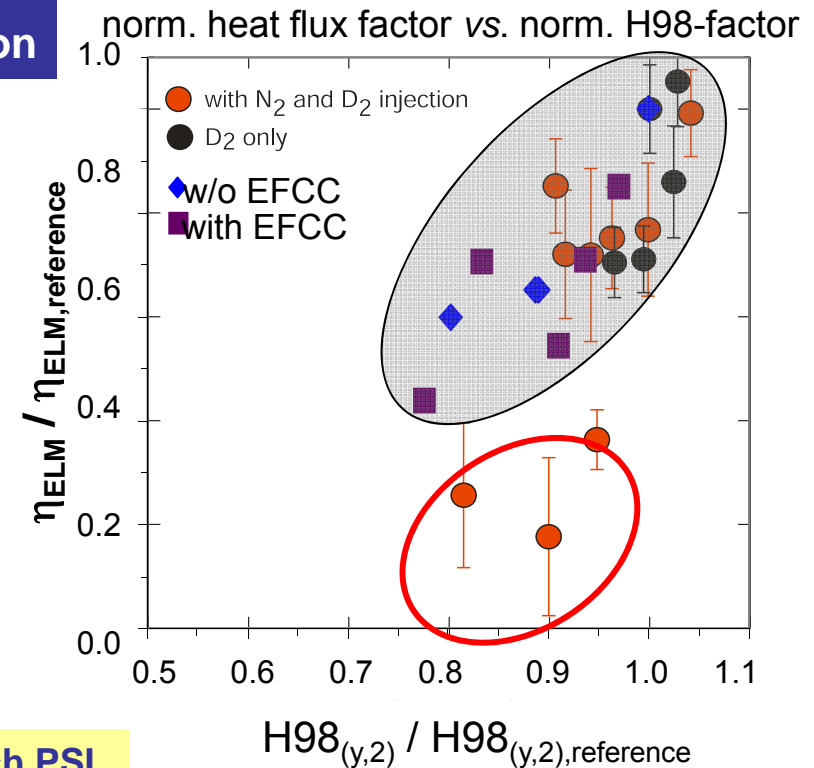
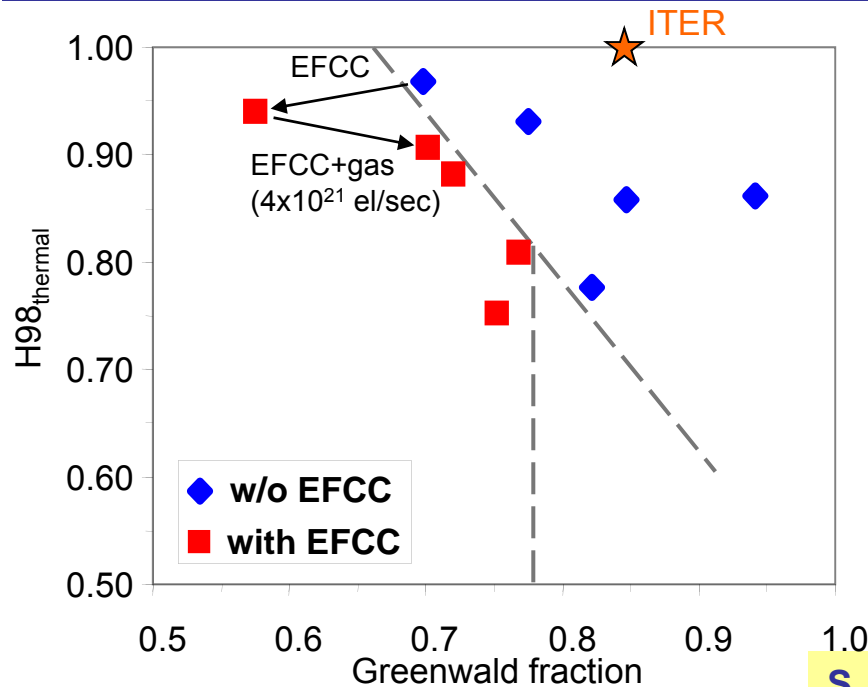


ELM energy and ELM heat load drops

- Three techniques have been compared at JET:

