

# Hydrogen in Tungsten as Plasma-facing Material

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## Introduction:

- H in W: Thermodynamic parameters

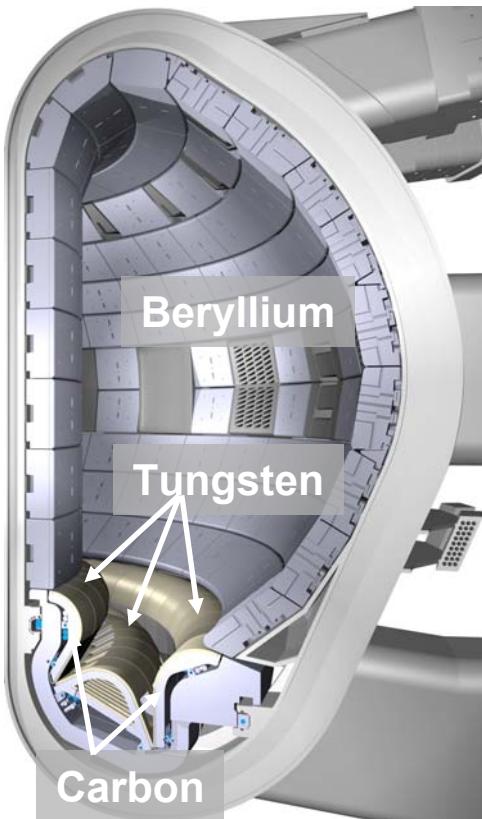
## Retention due to traps:

- Intrinsic traps: dependence on W structure
- Trap formation: due to low energy hydrogen ions  
hydrogen and helium ions  
due to neutrons

## Consequences:

- for inventory in ITER
- for the use of W in DEMO

## Initial ITER materials

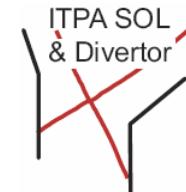


## Present strategy for ITER operation

- change to a **full W-divertor before DT**
- change to **all-W** as future DEMO relevant choice after extensive operation with Be wall

## Predicted edge plasma conditions

- Wall:  $800 \text{ m}^2$ ,  $\sim 1 \times 10^{21} / \text{m}^2\text{s}$   
surface temperature: **450 K**
- Divertor:  $<10 \text{ m}^2$ ,  $\sim 1 \times 10^{24} / \text{m}^2\text{s}$   
surface temperature: **1000 K**

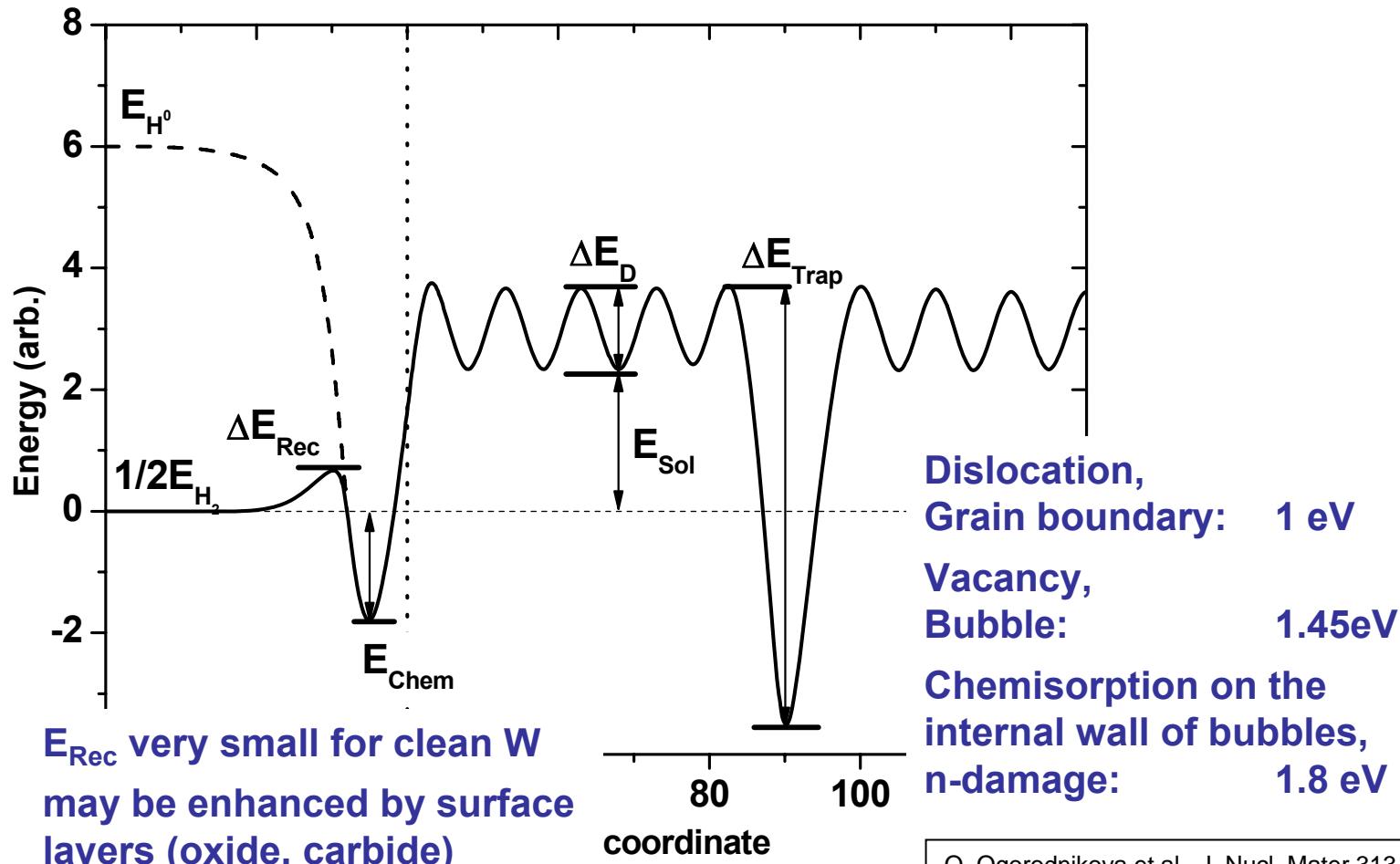


## Tritium inventory as safety concern

- present administration limit  
**700 g mobilisable tritium**

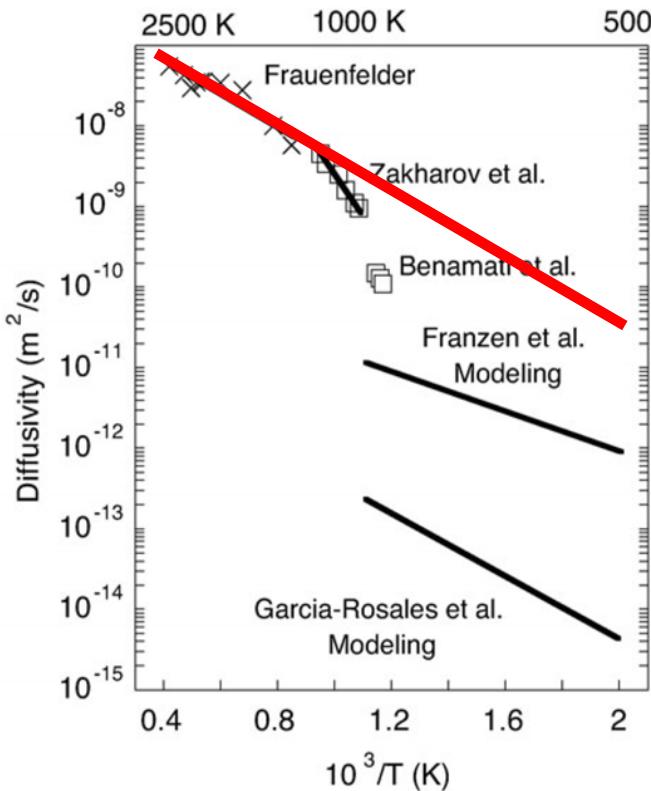
# Hydrogen in W: Thermodynamic parameters

