

## Passive protection of the ITER first mirrors

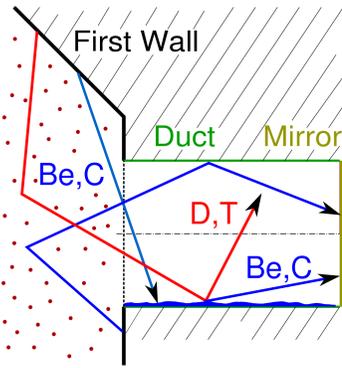
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### The issue: protection of first mirrors from deposition

- Degradation of mirrors limits the life-time and performance of ITER optical diagnostics
- Preliminary analysis [A. Litnovsky et al. NF2009], [V. Kotov et al FED2011]:  
deposition of impurities is more dangerous than sputtering

### Physical processes leading to deposition



- Recessed first wall elements: no ion fluxes
- Fluxes of neutral impurities due to:
  - Line-of-sight transport
  - Elastic collisions with ions
- Transport to the mirror:
  - Prompt deposition
  - Reflection from the duct wall
  - *Re-erosion of deposits from the duct wall*

### Engineering model: a conservative (upper) estimate

Basic assumptions:

- Uncertainties:
- Impurity reflection coefficients = ?
    - Low energies: TRIM is not valid
  - Erosion yield of deposits = ?
    - Known to be higher than for bulk
  - TRIM is used only for reflection of fast DT atoms
  - Prescribed reflection coefficient  $R_N$  for impurities
  - The whole duct wall is already covered by deposit
  - The deposit is sputtered by DT atoms
  - "Handbook" sputtering yield is multiplied by  $f_{enh}$
  - Full sticking on the mirror

$$\Gamma_{imp} = \min \left[ C_{imp} A_{imp}^1 \Gamma, \overbrace{C_{imp} A_{imp} + f_{enh} I_{imp}}^{gross\ deposition} \Gamma - f_{enh}^M E \Gamma \right]$$

$\Gamma_{imp}$  is the impurity flux density on the mirror

$\Gamma$  is the flux density of DT atoms incident to the duct entrance aperture

$C_{imp} \Gamma$  is the impurity flux density incident to the aperture

$C_{imp} A_{imp} \Gamma$  is the impurity flux calculated for given  $R_N$  w/o re-erosion from the duct wall

$C_{imp} A_{imp}^1 \Gamma$  is the impurity flux calculated for  $R_N = 1$  w/o re-erosion from the duct wall

$f_{enh} I_{imp} \Gamma$  is the impurity flux to the mirror due to re-erosion of deposit from the duct wall

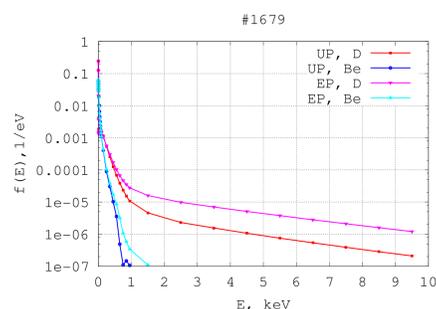
$f_{enh}^M E \Gamma$  is the sputtering rate of the deposit from the mirror itself

- The model is implemented in EIRENE: the Monte-Carlo particle transport code

### Atoms incident to the entrance aperture

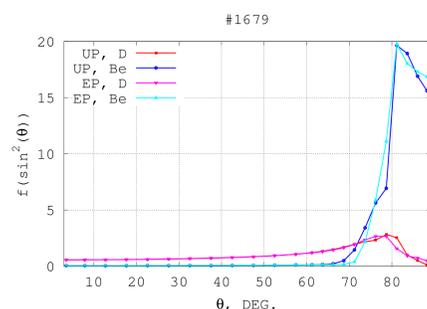
- Monte-Carlo neutral transport (EIRENE) in the main chamber with fixed plasma
- Plasma background from B2-EIRENE (scrape-off-layer) and ASTRA (core and pedestal)

Example of Energy Distribution



High Energy Tail  $\Rightarrow$   
 $\Rightarrow$  effective re-erosion is expected

Example of Angular Distribution



Grazing Incidence  $\Rightarrow$   
 $\Rightarrow$  small prompt deposition is expected

### Summary

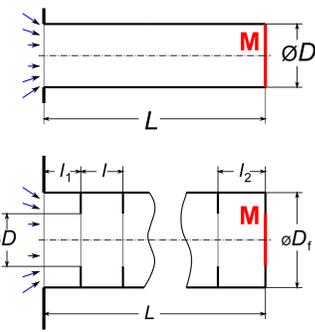
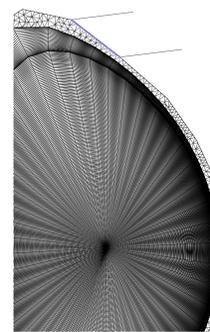
- A conservative (engineering) model of impurity deposition on the mirrors is proposed
- Attenuation of the gross deposition in the cylindrical ducts with and without baffles is analyzed