(i) magnetic perturbation (ii) vertical kicks (iii) deuterium & nitrogen fuelling

All techniques: Increase of ELM frequency
Density pump put
Moderate confinement degradation



- ELM pacing capabilities of kicks and EFCCs limited in fuelled plasmas (control backup)

Experience from AUG full tungsten divertor

- Absence of C radiation => “hot” divertor
- W erosion during ELM phases dominates

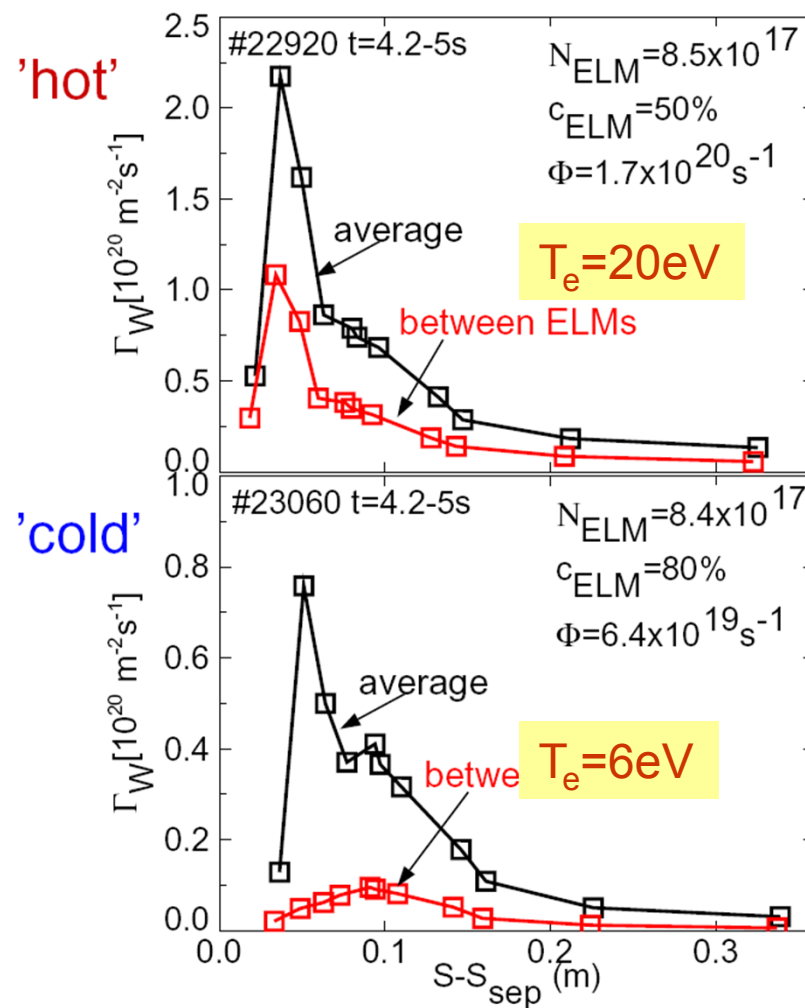
Means to reduce W sputtering in JET

- Radiation cooling
- ELM size control

Optimal operation

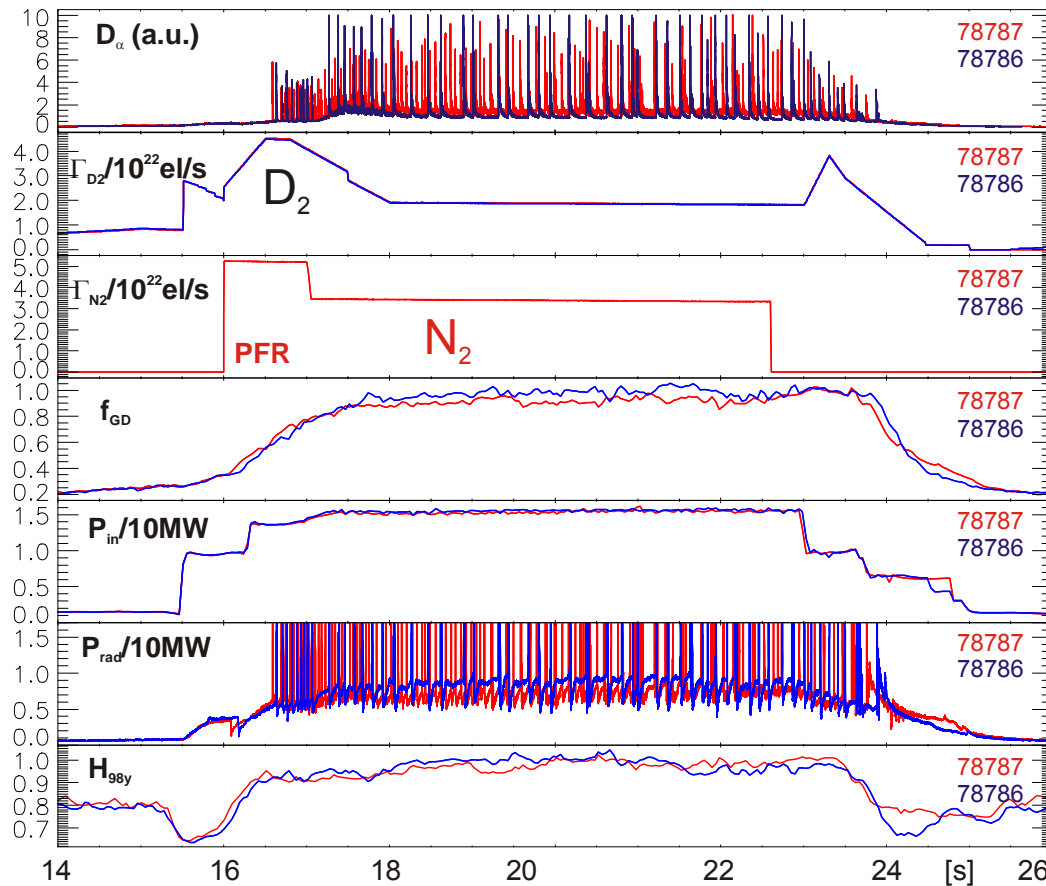
- Detached divertor plasma in the outer divertor with “mild” ELMs
- Natural detachment of the outer target by deuterium fuelling *S. Brezinsek et al. JNM 2009*
- Semi-detachment due to fuelling and nitrogen seeding *J. Rapp et al. NF 2010*