## Recombination   Diffusion   Trapping

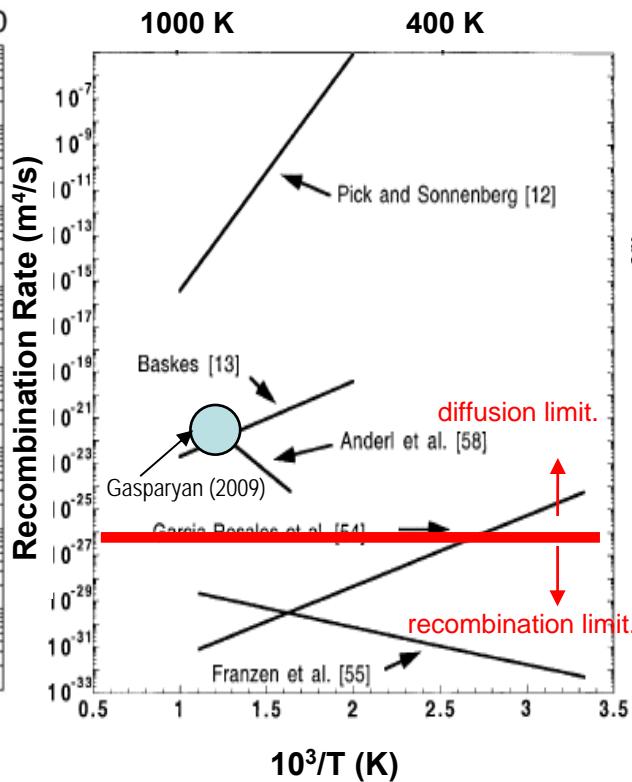


# Hydrogen in W: Thermodynamic parameters

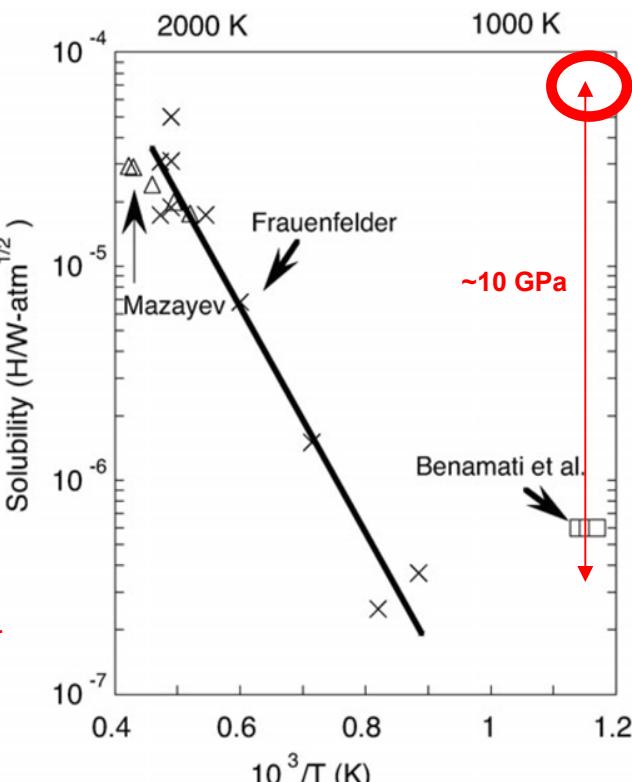
## Diffusion coefficient:



## Recombination rate coefficient:



## Solubility:



- Best values by Frauenfelder
- Lower values “effective” diffusion coefficients

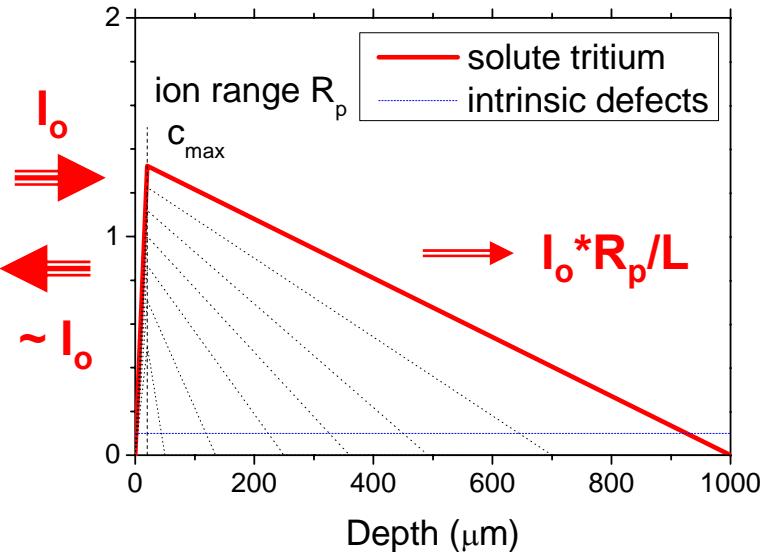
- Large scatter due to surface conditions
- Values above  $10^{-26} \text{ m}^4/\text{s}$  equivalent to diffusion limitation

- Very low solubility
- Values reached during implantation are equivalent to pressures of GPa

# Hydrogen retention in W:

## Schematics of retention in W:

- Example: 38-200eV D<sup>+</sup>, 10<sup>21</sup> D/m<sup>2</sup>s, 500 K  
no kinetic vacancy formation



From diffusion limited flux balance:

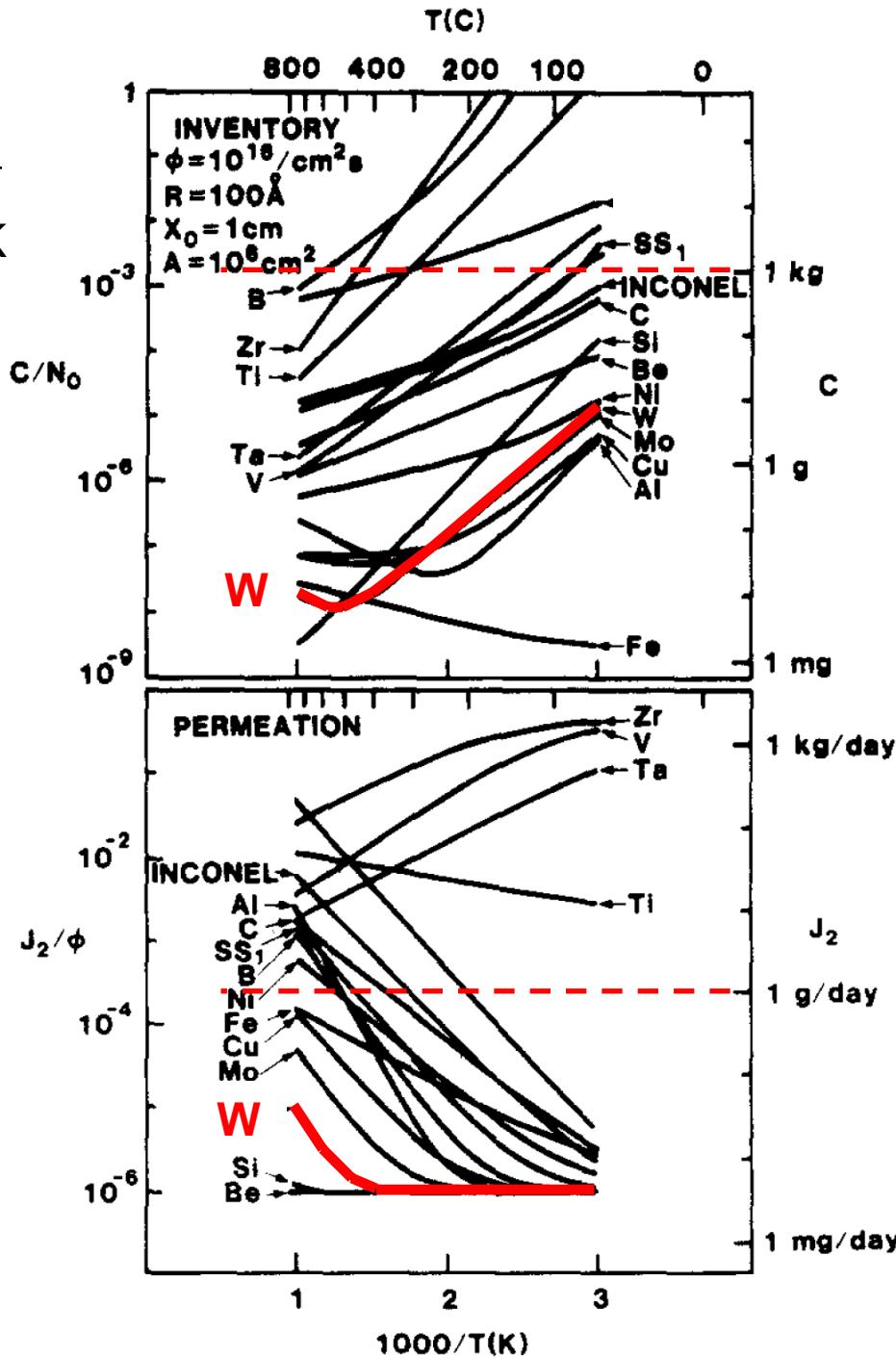
$$I_o = D * C_{\max} / R_p$$

Typical ITER wall values:

