

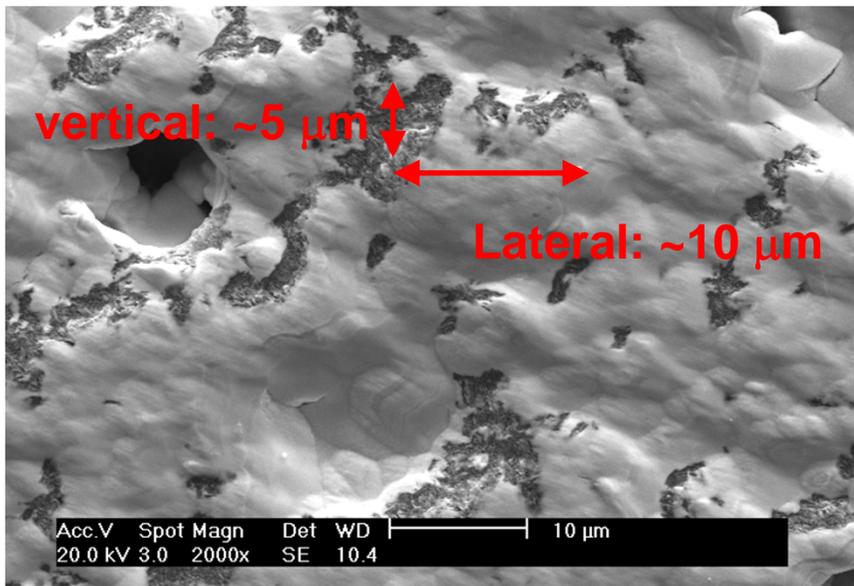
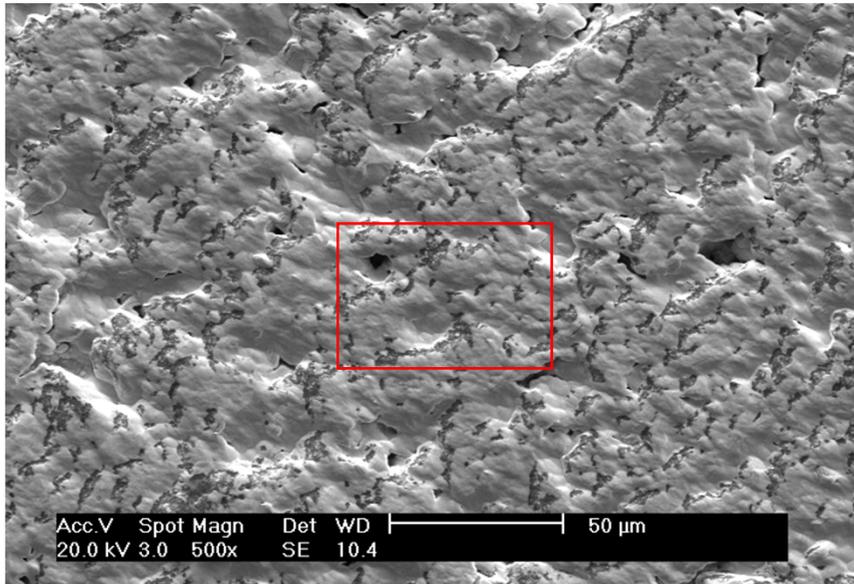
Impact of gyro-motion and sheath acceleration on the flux distribution on rough surfaces

K. Schmid

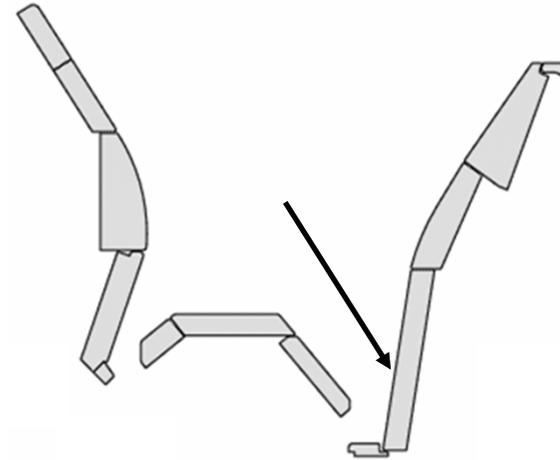
M. Mayer, C. Adelhelm, M. Balden

- ❖ **Introduction**
- ❖ **Experimental erosion patterns on W coated C**
- ❖ **Modeling particle trajectories in the sheath**
- ❖ **Impact angle distributions**
- ❖ **Variation of flux across rough surfaces**
- ❖ **Erosion distributions on real surfaces**
- ❖ **Summary**

Introduction



Inhomogeneous erosion of W in AUG
(M. Mayer PFMC 2009)



Initial: 1.5 μm W
 Mean erosion: 0.28 μm
 Max erosion: > 1.5 μm

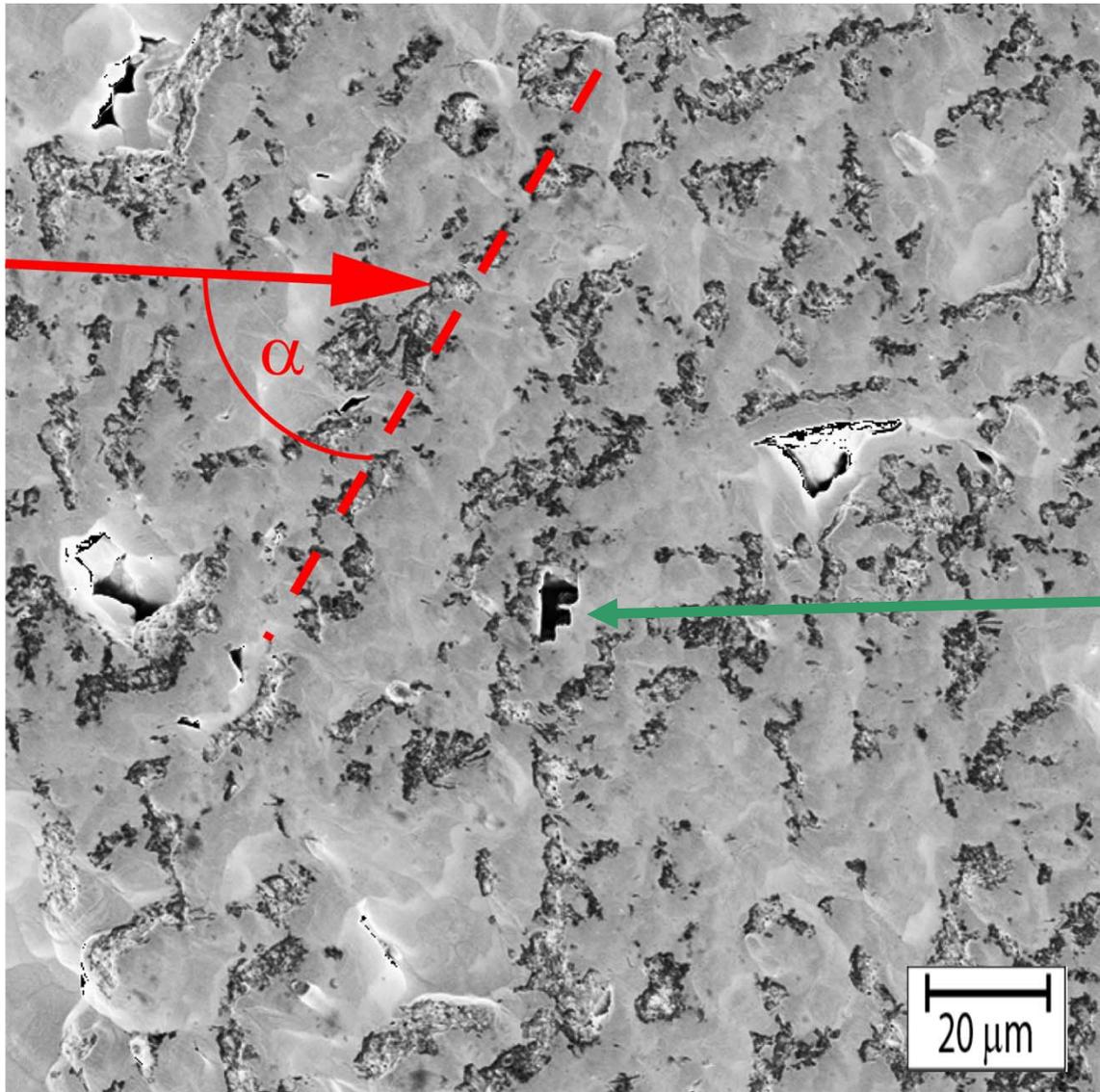
Very inhomogeneous erosion of marker

- ⇒ Larger local erosion on plasma-exposed surfaces than mean
- ⇒ Some W deposition in shadowed areas