- Baffles can bring extra reduction of gross deposition by an order of magnitude *in sufficiently long ducts*
- A case study for a real geometry: core CXRS, is made
- The estimated life-time is >500 full (400 sec) discharges
- Net erosion of deposit from the mirror is not excluded but no confident prediction can be made

### To be done

- Experimental data are required to validate the incident impurity fluxes at the aperture
- Real 3D structure of the first wall has to be taken into account in the model

### Reduction of gross deposition in the ducts with and without baffles



Fe duct wall  
Mo mirror  
Be impurity

#1639, #1679

$D_f = 2D, l = D$   
 $l_1 = 0, l_2 = 2D$

Attenuation factor  $C_{imp} \Gamma / \Gamma_{imp}$  in the Equatorial Port, assumed  $C_{imp} = 10\%$

$L/D$	2	5	10	20	30	duct
$R_N = 1.0$	4.7..5.0 8.5..8.7	8.9..9.5 20..21	16..17 41..43	29..31 49..52	43..46 118..128	w/o bfl. <b>with bfl.</b>
$R_N = 0.9$	4.7..5.0 8.5..8.7	9.0..9.5 60..63	20 730..780	150..164 3600..4300	550..620 13000..16000	w/o bfl. <b>with bfl.</b>
$R_N = 0.5$	5.6..5.9 10..11	32..34 420..520	170..180 2600..3500	910..1000 11000..16000	3000..3400 27000..41000	w/o bfl. <b>with bfl.</b>
$R_N = 0.1$	39..42 55..62	230..250 800..1400	1100..1200 3800..6300	5300..6000 15000..26000	16000..18000 32000..59000	w/o bfl. <b>with bfl.</b>
$R_N = 0.1$	10 17..18	56..58 570..800	280..290 3000..4500	1400..1500 13000..20000	4500..5000 29000..48000	w/o bfl. <b>with bfl.</b>

Significant extra reduction of depositions with baffles if  $L/D \geq 10$  and  $R_N < 1$

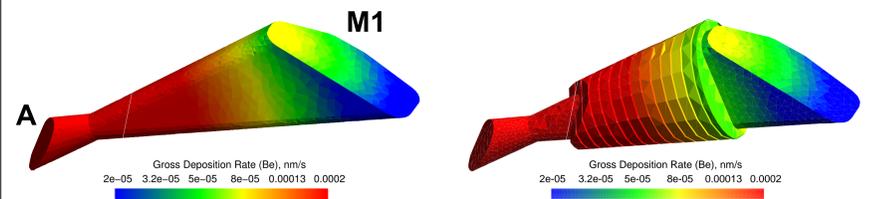
Main action of baffles - reduction of the re-erosion of deposit

E.g. a hypothetical extreme case  $\Gamma = 1e21 \text{ m}^{-3}/\text{s}$ ,  $C_{imp} = 10\%$  (1.6 nm/s).

$\Rightarrow$  Attenuation factor = 13000  $\Rightarrow$  20 nm is deposited after 400 shots.

### A case study: core CXRS diagnostic

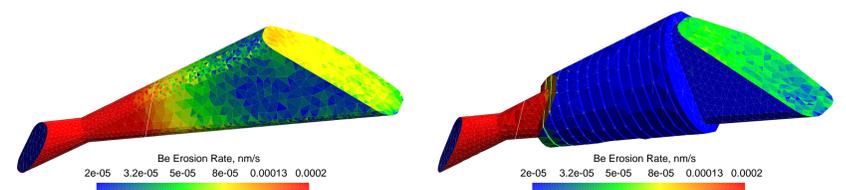
Example for  $R_N = 0.9$ ,  $f_{enh} = 10$  (attenuation factor  $\approx 50$ )



Estimated life-time (in 400 sec shots) in respect to Be deposition,  
 $\Gamma = 0.8e19 \text{ m}^{-3}/\text{s}$ ,  $C_{Be} = 0.3\%$  (0.004 nm/s), incident spectra of #1679,  
max tolerable thickness of deposit is 20 nm

$R_N$	0.9			0.5			0.1		
$f_{enh}$	1	5	10	1	5	10	1	5	10
W/o baffles	586	586	586	587	587	587	696	586	586
( $\sigma$ , %)	(2.9)	(2.9)	(2.9)	(2.9)	(2.9)	(2.9)	(23)	(2.9)	(2.9)
With baffles	618	618	618	1100	630	630	1900	630	630
( $\sigma$ , %)	(4.9)	(4.9)	(4.9)	(7.2)	(1.0)	(1.0)	(11)	(1.0)	(1.0)

Marginal effect of baffles in this case. The reason:  
no reduction of re-erosion from the front part



- Net-erosion conditions on the mirror are not excluded
- BUT the sign of the net deposition is sensitive in respect to  $R_N$ ,  $f_{enh}$ ,  $C_{imp}$
- The life-time estimate in respect to Mo erosion is >70000 shots (1  $\mu\text{m}$  is eroded)