$$R_p = 10 \text{ nm}, I_o = 10^{21} / \text{m}^2 \text{s}, D = 3 * 10^{-11} \text{ m}^2 / \text{s}$$

$$C_{\max} = 10^{-5}$$

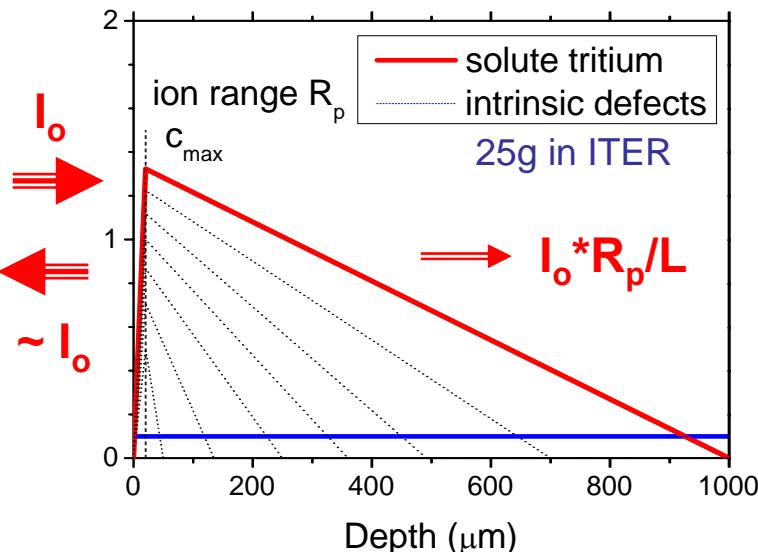
B. Doyle, D. Brice, J. Nucl. Mater (1984)



# Hydrogen retention in W: Schematic mechanisms

## Schematics of retention in W:

- Example: 38-200eV D<sup>+</sup>, 10<sup>21</sup> D/m<sup>2</sup>s, 500 K  
no kinetic vacancy formation



From diffusion limited flux balance:

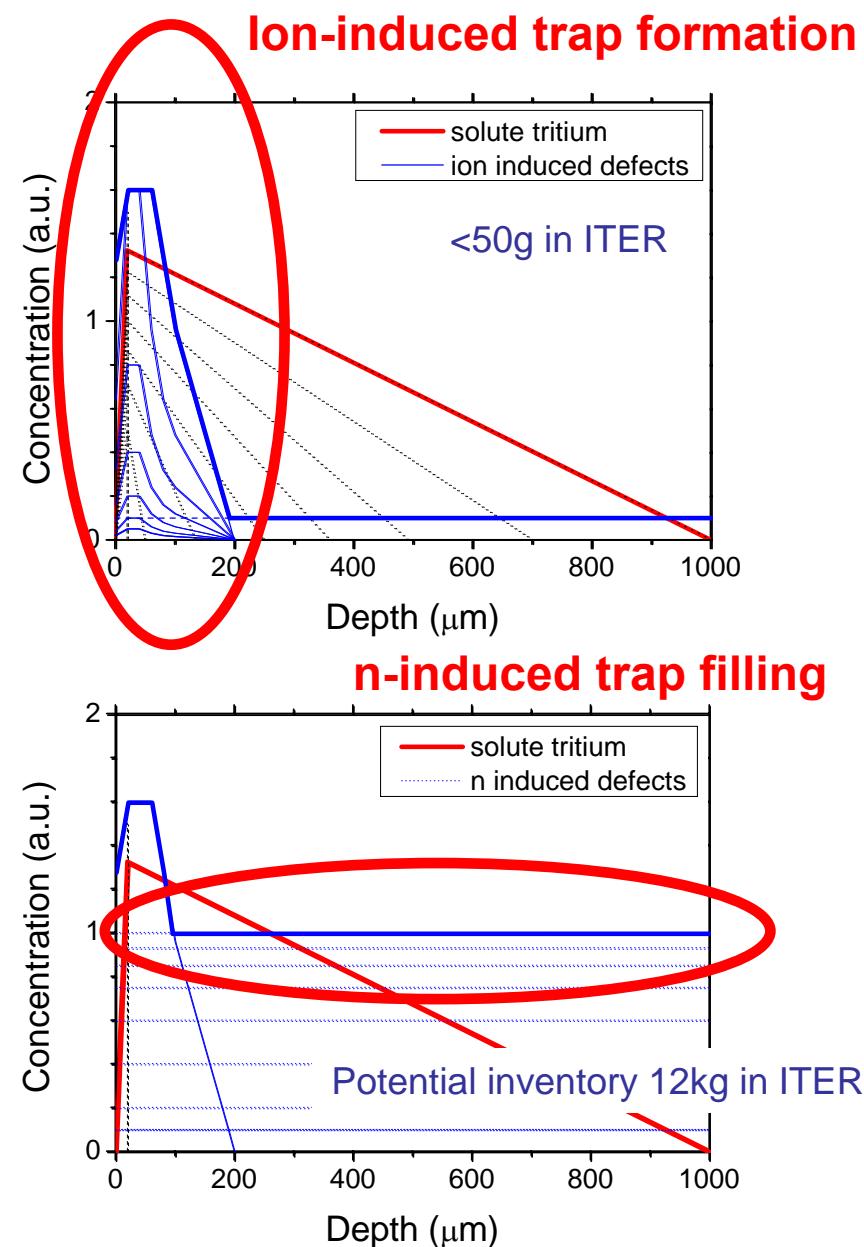
$$I_o = D * c_{\max} / R_p$$

At the vessel wall typical values are

$R_p = 10 \text{ nm}$ ,  $I_o = 10^{21} / \text{m}^2\text{s}$ ,  $D = 3 * 10^{-11} \text{ m}^2/\text{s}$

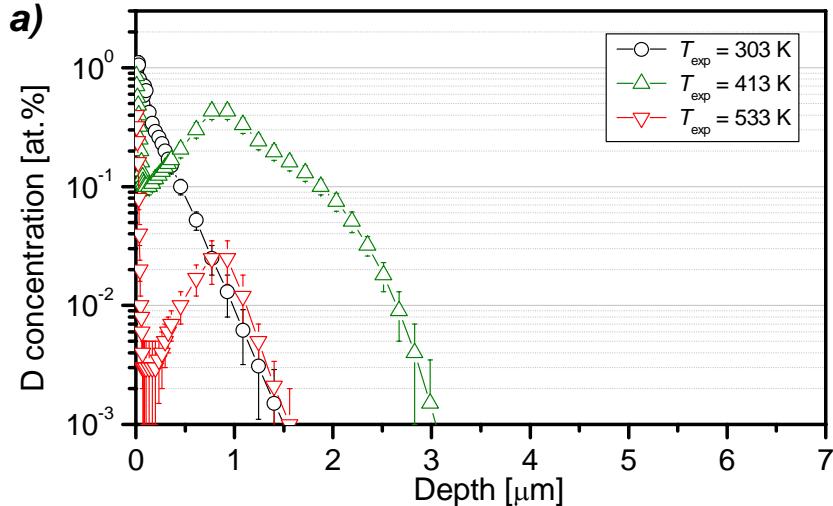
$$c_{\max} = 10^{-5}$$

B. Doyle, D. Brice, J. Nucl. Mater (1984)



# Intrinsic traps: dependence on W micro-structure

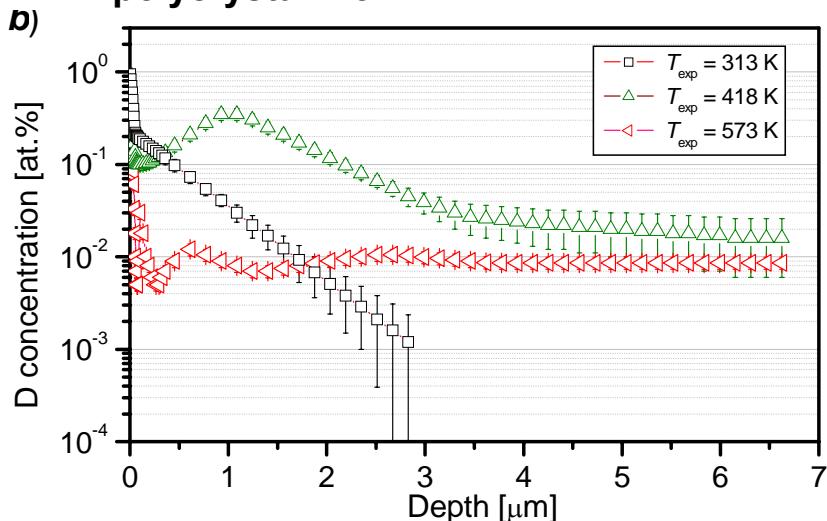
W single crystal



- Bulk trap density below detection limit in single crystalline W
- Bulk trap density about 10<sup>-2</sup> % in polycrystalline W (re-crystallized)
- Ion-induced damage at similar level