Experience from ASDEX Upgrade

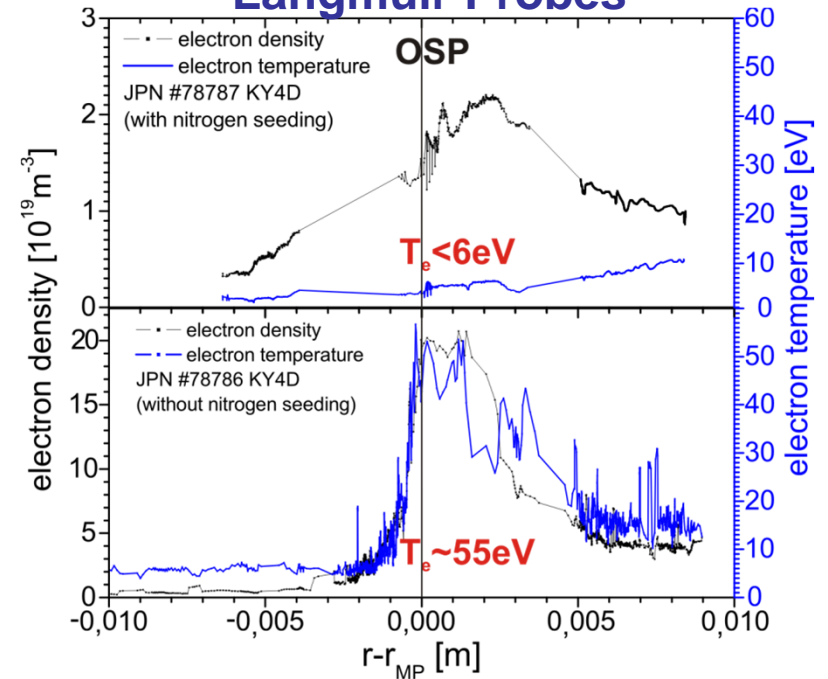


R. Dux et al. PSI2008

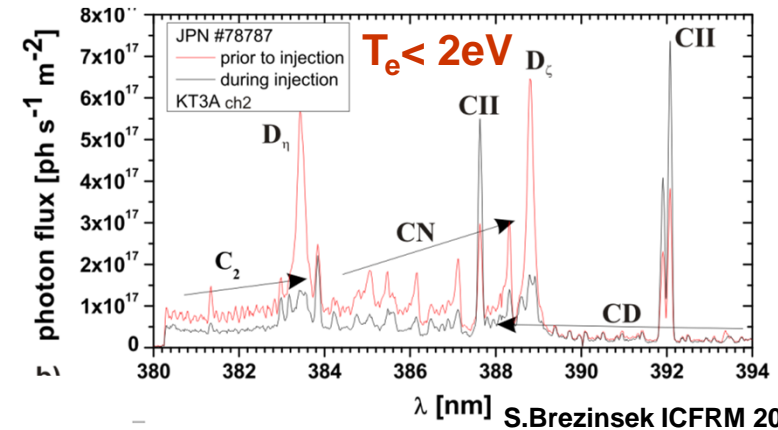
- Detachment and recombining plasma due to strong D₂ fuelling and N₂ seeding.
- ELM energy load acceptable