➤ **Why is that so ?**

Experimental erosion patterns on W coated C

❖ SEM image of eroded AUG tile from outer divertor



➤ Inhomogeneous erosion pattern

➤ Angle $\alpha \neq 90^\circ$ between eroded ridges and B-Field
 → Hints towards ExB effect

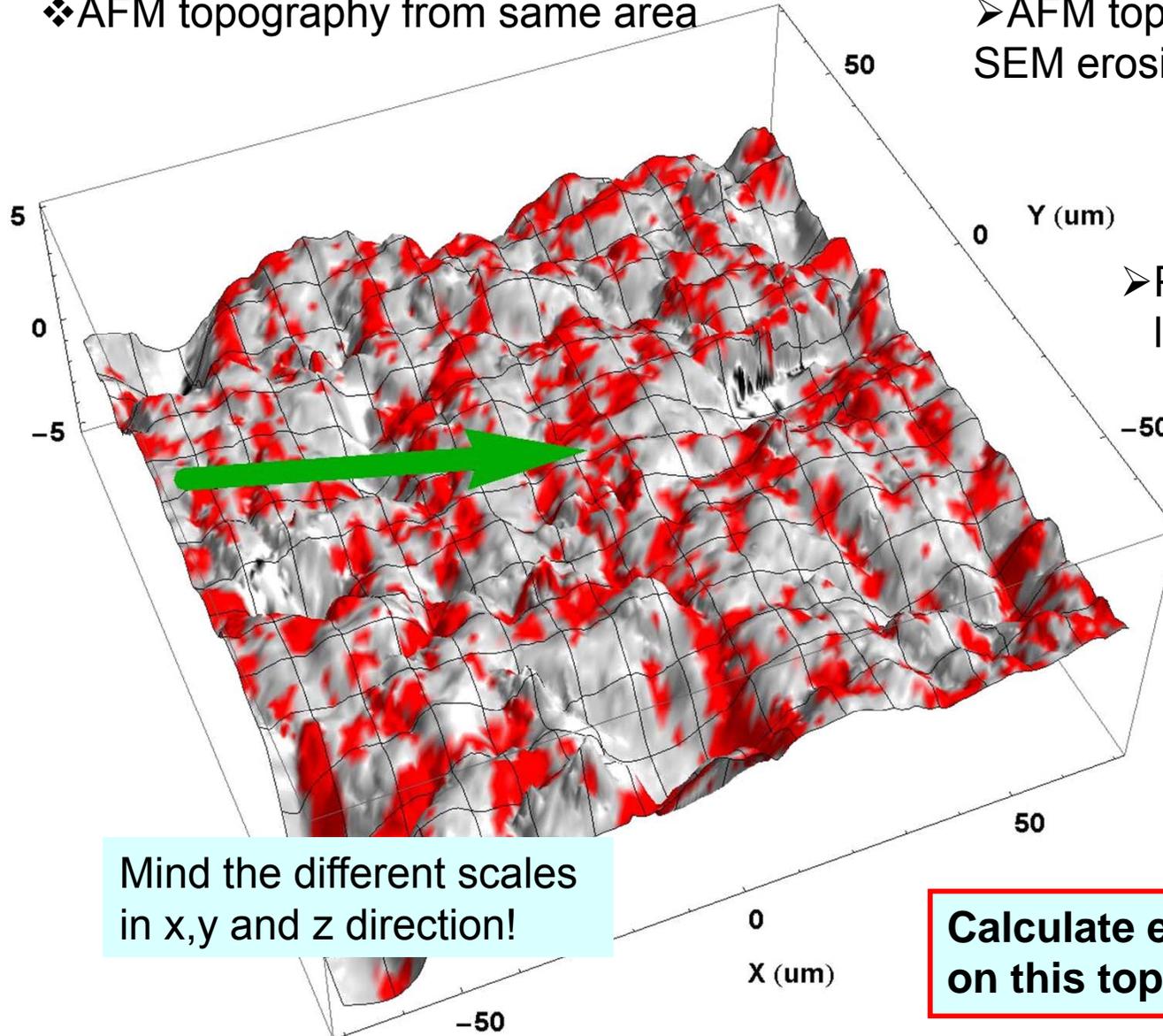
➤ Location marked by letter F in FIB

Experimental erosion patterns on W coated C



❖ AFM topography from same area

➤ AFM topography overlaid by SEM erosion pattern (red)



➤ Pronounced erosion on leading edges

Mind the different scales in x,y and z direction!

Calculate erosion flux distribution on this topography

❖ To calculate erosion fluxes one needs:

➤ Energy & Impact angles of energetic ions incident from the plasma

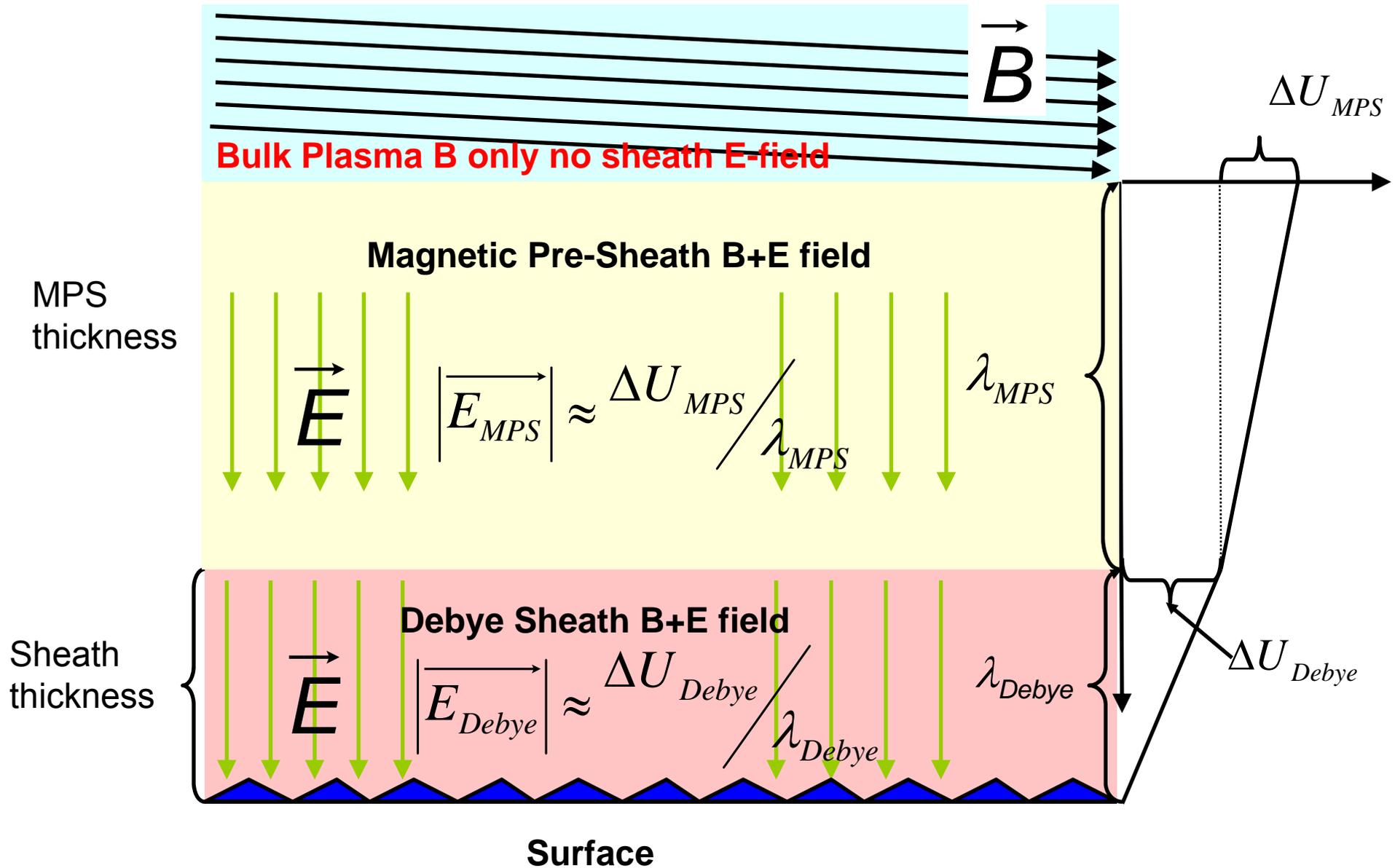
➤ Calculate trajectories and surface impact of particles moving in the sheath region of the plasma

- Model the electric fields in the sheath region
- Solve the equations of motion of particles in the sheath region

❖ Details see: ***K. Schmid et. Al Nucl. Fusion 50 (2010) 105004***

Modeling particle trajectories in the sheath

➤ Approximating the E -fields in the sheath



❖ With respect to initial conditions two cases are distinguished:

1. “Long range transport particles”

➤ Enter the sheath region from the bulk plasma on gyro orbits

2. “Prompt re-deposited particles”