V.Kh. Alimov, J. Roth, M. Mayer, JNM 337–339 (2005) 619

polycrystalline W



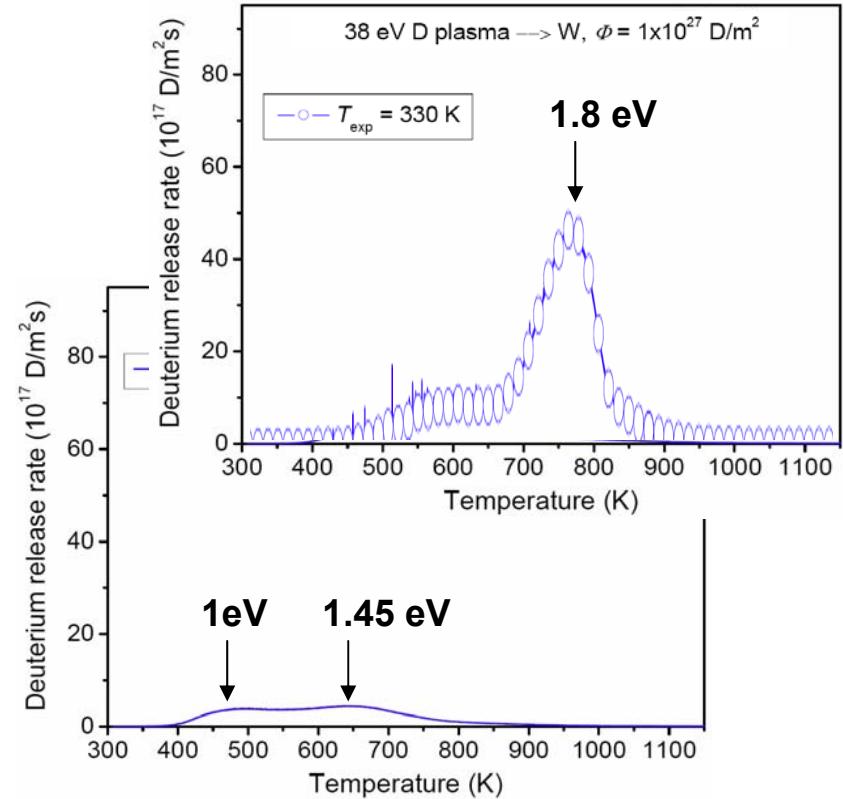
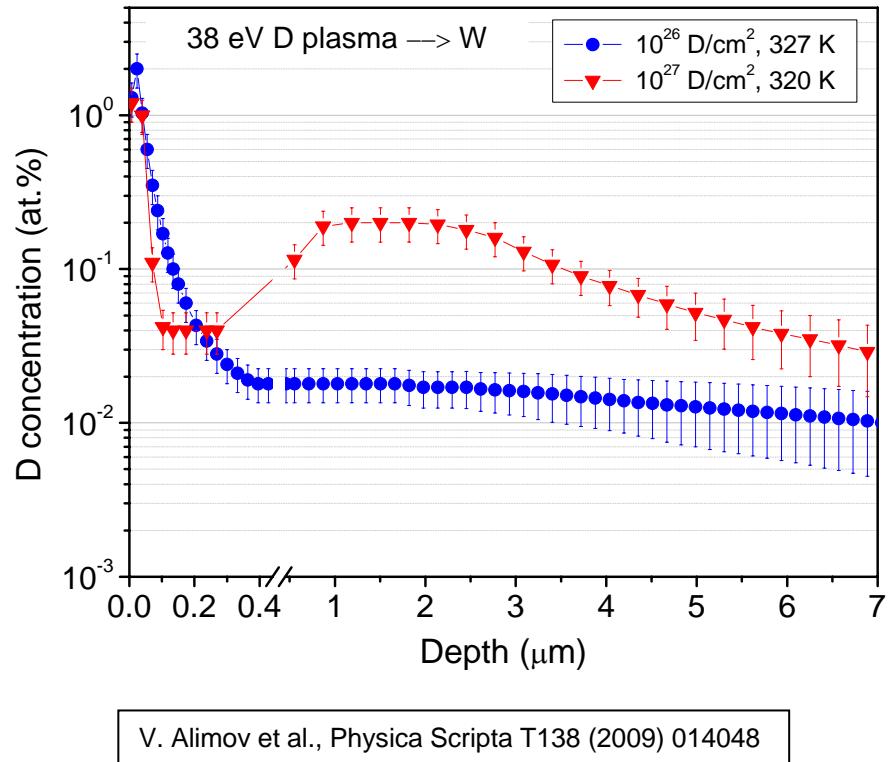
- pores in W/Re alloys and VPS coatings provide additional trapping sites
- At high fluences ion-induced traps dominate

A.V. Golubeva, et al., JNM 363–365 (2007) 893

# Trap formation: due to low energy ions

## Evidence:

- Depth profile of retained D
- Formation of strong traps from TDS



Modelling must assume damage production far beyond the ion range  
with activation energy around 1.8 eV: micro-bubbles ?

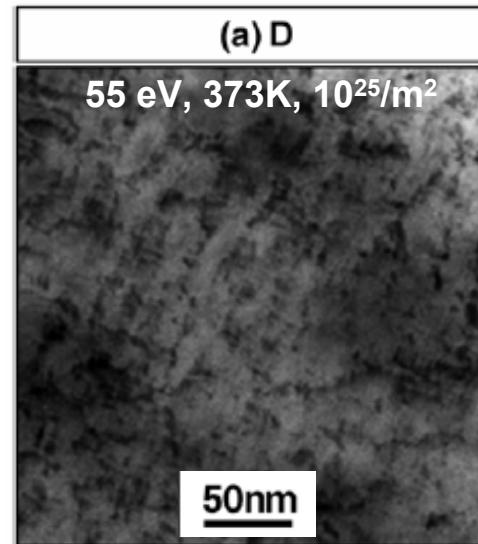
# Trap formation: due to low energy hydrogen ions

## Evidence:

- Direct sub-surface damage observation:

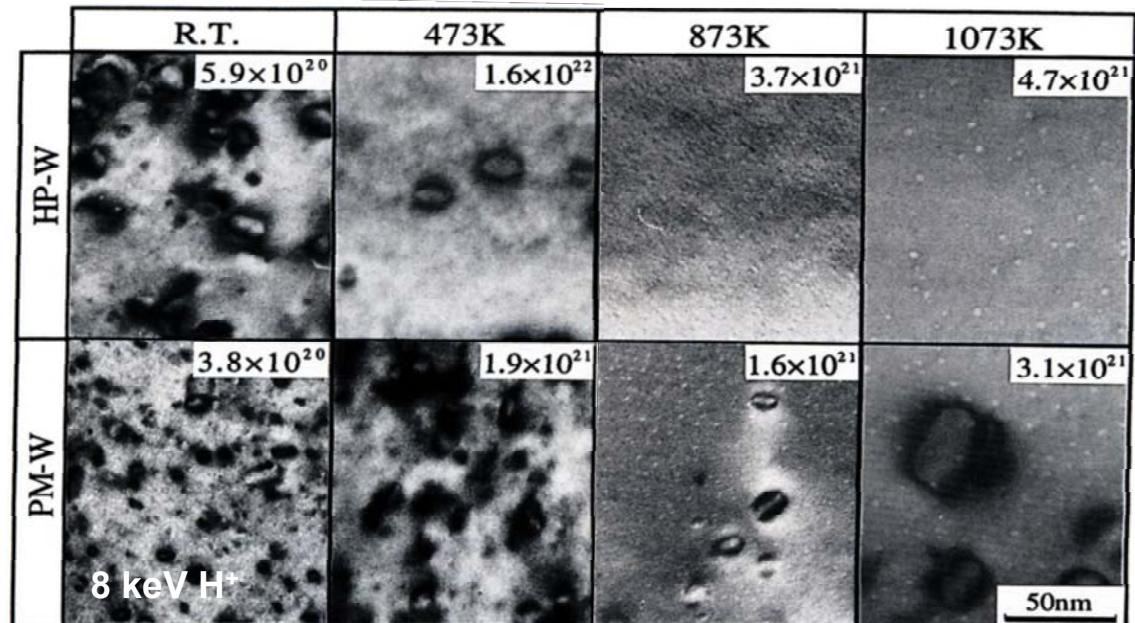
High resolution TEM showing intense strain fields, no voids