Langmuir Probes

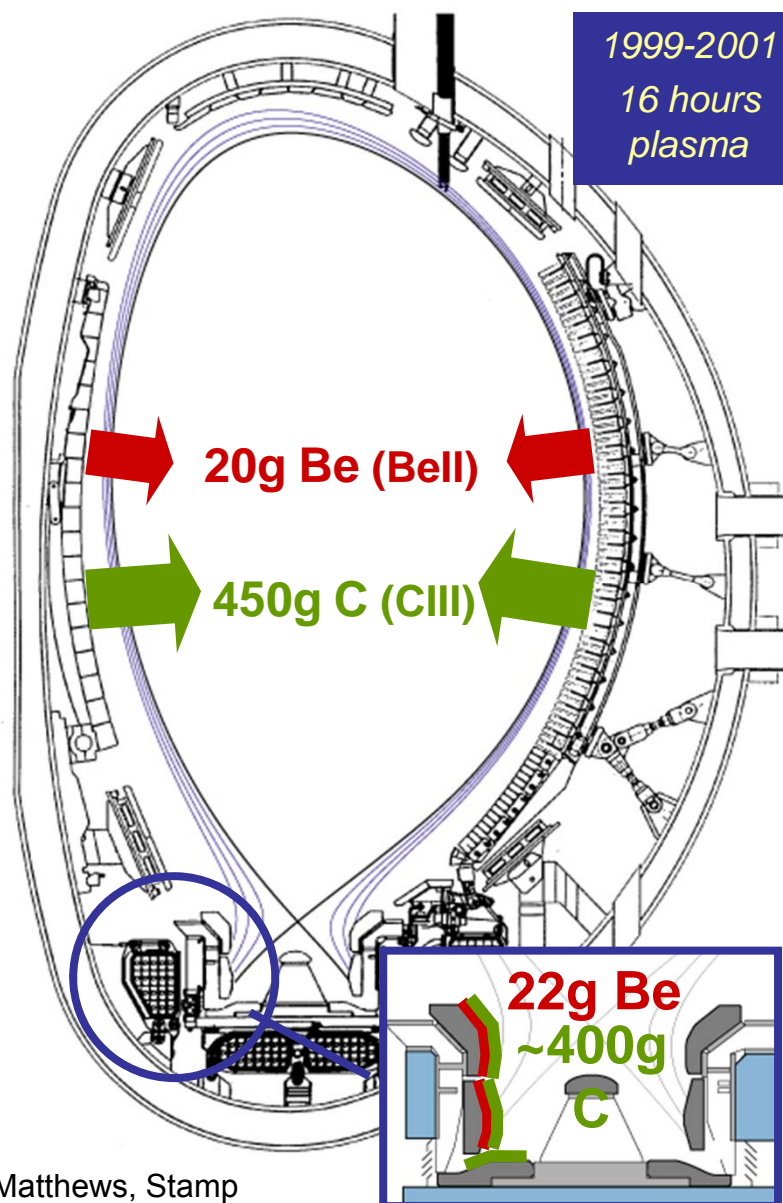


Balmer recombination lines ratio



S.Brezinsek ICFRM 2009

- **Reference plasmas for direct comparison of graphite and metallic wall**
 - Global material migration
 - **Migration to remote areas**
 - **Fuel retention data base**
 - Divertor functionality and SOL properties
 - ICWC wall conditioning
- References were taken in the first period of operation with moderate input power without any control techniques, but combinations have been applied in the later phase of preparation



Matthews, Stamp

JET with C/Be material mix

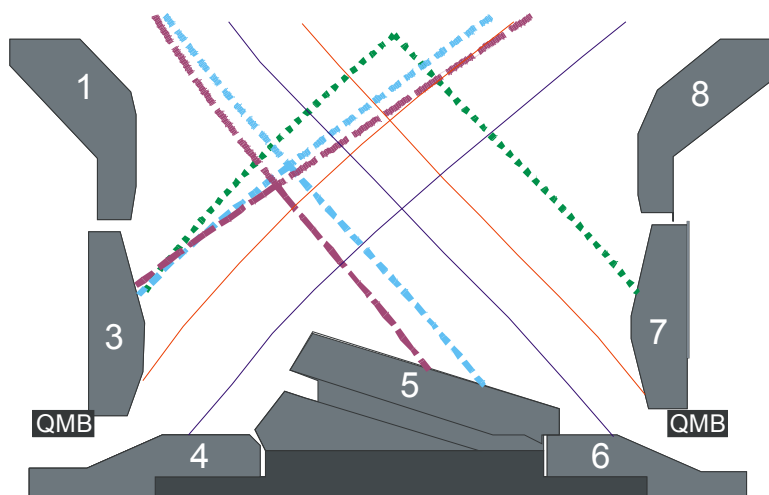
- Ion and neutral bombardment to the PFCs
- Main chamber dominant erosion source
- Material transport to the inner divertor due to SOL flows (deposition zone)