➤ Are sputtered and emitted with a cosine distribution

➤ Are ionized either within their gyro orbit radius or inside the MPS

❖ Input parameters used in calculation

Parameter	B (T)	δ (°)	T_e (eV)	n_e (m^{-3})	$\frac{v_{ }}{c_s}$
Central value	1	5	20	10^{18}	1
Variation range	0.5-2	4-10	10 – 30	$10^{18} - 10^{19}$	0.1 - 1

➤ $l_{MPS} \sim 2000 \mu m$

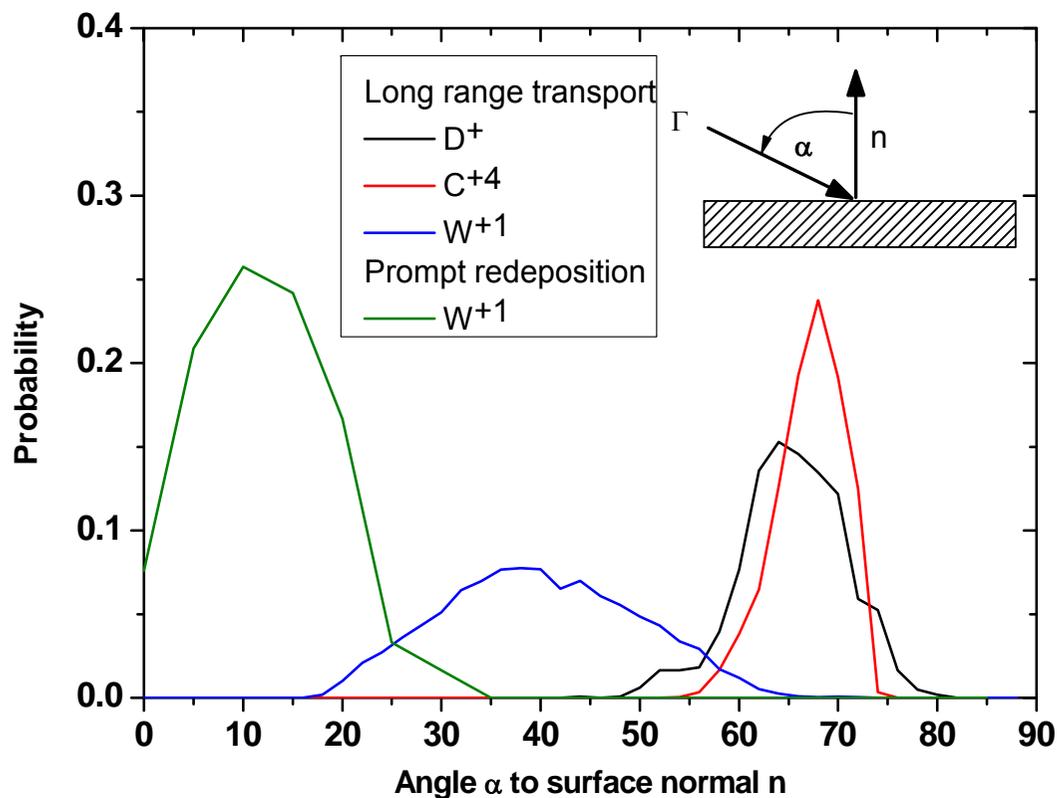
➤ $l_{Debye} \sim 33 \mu m$

➤ $E_{MPS} \sim 2 \times 10^4 \text{ V/m}$

➤ $E_{Debye} \sim 2 \times 10^5 \text{ V/m}$

❖ (E+B Field)

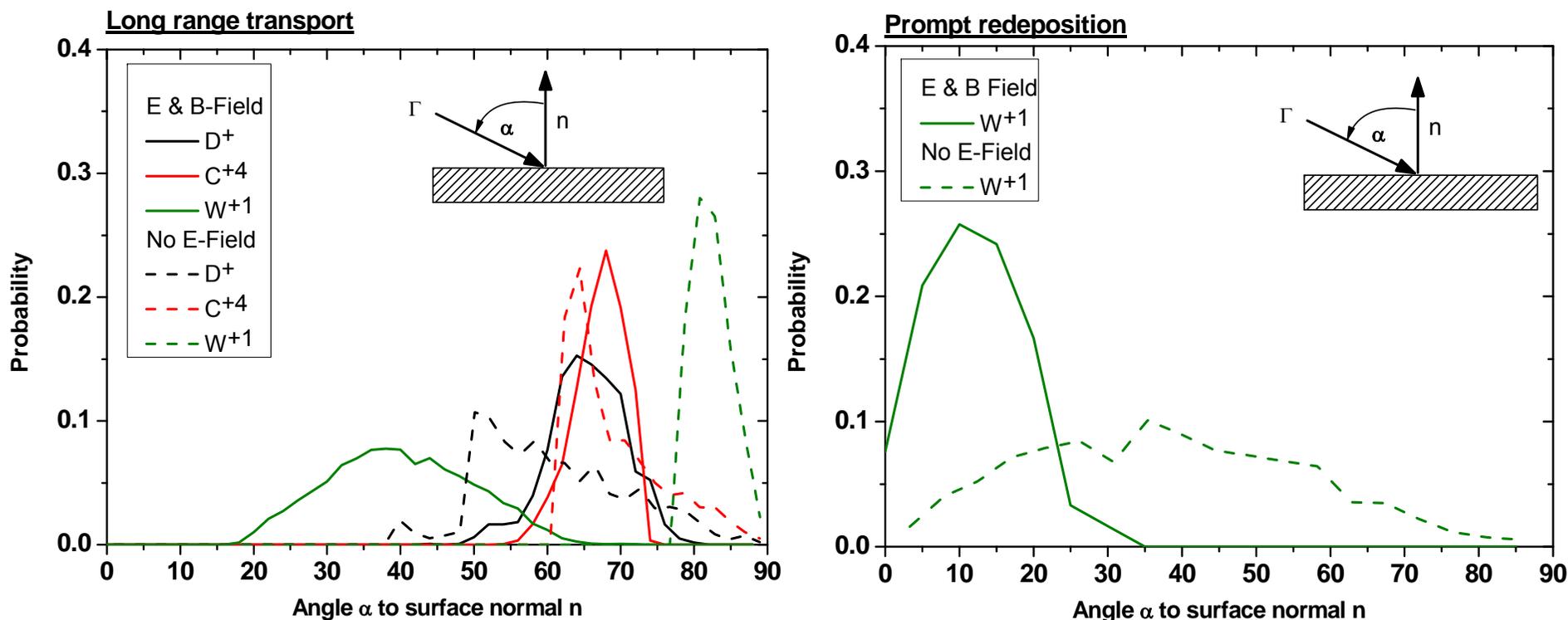
- Long range transport: Sample Ω , and Maxwell distribution
- For prompt redep.: Sample cosine distribution and ionization distance



➤ Long range transport particles impact at oblique angles

➤ Prompt re-deposited particles impact along surface normal

❖ (B Field only)

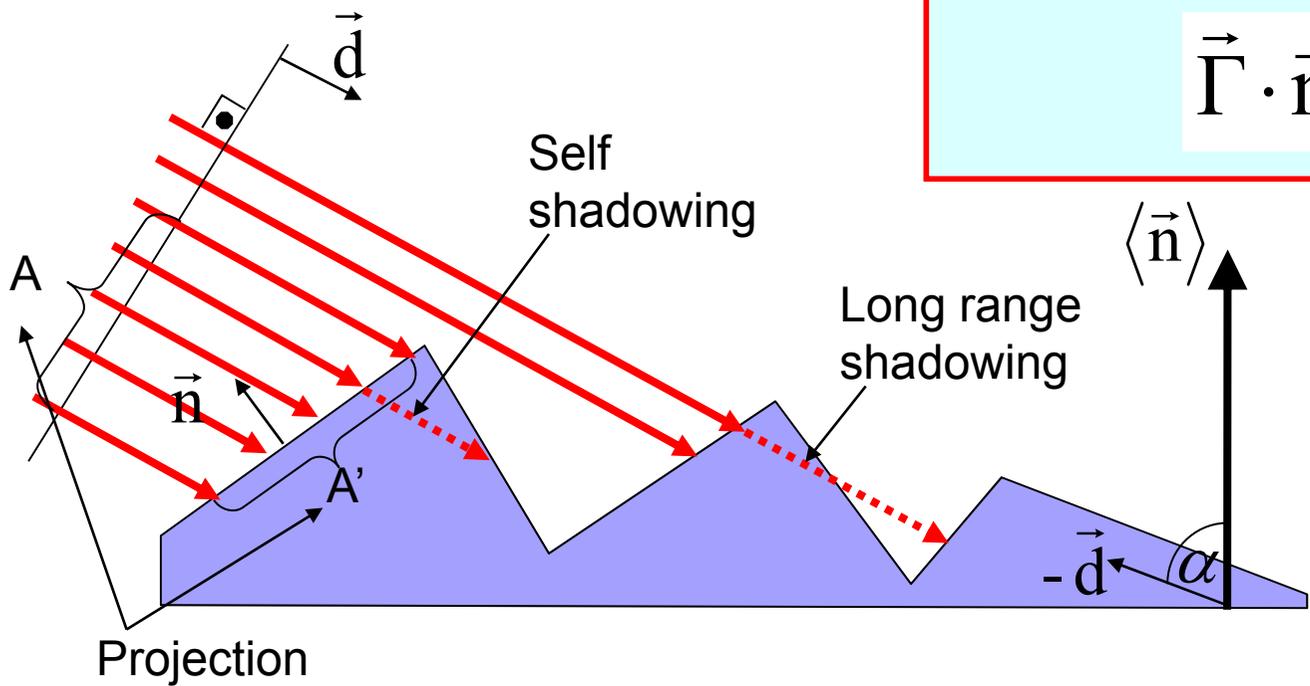


- Sheath acceleration has strongest influence on slow, heavy ($q/m \ll 1$) ions
- Prompt re-deposited particles are effected most