M. Miyamoto et al., Nucl. Fusion 49 (2009) 065035



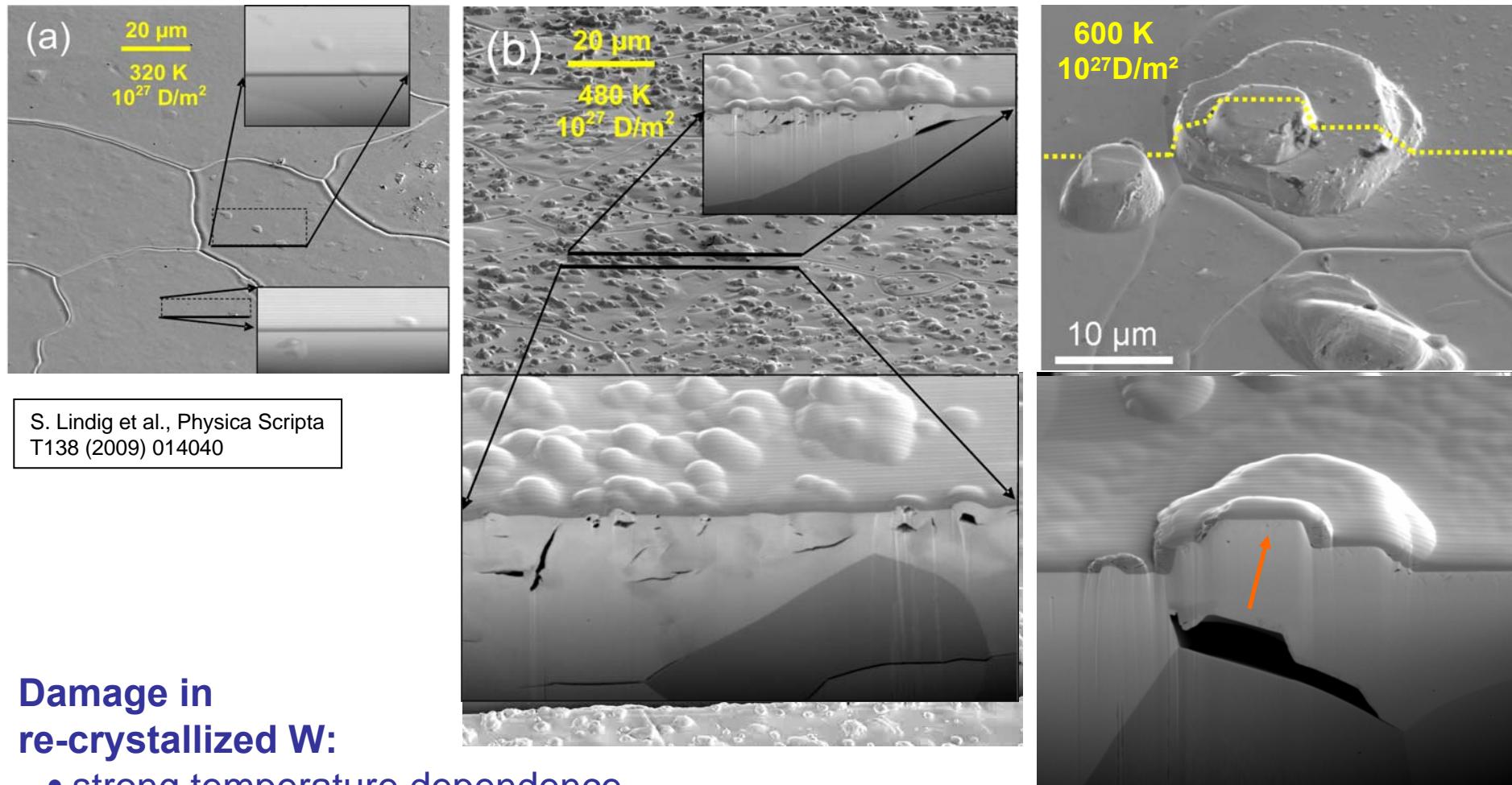
High resolution TEM showing transition from dislocation loops to bubbles <2nm with increasing implantation temperature

R. Sakamoto et al. JNM 220-222 (1995) 819



# Trap formation: due to low energy ions, high fluence

Ion beam cross-sectioning in SEM



## Damage in re-crystallized W:

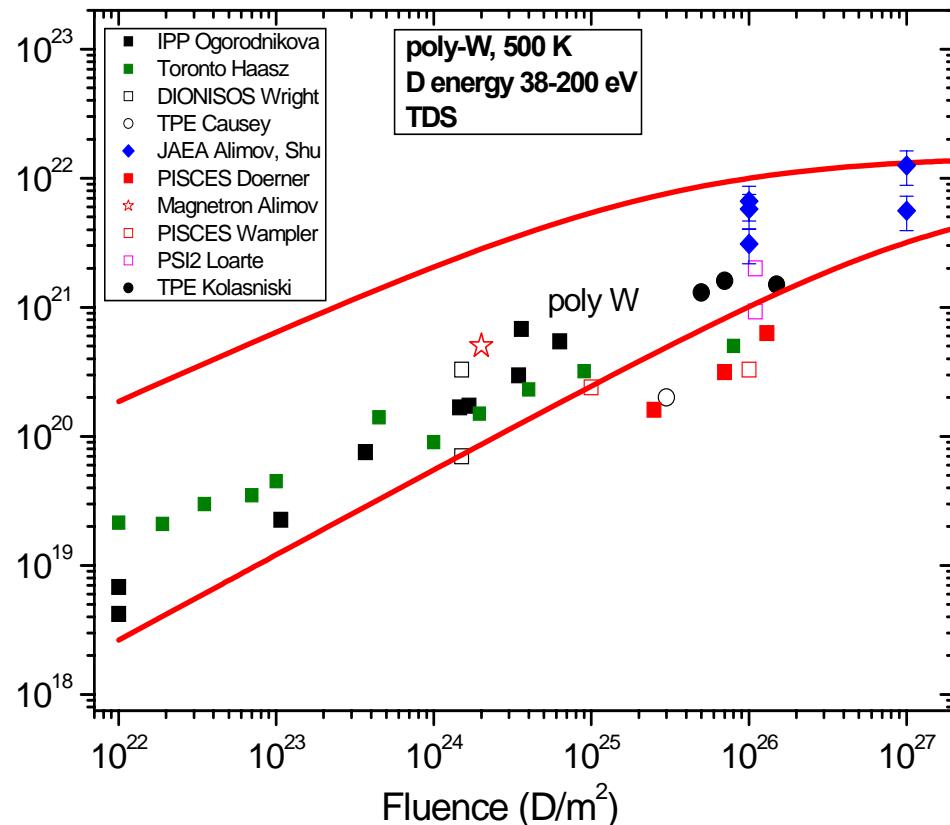
- strong temperature dependence
- brittle to ductile transition (BDT) from cracks to cavities at around 500 K
- cavity formation at grain boundaries and material transport to the surface above BDT
- material moving from grain boundary to surface in sliding plane system  $\{110\} <111>$

## D retention in W: Fluence dependence up to $10^{27}/\text{m}^2$

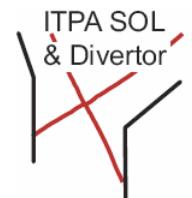
# Consequence:

# Fluence dependence of retention

- Large margins of uncertainty were assumed by the ITPA SOL/DIV for extrapolation
  - Saturation at high fluences due to formation of cracks and pores. Still within uncertainty of data!