- C transport to remote areas in steps
- Low Be content in remote areas
- Outer divertor in balance (MKII GB)
- C transport to remote areas in outer divertor observed (MKII HD)

Database for migration / ILW comparison:

- New configurations and a large set of new diagnostics
- Variations in input power, plasma parameters, gas rate, regime etc.
- Reference discharges document the C/Be influx, concentration and migration

Intrinsic carbon transport

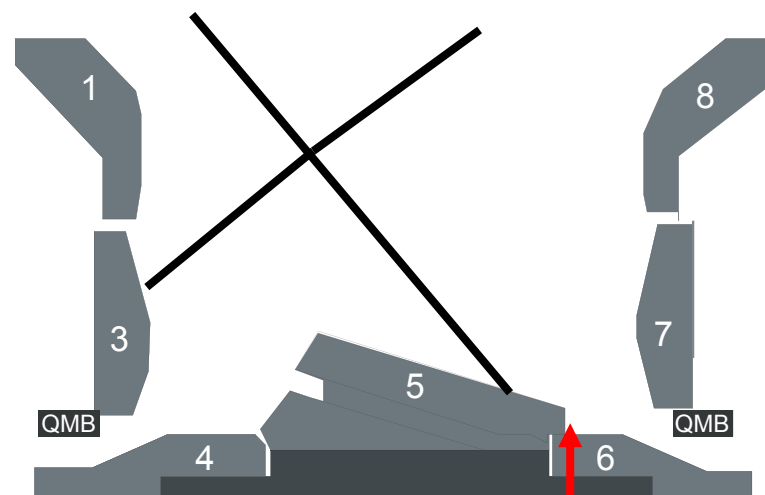
Material migration in outer divertor leg with comparable plasma and surface conditions



	inner QMB	outer QMB
OSP on tile 5	0.30 nm/s	0.58 nm/s
OSP on tile 5	0.66 nm/s	0.21 nm/s
OSP on tile 6	4.71 nm/s	-0.28 nm/s
OSP on tile 7	1.46 nm/s	0.37 nm/s
OSP on tile 7	0.58 nm/s	0.45 nm/s