❖ Flux distribution of particles incident at angle α with respect to average surface normal

→ Lateral variation of flux & erosion determined by variation in

$\vec{\Gamma} \cdot \vec{n} (x, y)$



$$\Gamma(x, y) = \Gamma_0 f_{\text{Proj}}(x, y) f_{\text{Self-shadow}}(x, y) f_{\text{Long range shadow}}(x, y)$$

→ Possible explanation for experimentally observed erosion / deposition patterns

❖ Erosion on leading edged due to “Long range transport particles”

➤ Oblique impact angles are ~affected by roughness

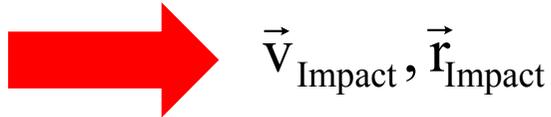
❖ Homogeneous deposition due to “Prompt re-deposited particles”

➤ Normal impact angles are ~**un**affected by roughness

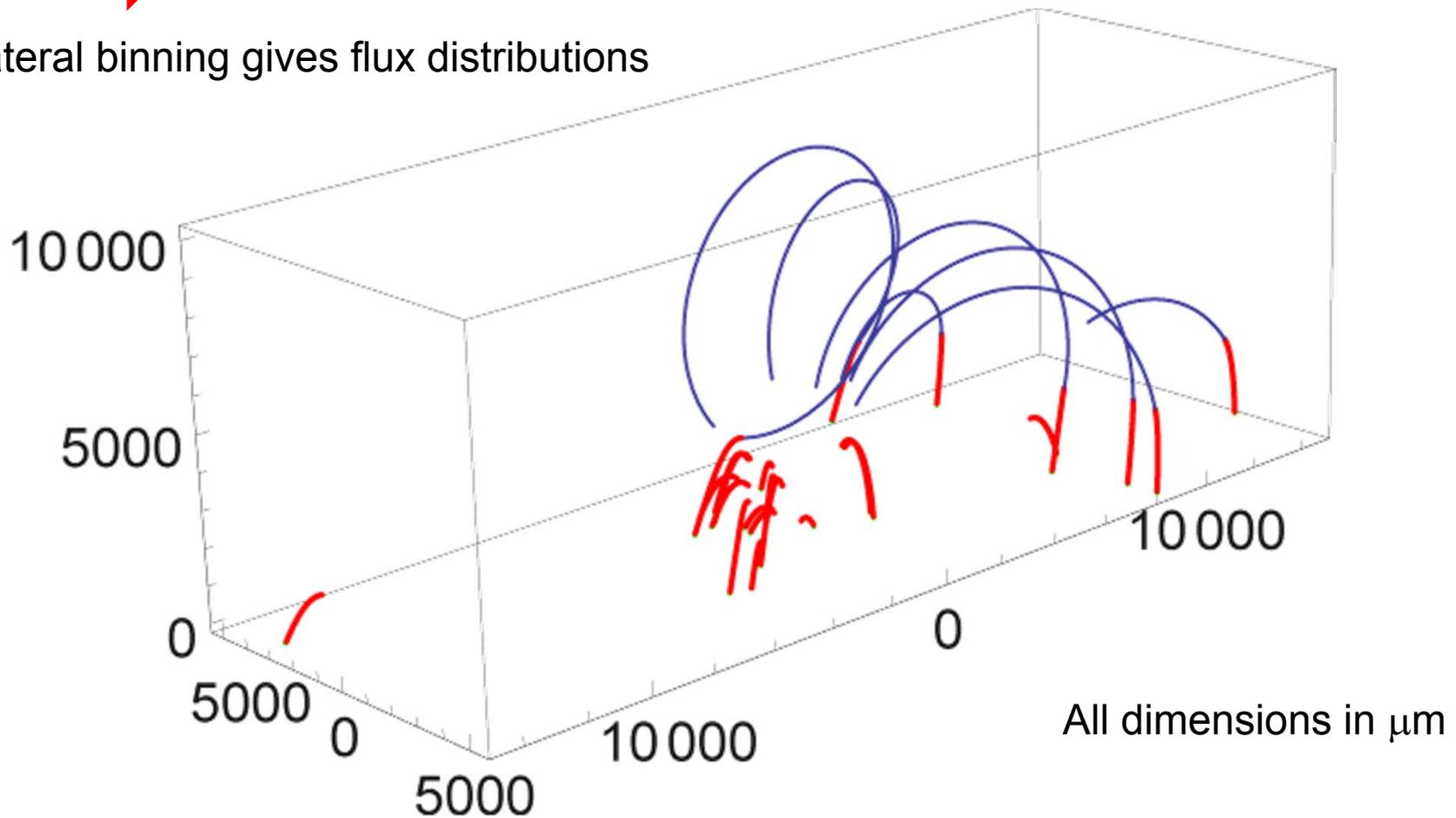
To test hypothesis → Calculate flux distributions on real surfaces

Flux distributions on real surfaces

- ❖ Ray tracing of particles, sampling the potential range of initial conditions
- ❖ Calculate first impact of trajectory with rough surface



- ❖ Lateral binning gives flux distributions



❖ Calculate erosion depth due to D and C⁺⁴ impact including

❖ Prompt re-deposition of W

❖ W self-sputtering

• Net erosion flux on bin j:

$$\Gamma_{net,j}^{ERO} = \left(\Gamma_j^{ERO,byD} (1 - \nu_c) \right) + \left(\Gamma_j^{ERO,byC} (\nu_c) \right) \quad (20)$$

$$+ \Gamma_{net,j}^{ERO} * R * Y_j^{\text{Eff by W}} - (\Gamma_{net,j}^{ERO} * R(1 - \text{Refl}))$$

$\Gamma_j^{ERO,byD}, \Gamma_j^{ERO,byC}$ = Erosion flux due to impact of D and C⁺⁴ respectively