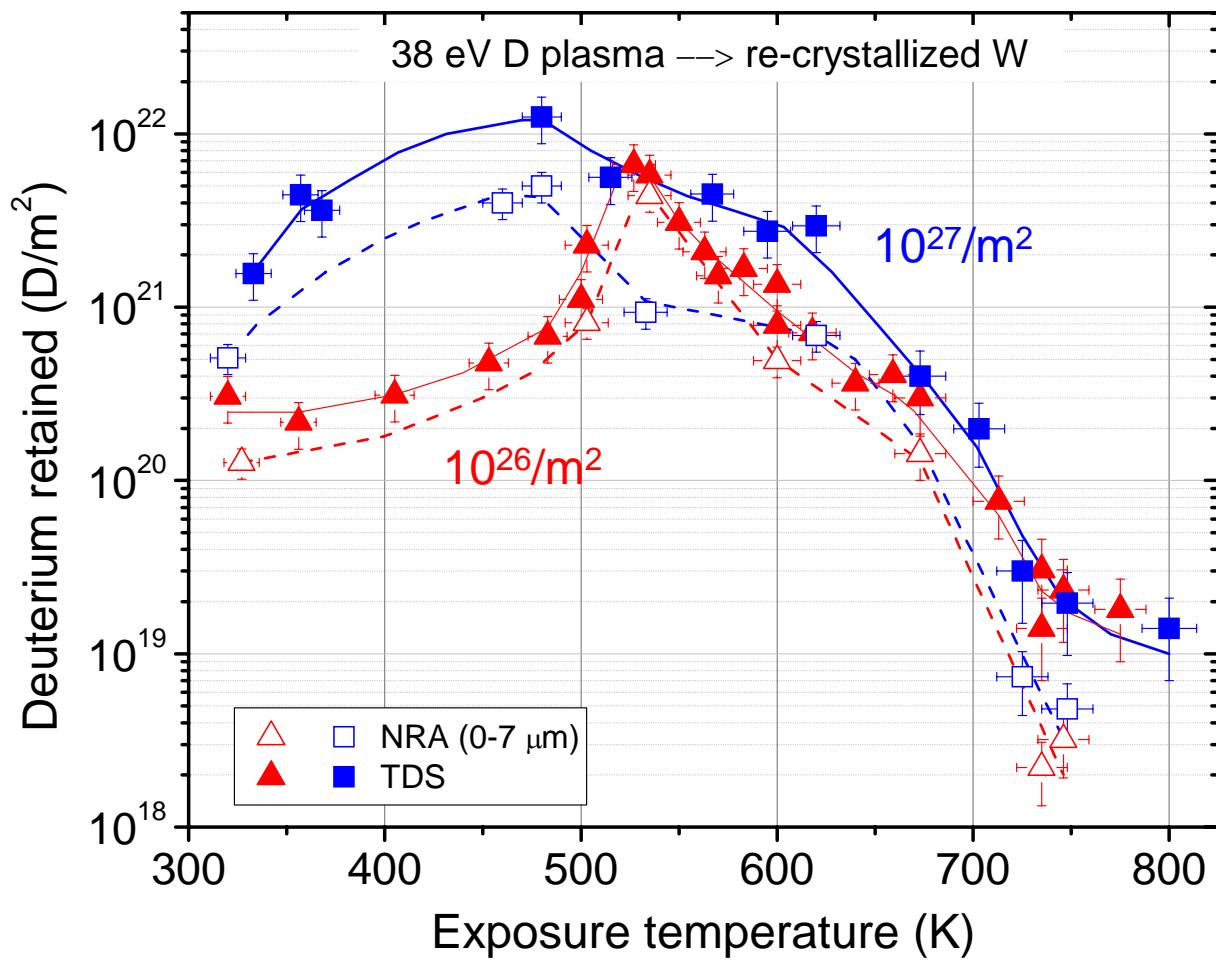


J. Roth et al., IAEA Geneva, IT/P6-16 (2008)  
 B. Lipschultz, J. Roth, et al., MIT Rep. PSFC/RR-10-4 (2010)



# D retention in W: Temperature dependence

## Consequence:



Maximum retention near 500 K saturates at about  $10^{22}/m^2$ .

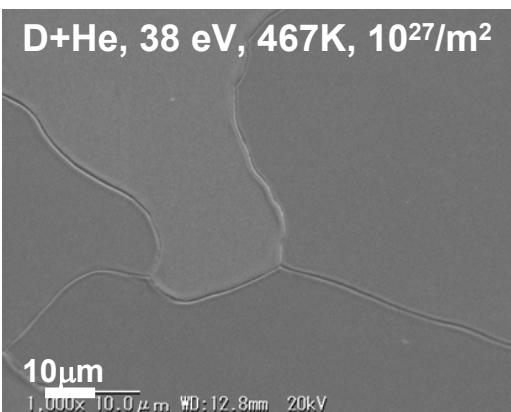
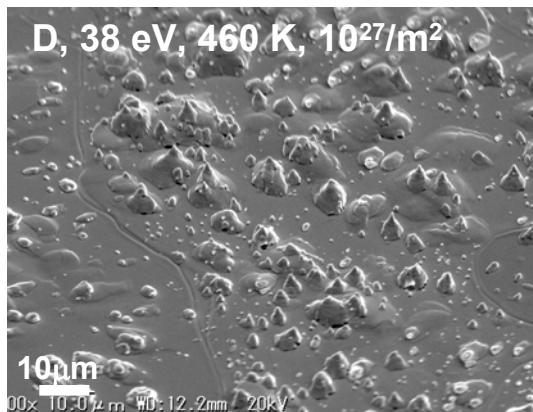
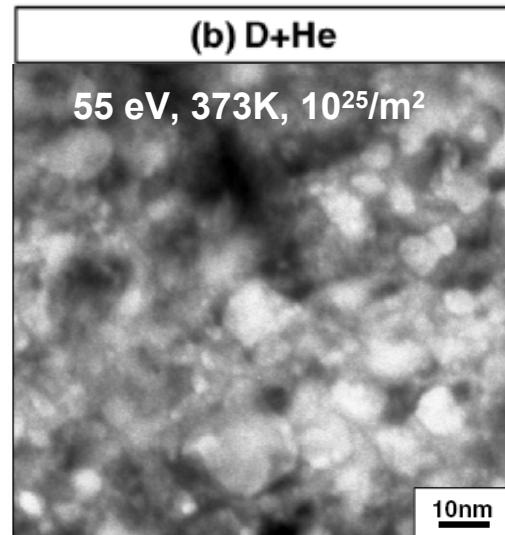
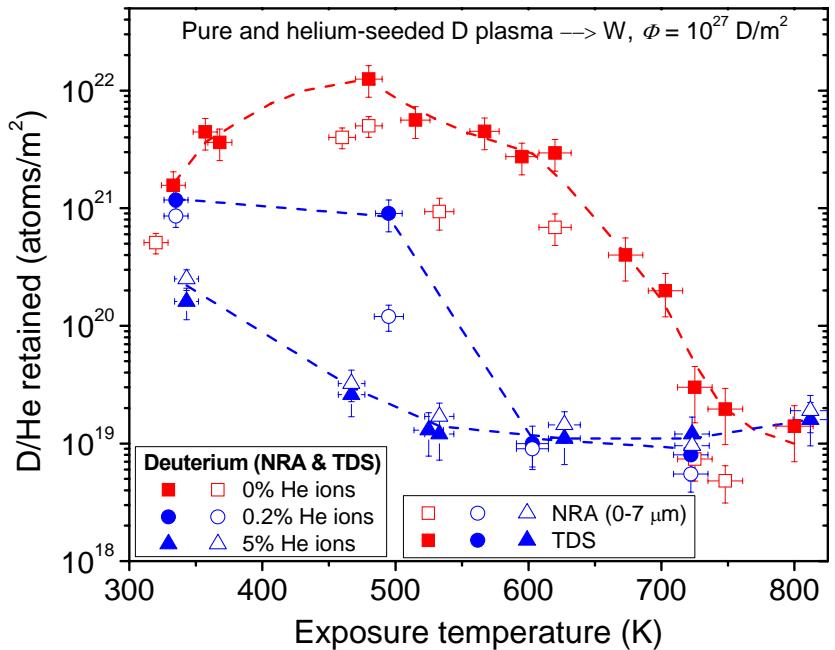
Low retention below 500 K increases with fluence.

Difference between TDS and NRA (1 to 7  $\mu m$ ) indicates deep penetration and trapping.

V. Kh. Alimov et al, JNM in press,  
doi: 10.1016/j.jnucmat.2011.01.088

# D retention in W: Simultaneous D and He irradiation

M. Miyamoto et al., Nucl. Fusion 49 (2009) 065035



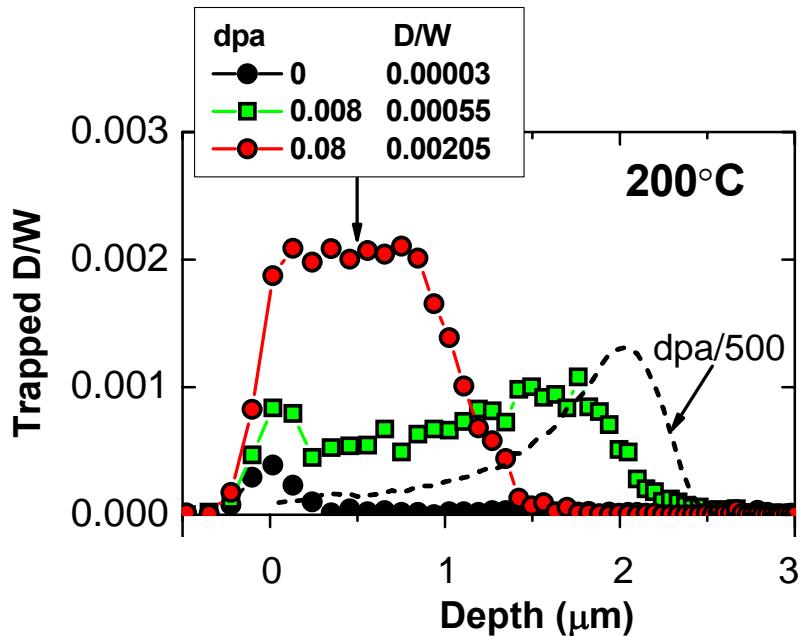
Helium bubbles prevent the penetration and provide outward pathways for D.