Carbon tracer experiment

- ILW reference plasma in H-mode
- Circ. injection into outer divertor
- Gas balance analysis in parallel



total 7g ¹³C in 30 discharges

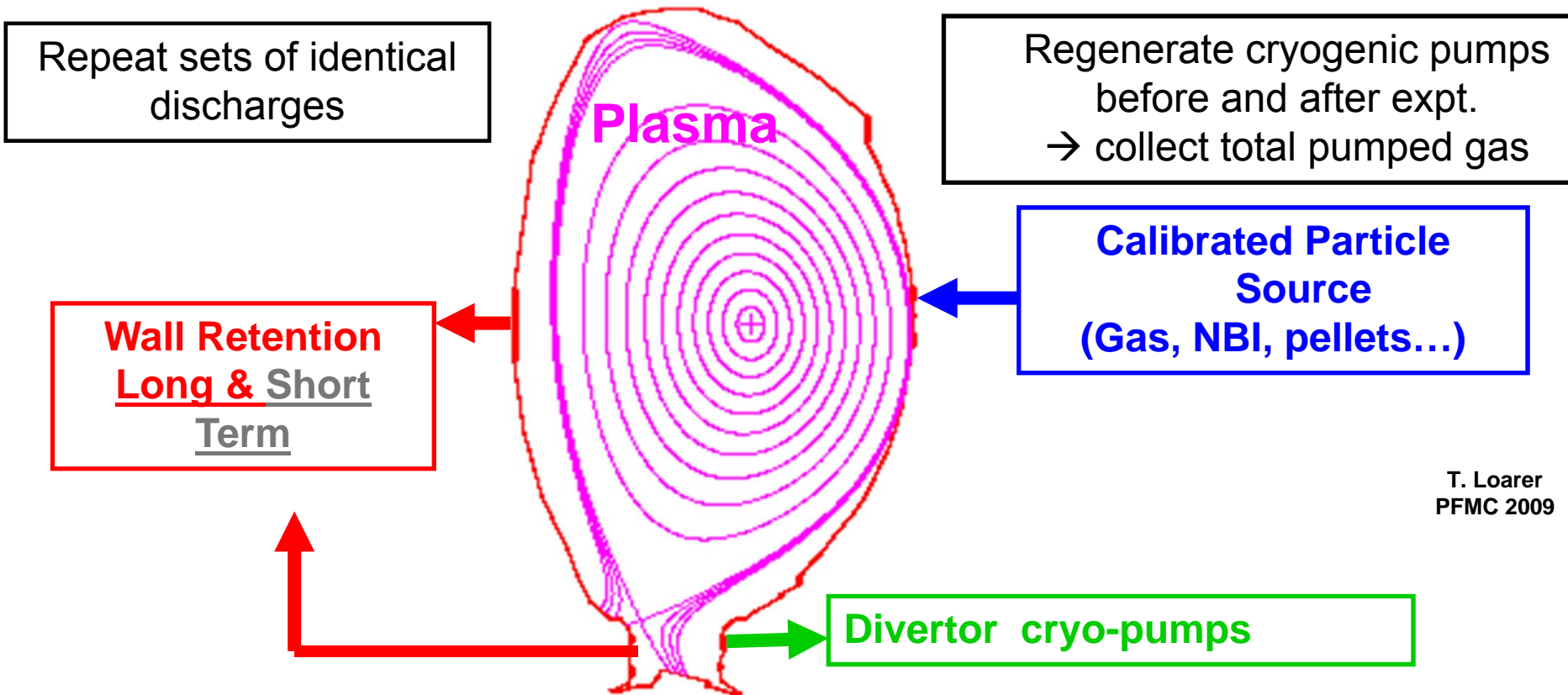
¹³CH₄

M. Rubel and P. Coad et al.

- 1/3 of ¹³CH₄ pumped by divertor cryo
- Post-mortem analysis ongoing

S. Brezinsek PSI

J. Likonen PSI



T. Loarer
PFMC 2009

$$\text{Injection} = \text{Pumped} + \text{Short Term Ret} + \text{Long Term Ret}$$