ν_c = Fraction of C⁺⁴ in the incident flux

R = Fraction of eroded W that is prompt re-deposited

$Y_j^{\text{Eff by W}}$ = Effective W self sputtering yield

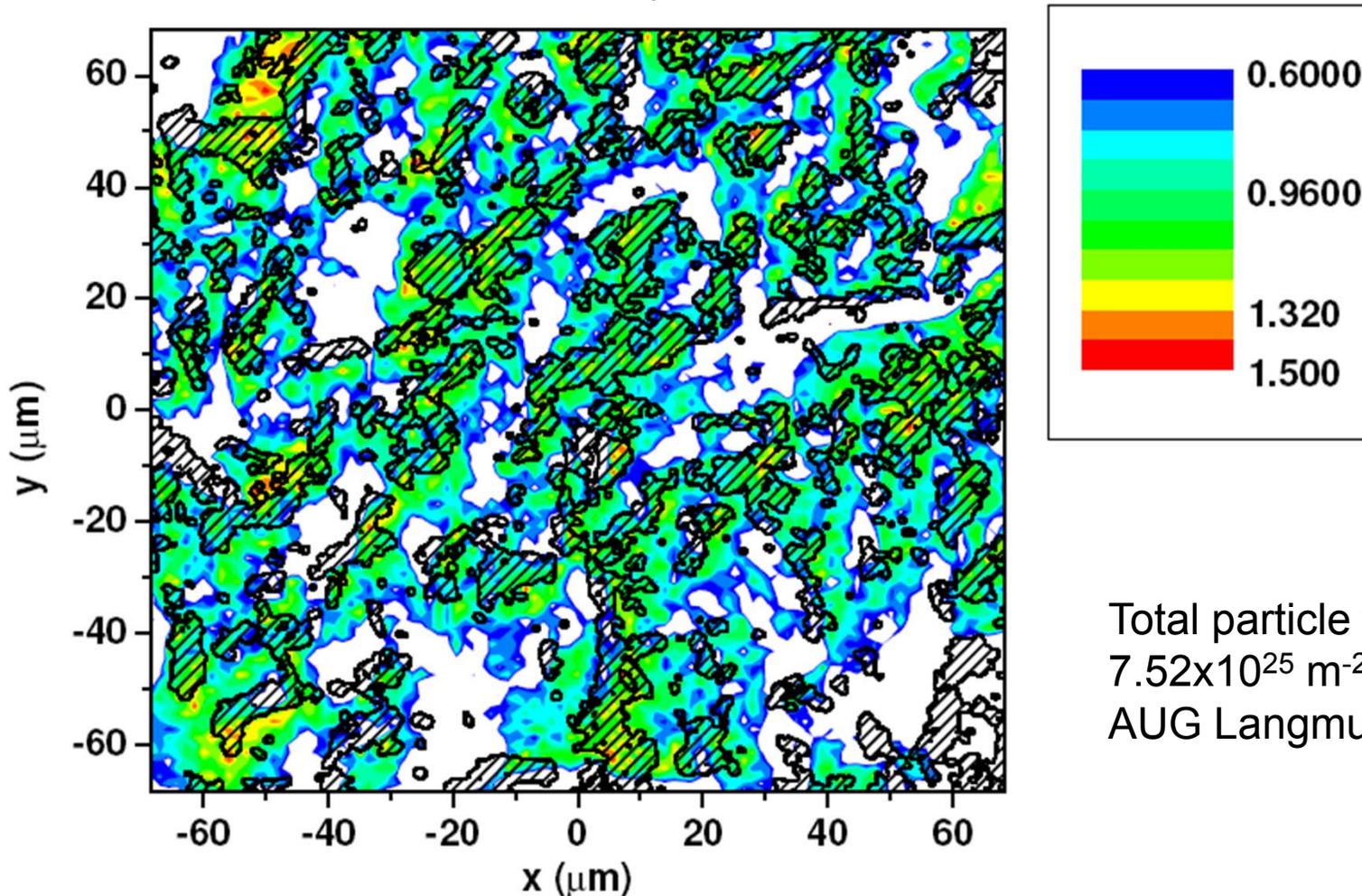
due to prompt re-deposited W at bin j

Refl = W reflection yield

➤ Solve equation 20 for $\Gamma_{net,j}^{ERO}$ multiply with time and divide by W number density

→ Total erosion depth

❖ Calculated erosion depth for $v_c = 0.3\%$ and $R = 30\%$



Total particle fluence of $7.52 \times 10^{25} \text{ m}^{-2}$ taken for AUG Langmuir probe data

➤ Calculated erosion pattern matches experimental erosion patterns using reasonable values for v_c and R

- ❖ A model explaining inhomogeneous erosion deposition on rough surfaces based on $E \times B$ motion in the plasma sheath is proposed:
 - Long range transport particles erode the leading edges
 - Prompt re-deposited material deposits homogeneously, also areas shadowed to the long range transport particles

- ❖ The acceleration in the electrostatic sheath field has a strong impact on the impact angle distribution. (In particular for heavy ions)

- ❖ The model reproduces both the erosion pattern shape and the total amount of eroded material.

Discussion slides



Modeling particle trajectories in the sheath

➤ Approximating the E -fields in the sheath

$$\Delta U_S = \frac{1}{2} T_e \log \left(\frac{2\pi m_e (T_e + T_i)}{T_e m_i} \right)$$

- ❖ Total sheath potential drop
- ❖ ~constant with B-field angle δ

T_i, T_e = Ion and electron temperature respectively

m_i, m_e = Ion and electron mass respectively

$$\Delta U_S = \Delta U_{MPS} + \Delta U_{DS}$$

MPS = Magnetic pre-sheath, DS = Debye sheath

$$\Delta U_{MPS} = \frac{T_e}{e_0} \ln (\cos(\pi - \delta))$$

$$\Delta U_{DS} = \Delta U_S - \Delta U_{MPS}$$

$$l_{MPS} = \sqrt{6} \left(\frac{c_s}{\omega} \right) \sin(\delta)$$

$$l_{DS} = \sqrt{\frac{\epsilon_0 T_e}{e_0 n_e}}$$

$$E_{MPS} = \frac{\Delta U_{MPS}}{l_{MPS}}$$

$$E_{DS} = \frac{\Delta U_{DS}}{l_{DS}}$$

- ❖ MPS part of the total sheath drop
- ❖ Varies with B-field angle δ

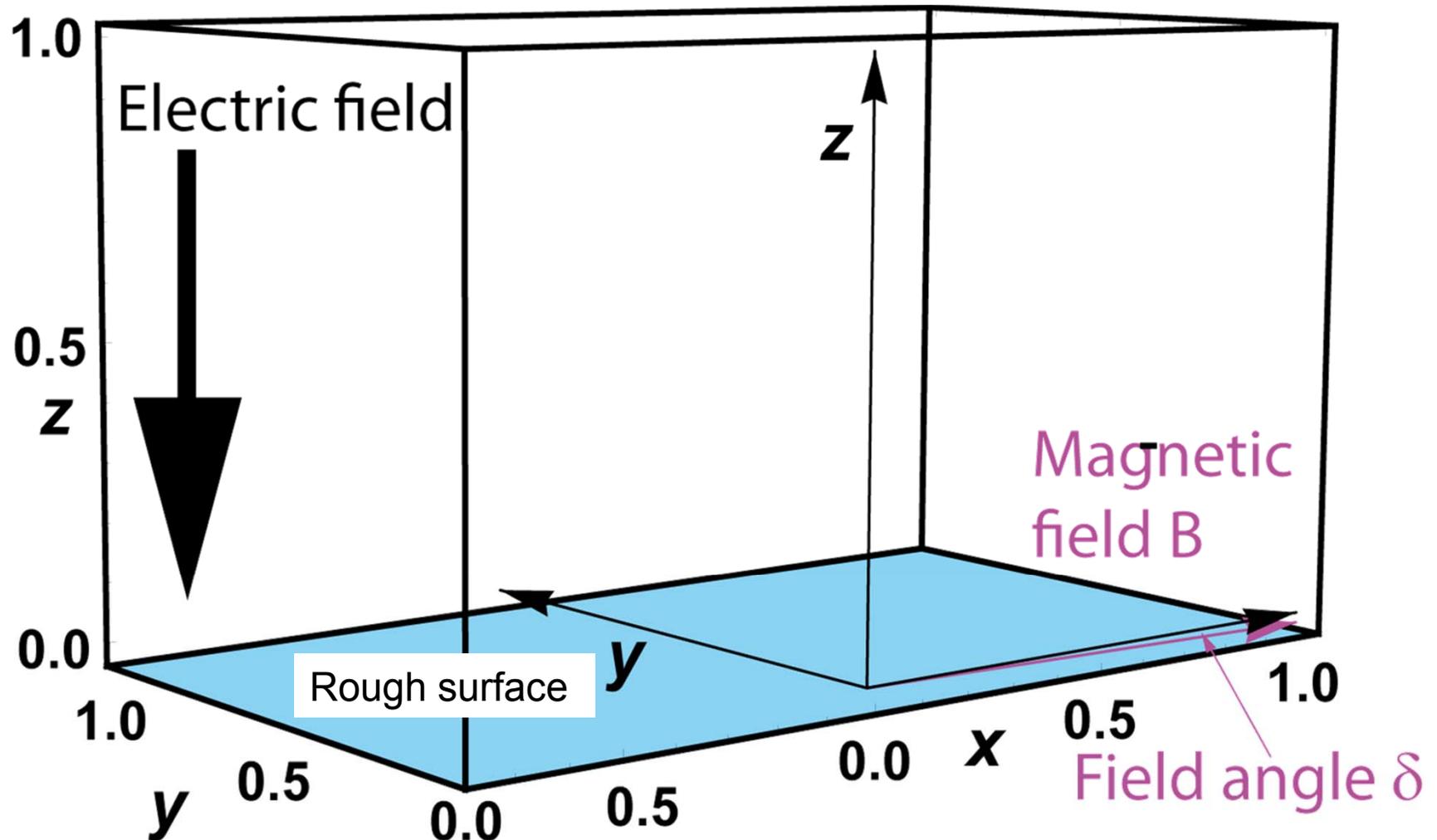
- ❖ Debye part of the total sheath drop

Modeling particle trajectories in the sheath

➤ *Solving the equations of motion*



❖ Coordinate system used



➤ Solving the equations of motion

❖ Equations of motion

$$\ddot{x}(t) = \beta B_Z \dot{y}(t)$$

$$\ddot{y}(t) = \beta (B_X \dot{z}(t) - B_Z \dot{x}(t))$$

$$\ddot{z}(t) = \beta (-B_X \dot{y}(t) - E_Z)$$

$$\beta = \frac{q}{m} \text{ Charge to mass ratio}$$

$$E_Z = \text{Z-Component of the electrical field } \vec{E} = (0, 0, E_Z)$$

➤ Solved using Mathematica, yields analytical solution

➤ Trajectories require initial conditions: $\vec{r}(t = 0) = \vec{r}_{\text{Init}}$