V. Kh. Alimov, J. Roth, et al. Phys. Scr. 2009 014048

# Trap formation: due to neutrons

## Damage simulation:

n-damage simulated by energetic ion bombardment: H, C, Si, W  
Heavy ion damage cascade most similar to neutrons



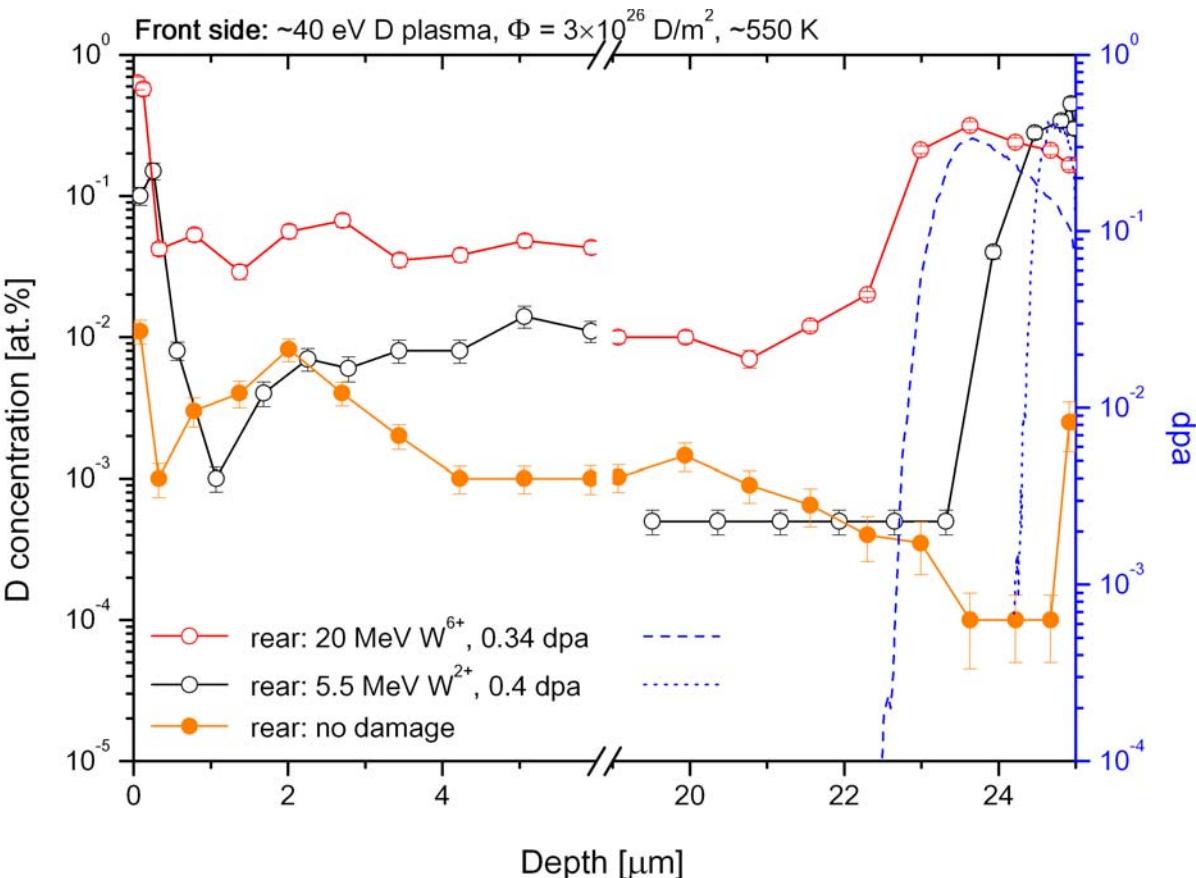
- 12 MeV Si, subsequent D plasma in PISCES ( $10^{26} (\text{D+5\%He})/\text{m}^2$ , 100 eV)
- At 200°C D trapping is limited by slow kinetics, ie. permeation.
- Sequential trap filling allows the determination of permeation kinetics.

W.R.. Wampler, R. Doerner, Nucl. Fusion 49 (2009) 115023

# Trap formation: due to neutrons

## Damage simulation:

- Retention in 25  $\mu\text{m}$  W foil
- Irradiation damage at rear surface: 5.5 and 20 MeV W-
- Plasma exposure at front side: 40 eV D<sup>+</sup>,  $3 \times 10^{26} \text{ D/m}^2$

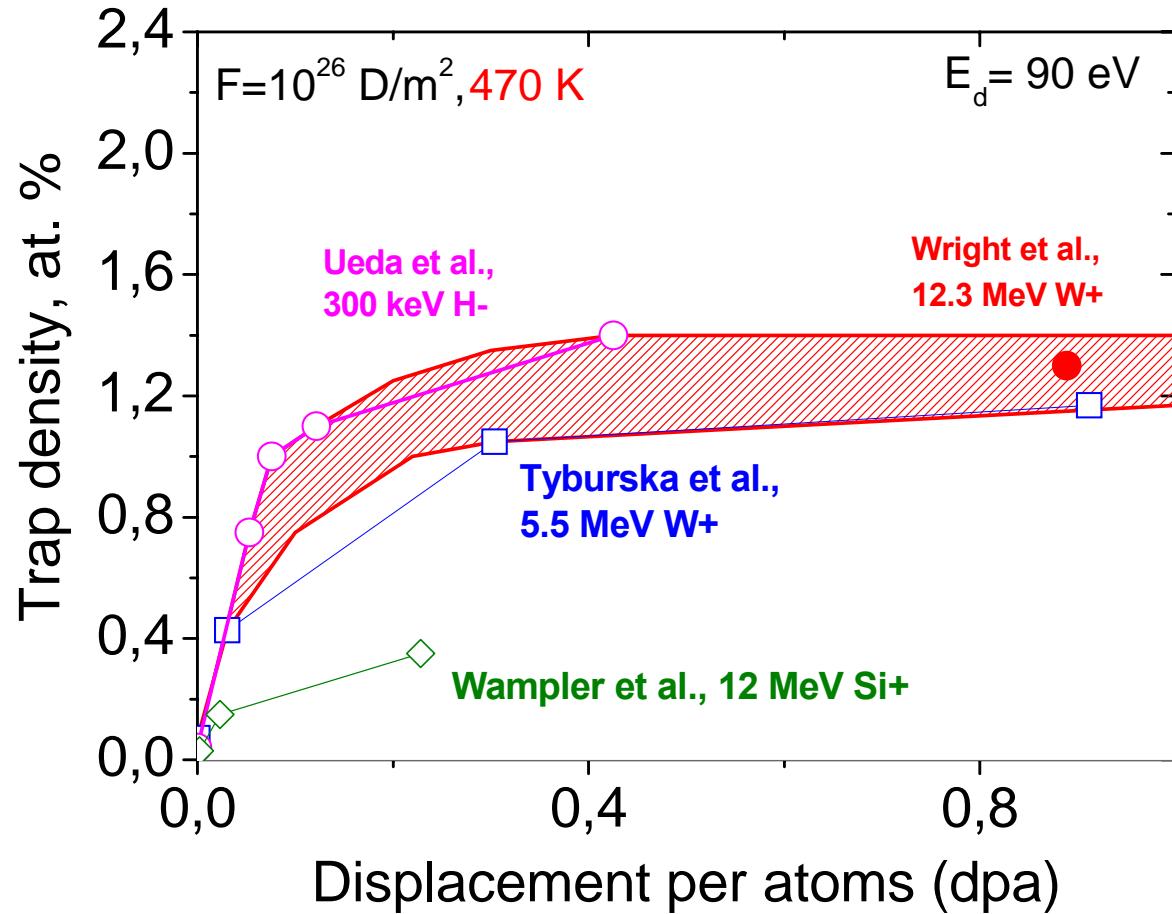


- D permeation and retention in damage on the rear side
- D retention in the plasma side is enhanced by damage on the rear side