Total recovered from cryo-regeneration:
Pumped + intershot outgassing over ~800s (assumed equal to Short Term Ret)

Dedicated series of experiments: L and H mode in 2007-2009 (ILW references)

Plasma HT3R	Injection (Ds ⁻¹)	Heating phase (s)	Long term retention (Ds ⁻¹)	Divertor phase (s)	Long term retention (Ds ⁻¹)	Normalisation to L-mode
L-mode early X	~1.7×10 ²²	75	2.40×10 ²¹	170	1.05×10 ²¹	0.83
L-mode late X	~1.8×10 ²²	81	2.04×10 ²¹	126	1.27×10 ²¹	1.00
Type III	~1.7×10 ²²	72	2.40×10 ²¹	126	1.37×10 ²¹	1.08
Type I	~1.7×10 ²²	32	2.83×10 ²¹	50	1.70×10 ²¹	1.33

- Long term retention in carbon-dominated JET depends on plasma scenario
- Increase of retention from L-mode to moderate type I ELMy H-mode by 33%
- Moderate impact of the limiter phase in the fuel retention experiments

Additional data sets provide similar retention rates: ~1-2×10²¹ Ds⁻¹

- L- und H-mode in new LT configuration
- H-mode plasma with ELM control (vertical kicks)
- H-mode plasma including cleaning discharges for fuel recovery
- H-mode plasma with impurity seeding (nitrogen)
- H-mode plasma with tracer injection

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- **Plans for ILW exploitation**

Scientific headlines

Characterisation of the ILW
Exploration of ITER operating scenarios with the ILW
Physics issues essential to the efficient exploitation of ILW

Exploitation plan

- **Scientific experiments will begin with the very first plasma followed by progressive exploitation of all systems to their full capabilities**
- **Expansion of operational domain interspersed by periods of commissioning and interventions**
- **Step-wise increase of input power to minimise risks**
 - **Ohmic restart to document initial material migration and mixing**
 - **L-mode campaign, low power H-mode and standard H-mode**
- **Repetition of plasmas to document changes in wall conditions**
- **Accepted proposals presented at planning meeting 11/2010**

The needs to operate within the new plasma-facing components limits define to a certain extent the range of PSI investigations required to characterise and explore the ILW!

Second part of investigations is purely scientific driven to obtain input for predictions for ITER!

- Plasma operation at high density \Leftrightarrow divertor characterisation
- Impurity seeding \Leftrightarrow radiation distribution
- ELM pace-making techniques \Leftrightarrow power and heat load studies

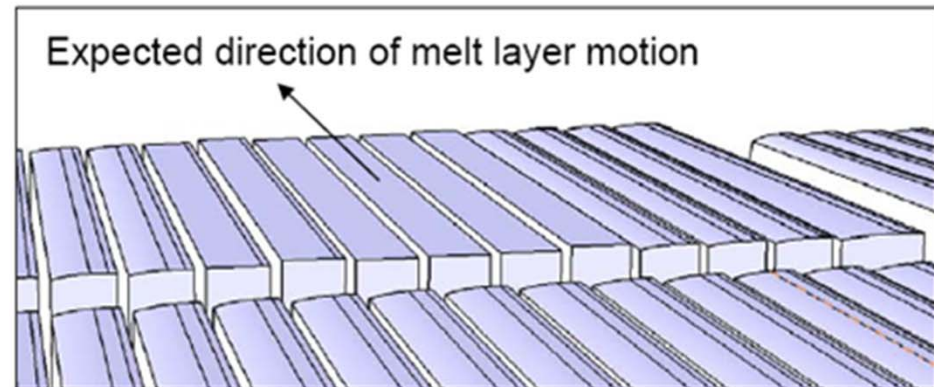
- Material migration and mixing studies (references)
- Fuel retention at fuel removal studies (references)
- Material limit experiments

- ... more than 200 proposals for 3 years

First plasma in July 2011

Suggested arrangement

- 16 lamellae are squared, at reference level
- 6 lamellae are squared, and displaced vertically



Yellow arrows indicate ref. level