$$\dot{\vec{r}}(t = 0) = \vec{v}_{\text{Init}}$$

Modeling particle trajectories in the sheath



➤ Solving the equations of motion

1. “Long range transport particles”

$$\vec{v}_{init} = (v_{\parallel}, V_{\perp}, 0) \cdot \mathbf{M}$$

$$\mathbf{M} = \mathbf{R}(\Omega, (1, 0, 0)) \cdot \mathbf{R}(\delta, (0, 1, 0))$$

v_{\parallel} = Velocity along magnetic field

v_{\perp} = Velocity perpendicular to magnetic field

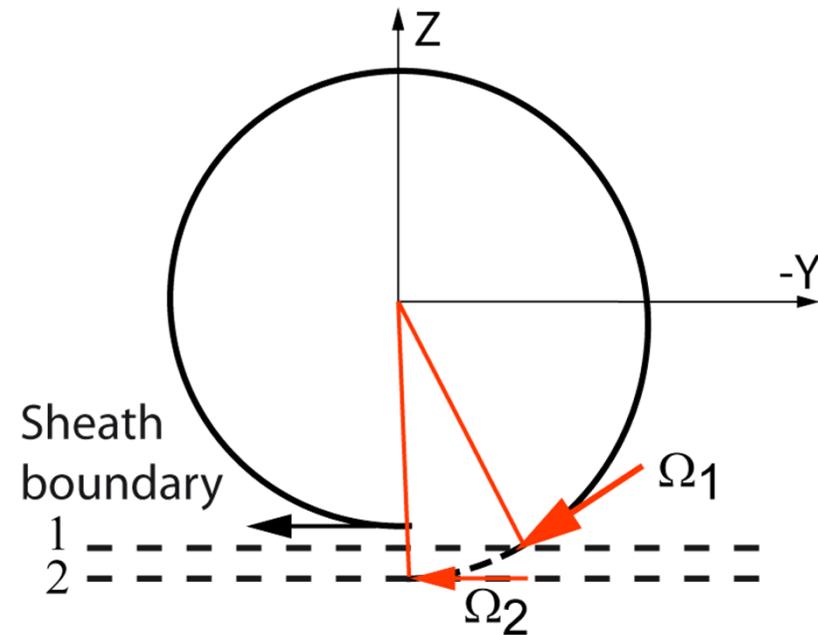
δ = magn. Field angle

Ω = Gyro orbit phase angle on MPS impact

➤ Ω Depends on velocity v_{\parallel}/v_{\perp} and q/m ratio

$$|v_{\parallel}| \sim v_{\text{Bohm-D}}(T_e)$$

$$|v_{\perp}| \sim \text{Maxwell distributed}(T_e)$$

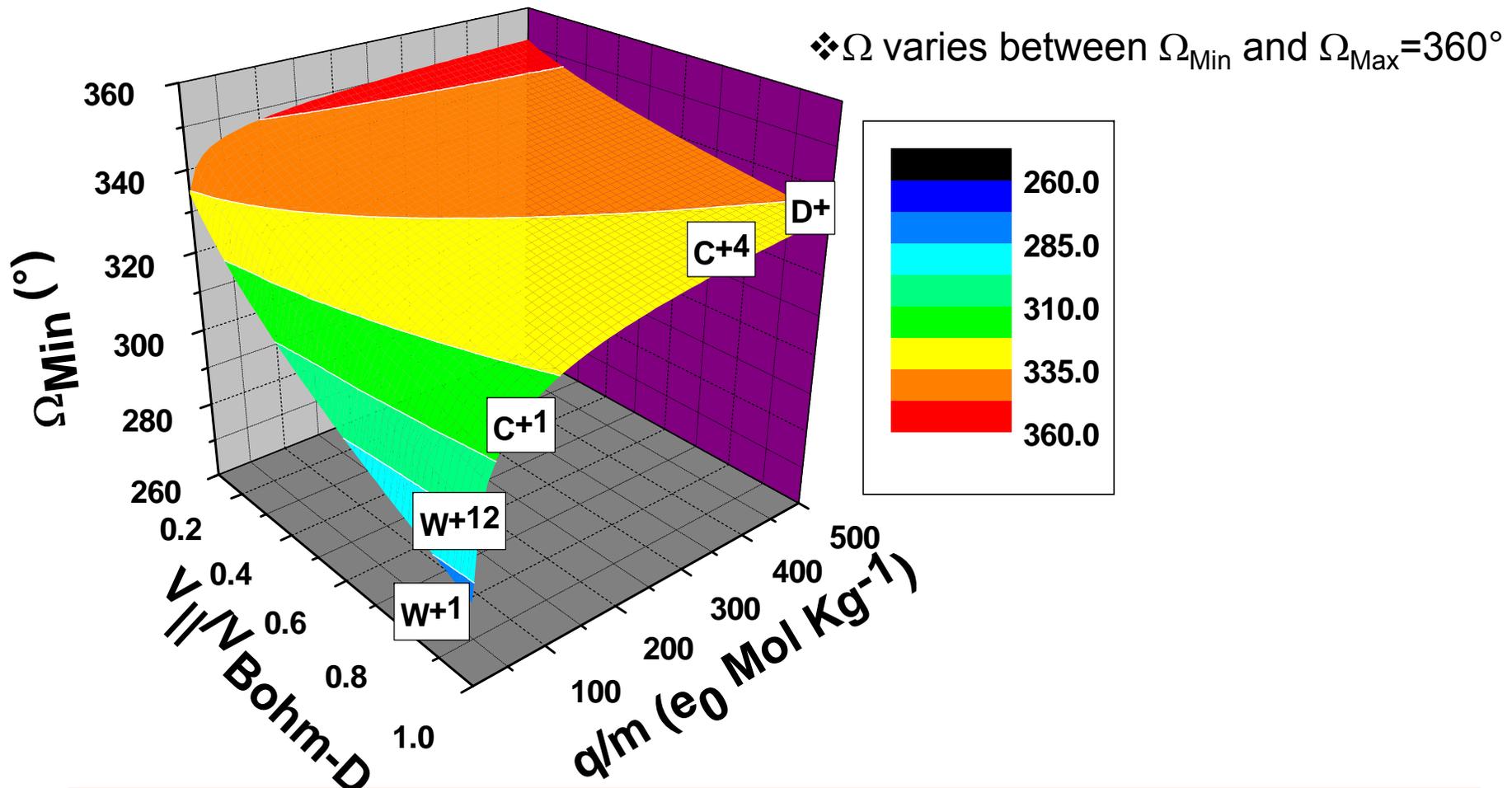


Modeling particle trajectories in the sheath



➤ Solving the equations of motion

❖ Possible values for Ω for “Long range transport particles”



- Light particles → Small impact angle range → Narrow impact angle distribution
- Heavy particle → Broad impact angle range → Broad impact angle distribution

2. “Prompt re-deposited particles”

❖ “Sputter launch” according to cosine distribution

$$\vec{d}_{Cos} = (0, 0, 1) \cdot \mathbf{R}(\vartheta, (1, 0, 0)) \cdot \mathbf{R}(\varphi, (0, 0, 1))$$

$$\vartheta = \arcsin(\sqrt{r_\vartheta})$$

$$\varphi = 2\pi r_\varphi$$

$\mathbf{R}(\alpha, \vec{r})$ = Rotation matrix around axis \vec{r} by angle α

r_φ, r_ϑ = Uniform random numbers from 0-1

❖ Initial velocity $\frac{1}{2}$ surface binding energy (typical for physical sputtering)

$$|\vec{v}_{init}| = \sqrt{\frac{2 \langle E_{Sput} \rangle}{m}}$$

$\langle E_{Sput} \rangle$ = Mean energy of sputtered particles

m = Mass of sputtered particle

\vec{V}_{Init}

2. “Prompt re-deposited particles”

❖ Ionized to +1 at normal distance z above surface

$$z_{\text{Min}} < z < z_{\text{Max}}$$

$$z_{\text{Min}} = \lambda_{\text{Debye}}$$

$$z_{\text{Max}} = \max(l_{\text{MPS}}, r_{\text{gyro}})$$

→ For W^{+1} typical ionization distance from surface is several mm

❖ No variation in ionization probability within z_{Min} and z_{Max} taken into account

➤ *Limits of the model description*

- Feature height \sim Sheath dimension
 - Surface roughness influences sheath electric field
 - Requires PIC-Code or similar to calculate field distribution
 - Can not be treated in the simple frame of this model

- Feature height \gg Sheath dimension
 - Sheath follows surface roughness
 - Particles impact locally on “flat” surface
 - Electric field not homogeneous near edges
 - Can partly be treated in the simple frame of this model