B. Tyburska et al., J. Nucl. Mater. 395 (2009) 150

# Trap formation: due to neutrons

## Damage simulation:



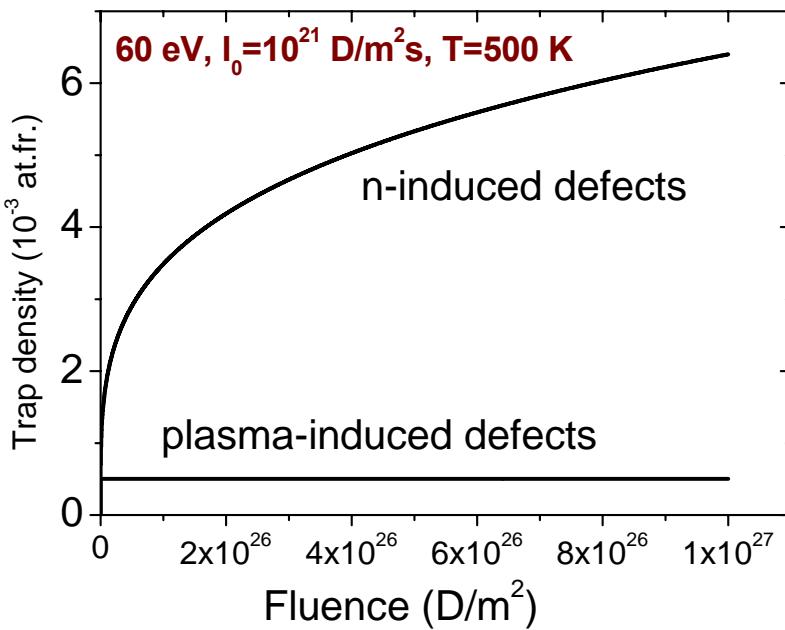
- Radiation induced trap density saturates at 1.2% above 0.4 dpa
- These data provide valuable input for modelling

B. Tyburska et al., J. Nucl. Mater. 395 (2009) 150

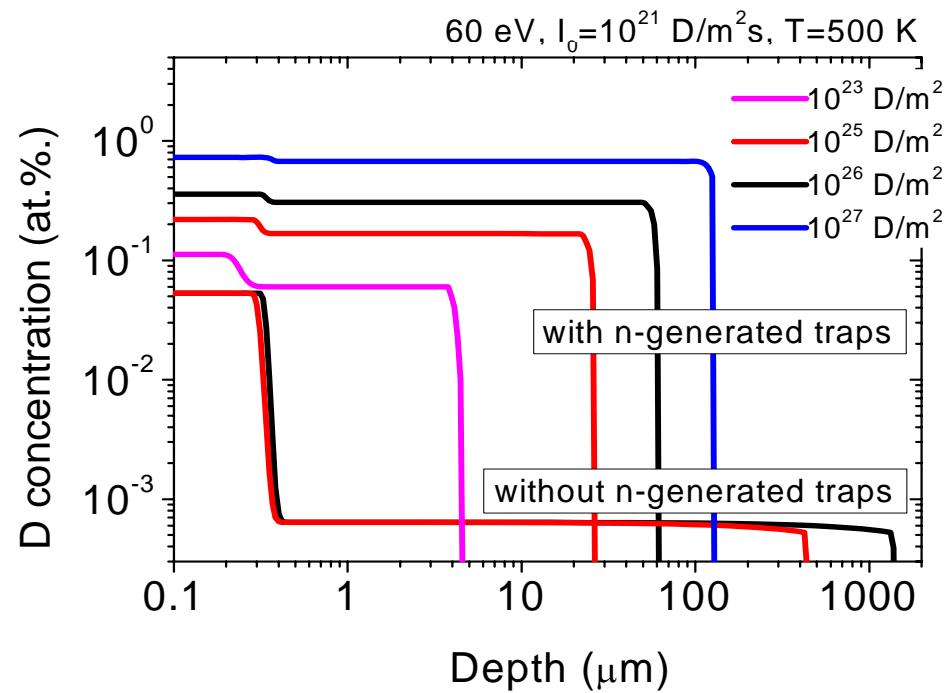
# Trap filling of neutron damage

## Modelling of ITER wall conditions:

- Damage evolution:  
 $10^{-7}$  dpa/s from IO  
saturation trap density 1%

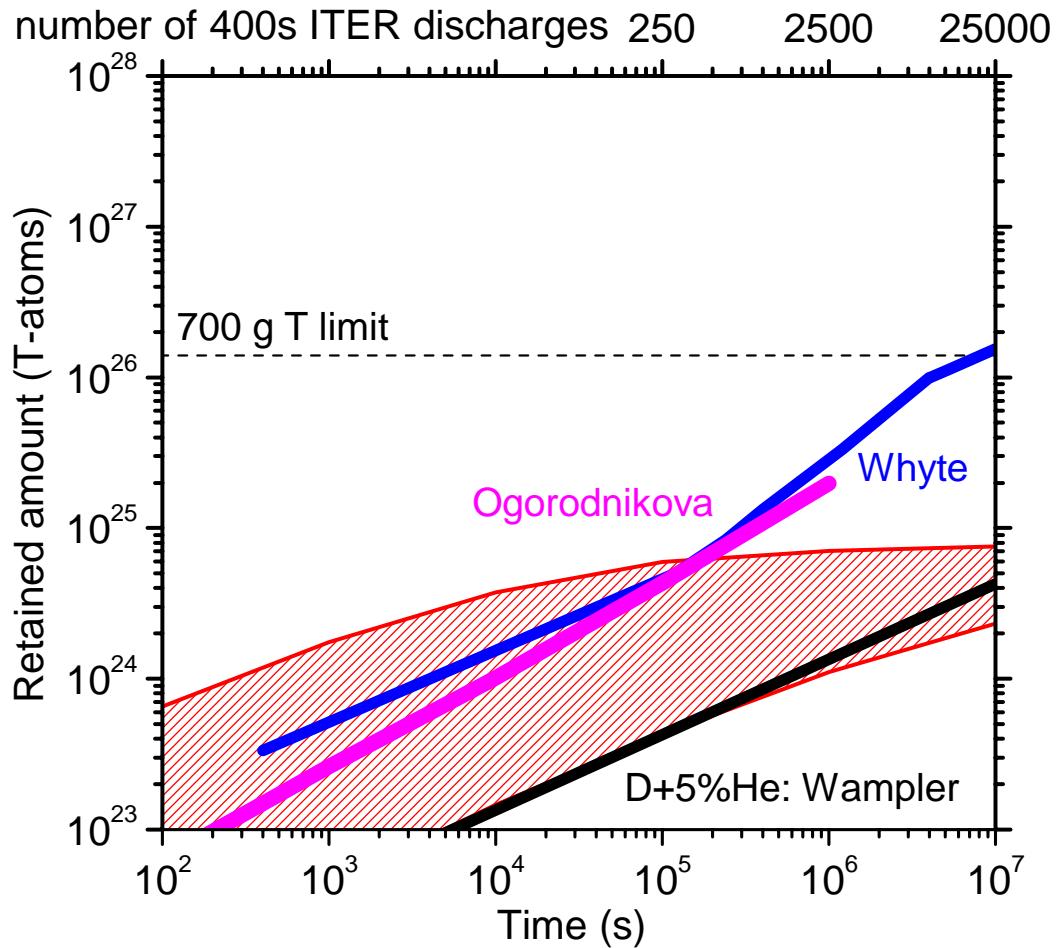


- Diffusion and trap filling:  
Diffusive trap filling modelled using established diffusion coefficient



- Filling of  $100\mu m$  W armour in about  $10^6$ s,  
 $\Rightarrow 1mm$  in 3 years steady state operation
- Relevant to DEMO rather than ITER

# Consequences for inventory in ITER



- Without additional irradiation damage the tritium limit in an all-W ITER will remain tolerable
- n-irradiation damage has the potential to enhance the inventory up to the tritium limit

O. Ogorodnikova et al., J. Nucl. Mater. (2011) in press

# Consequences

for the use of W in ITER:

**Data base** of transport coefficients is **sufficient** for predicting retention in W for ITER.

**T inventory in W will not be a challenge** within ITER lifetime

**Inventory in n-defects contributes only at the end of ITER lifetime.** n-induced defect production rate is low, trap filling is diffusion limited and will take many years

**High flux low energy ion bombardment** leads to stress fields due to over-saturation which **can produce cracks and further trap sites.**



**Test structural stability** of W under hydrogen irradiation and **transient heat loads** (PISCES, AUG, JET)

# Consequences

for the use of W in DEMO:

**Steady-state operation** will result in flux and fluence levels far exceeding those in present devices leading internal stress fields and damage.

**Higher wall temperatures ( $\leq 600^{\circ}\text{C}$ )** will reduce total retention but increase **permeation** to the cooling structure interface.

**Brittleness of pure W** will be enhanced by n-irradiation

- **Higher ductility W alloys** with acceptable PWI properties, such as low erosion and T inventory
- **Study effects of permeation** to the coolant interfaces of components in realistic conditions with large temperature and stress gradients