- Feature height \ll Sheath dimension
 - Sheath not influenced by surface structure
 - Particles impact along their trajectories on the different surface inclinations
 - Flux and impact angle distribution can be calculated (see following slides)

- ❖ Calculate impact angles on flat surfaces

$$\alpha = \arccos \left(\frac{-\vec{v}_{imp} \cdot \vec{n}_{imp}}{|\vec{v}_{imp}| * |\vec{n}_{imp}|} \right)$$

- ❖ Radius of curvature ρ

$$\rho = \frac{|\partial_t \vec{r}(t)|^3}{\partial_t \vec{r}(t) \times \partial_{t,t} \vec{r}(t)} \quad \sim \text{mm} \gg \text{roughnes}$$

→ Particles impinge essentially along straight lines on the rough surface

❖ Local surface normal

$$\vec{r} = (x, y, z(x, y))$$

$$\vec{n} = \frac{\partial \vec{r}}{\partial x} \times \frac{\partial \vec{r}}{\partial y}$$

❖ Projection:

$$f_{proj} = -\vec{\Gamma} \cdot \vec{n}$$

$$\vec{\Gamma} = \Gamma_0 * \vec{d}$$

$$\vec{d} = \text{Normalized direction vector}$$

$$\vec{n} = \text{Local normalized surface normal}$$

→ Lateral variation of flux & erosion determined by variation in

$$\vec{\Gamma} \cdot \vec{n} (x, y)$$

❖ Self shadowing:

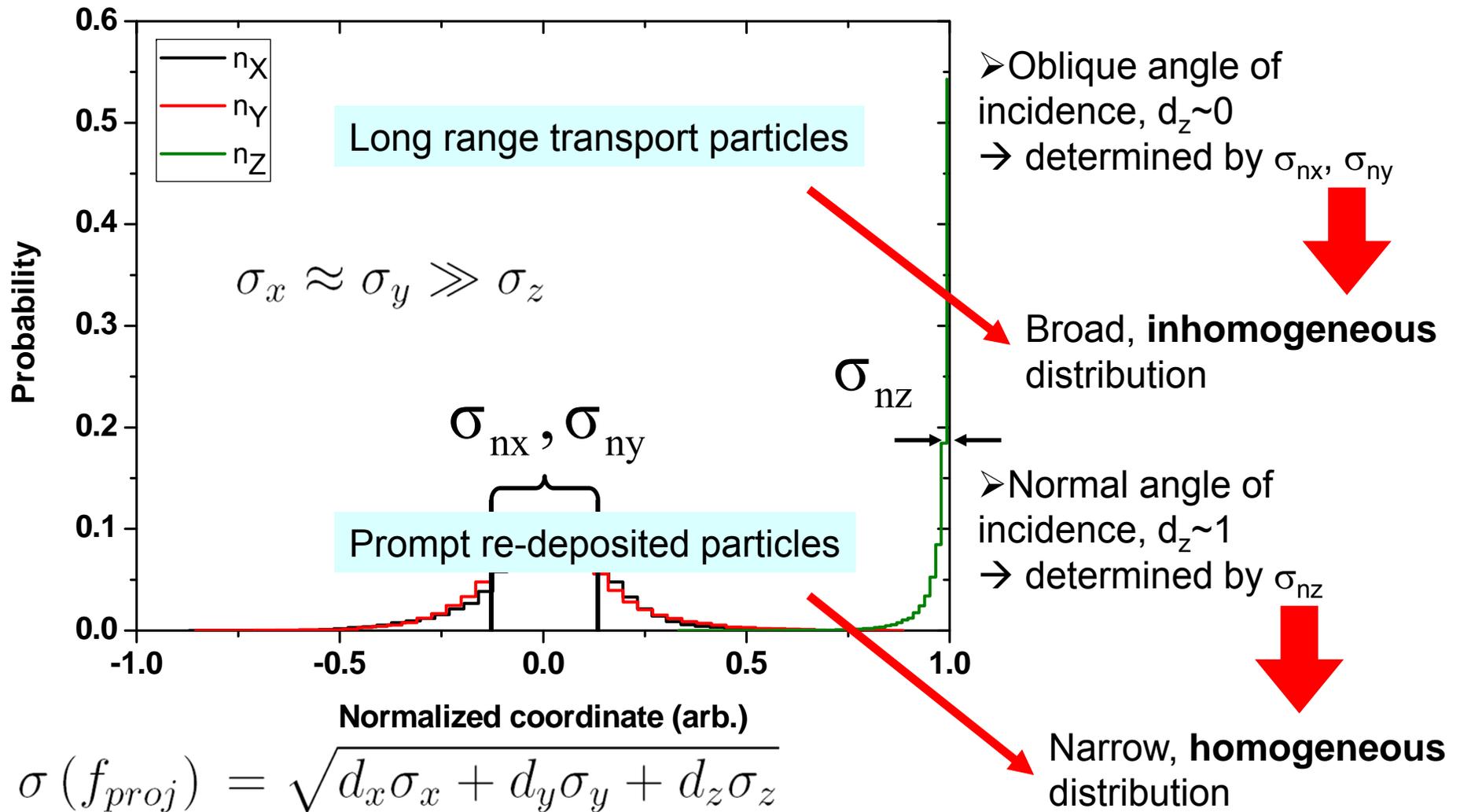
$$f_{self} = \begin{cases} 1 & -\vec{\Gamma} \cdot \vec{n} \geq 0 \\ 0 & -\vec{\Gamma} \cdot \vec{n} \leq 0 \end{cases}$$

➤ Long range shadowing: Requires ray tracing

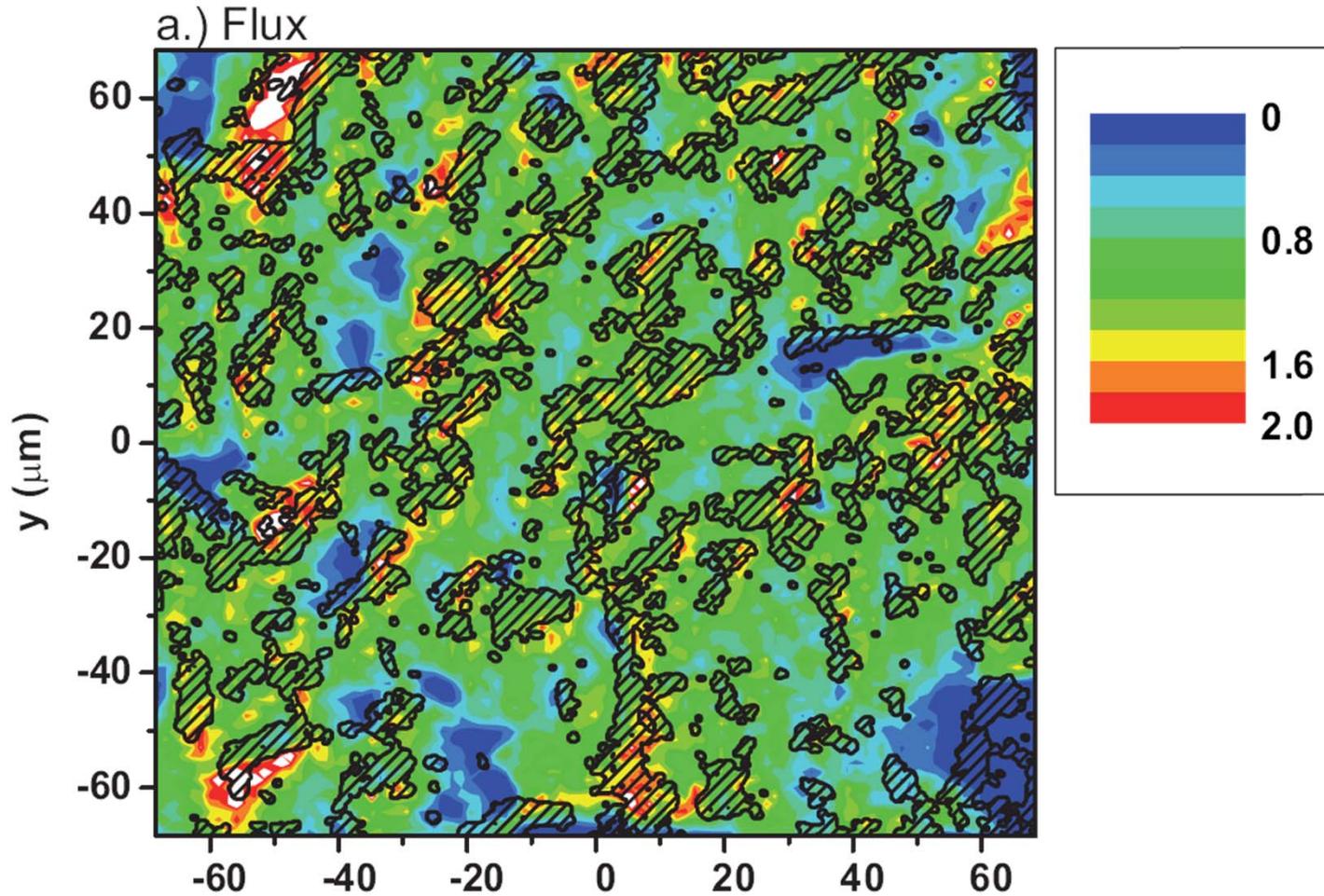
Variation of flux across rough surfaces



❖ Variation in $\vec{\Gamma} \cdot \vec{n}(x, y)$ based on σ_{nx} , σ_{ny} , σ_{nz} from gaussian error propagation:

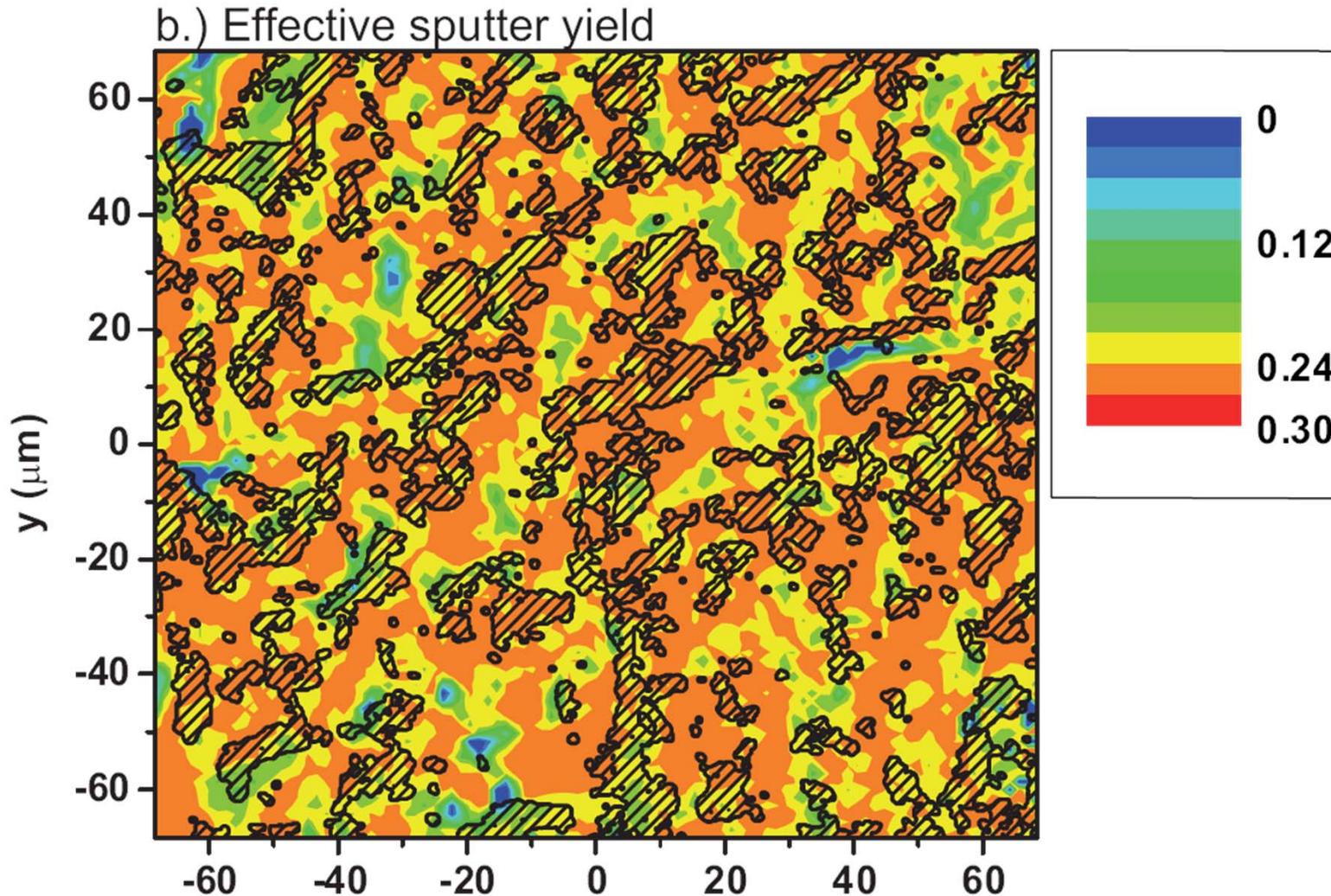


❖ Flux distribution of C^{+4} for a total influx of $1 C^{+4} (m^{-2})$

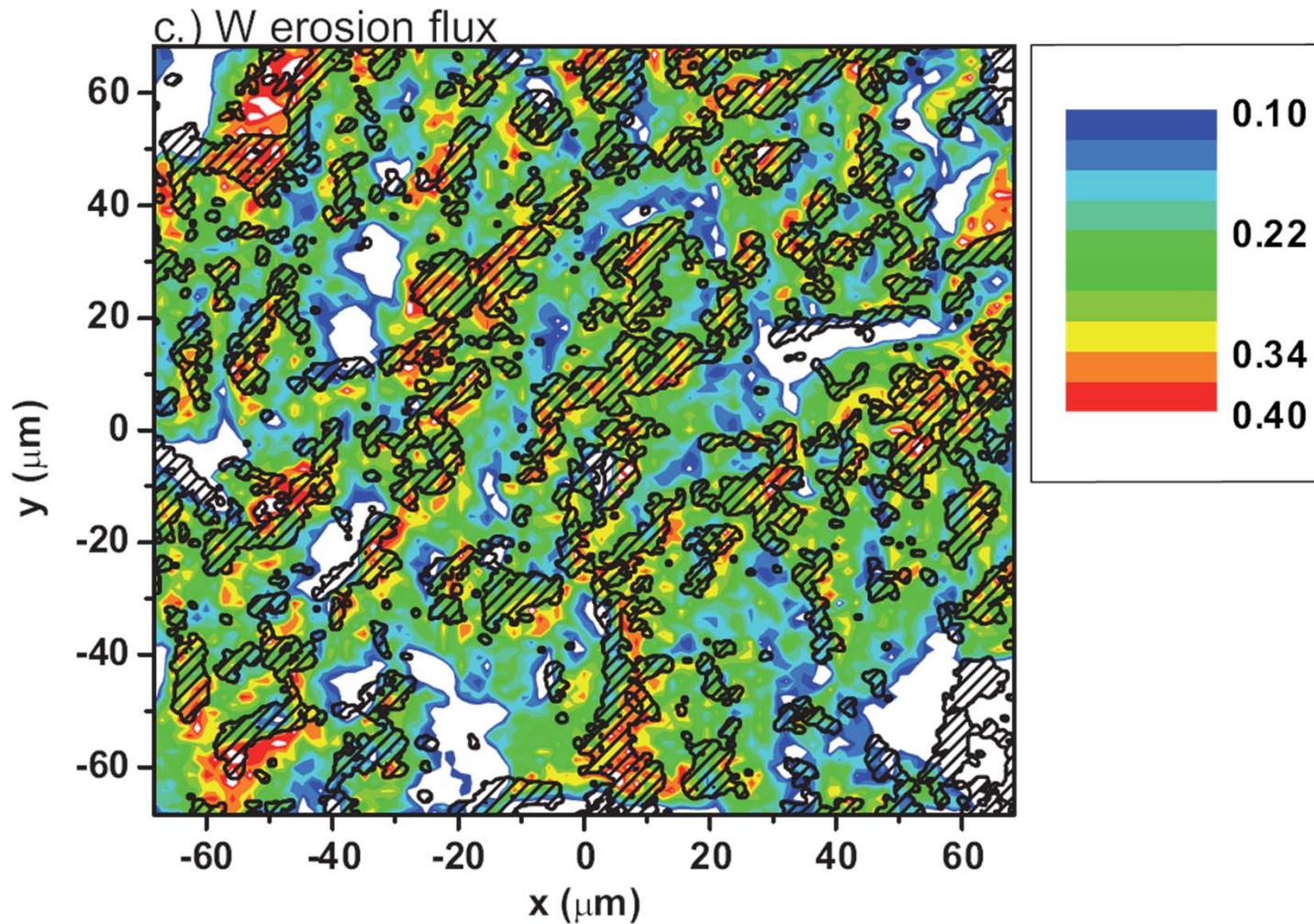


➤ Flux peaking correlated with experimentally found erosion patterns

- ❖ Effective sputter yield of W by C^{+4} using a combination of Bohdansky and Yamamura formula



❖ W erosion flux by C^{+4} for a total influx of $1 C^{+4} (m^{-2})$



➤ Areas of peak erosion fit experimentally found erosion patterns