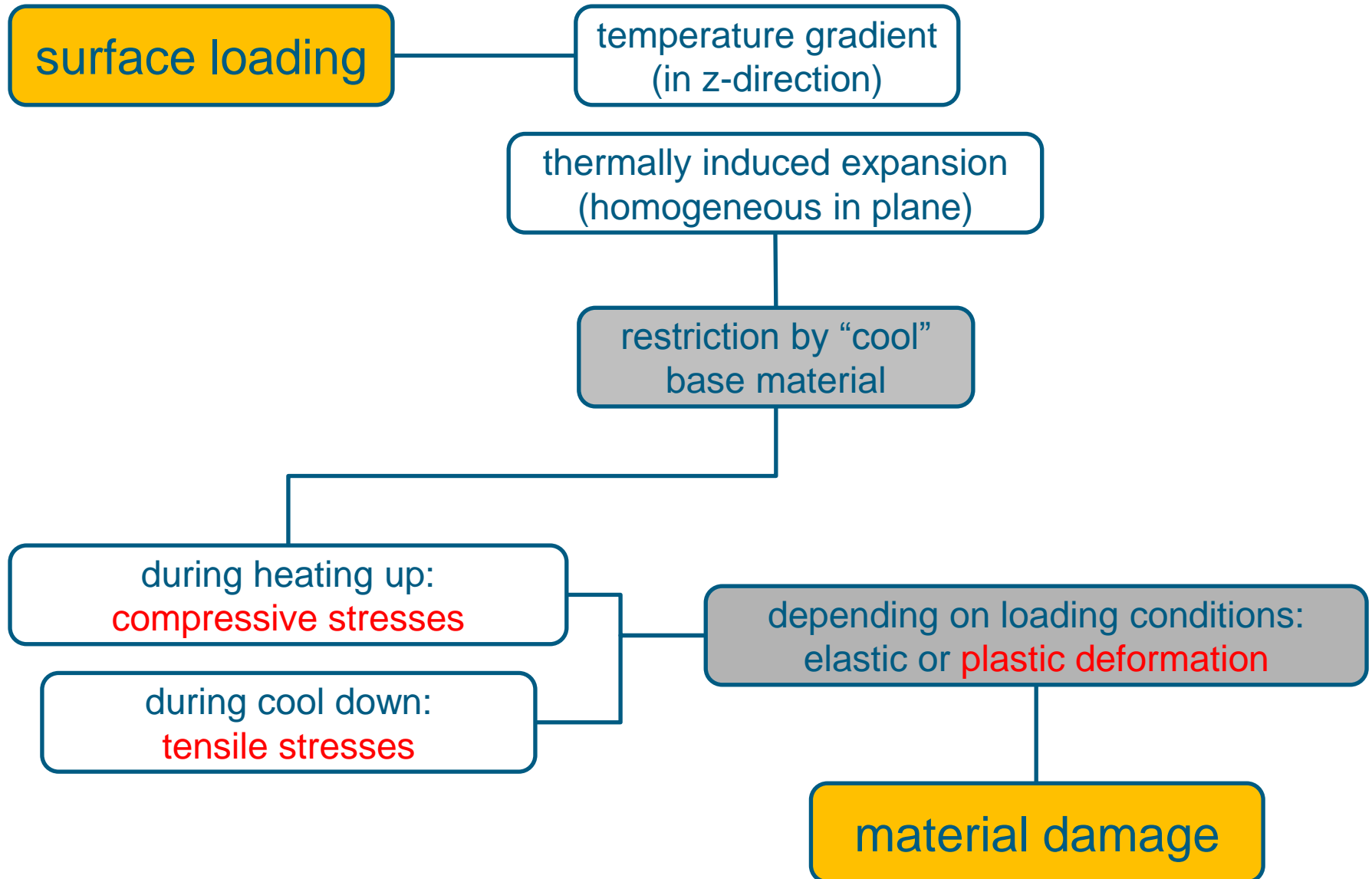


Thermal shock response of fine and ultra fine grained tungsten based materials

G. Pintsuk¹, H. Kurishita², J. Linke¹

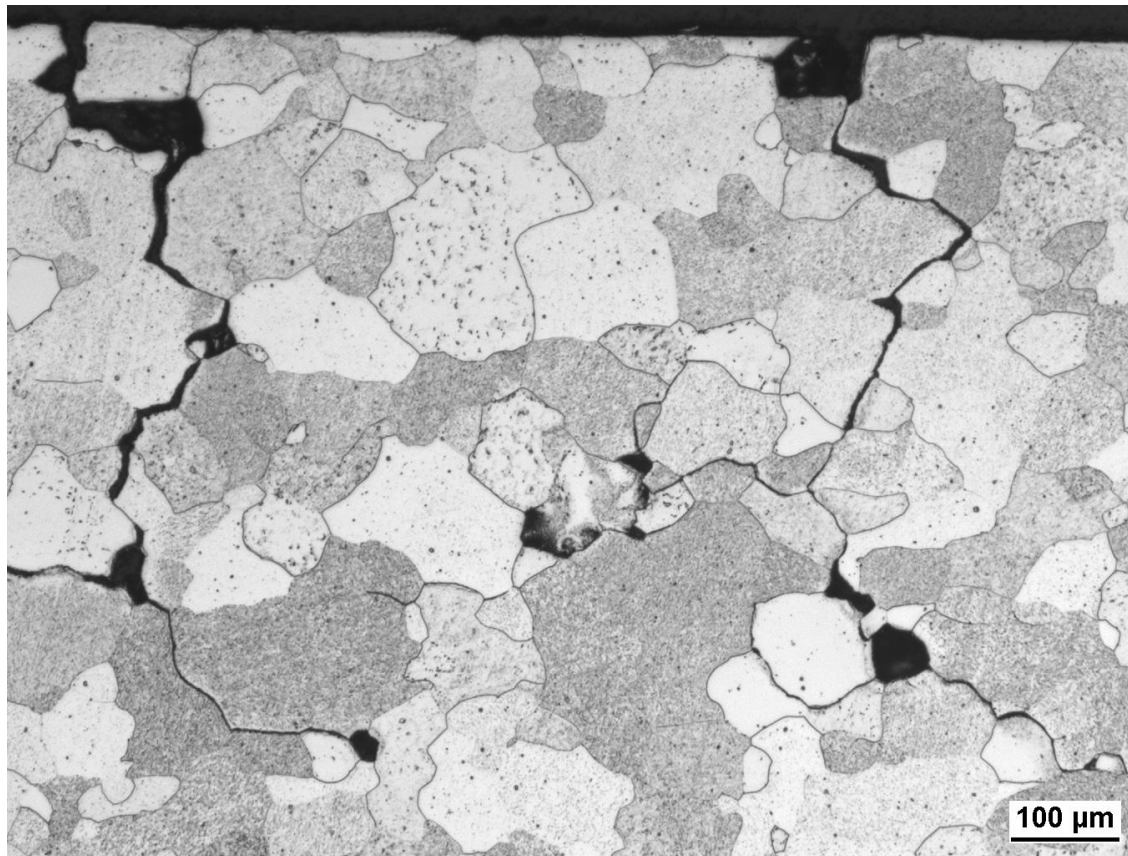
¹ *Forschungszentrum Jülich, EURATOM Association, 52425 Jülich, Germany*

² *International Research Center for Nuclear Materials Science, IMR, Tohoku University, Oarai, Ibaraki 311-1313, Japan*



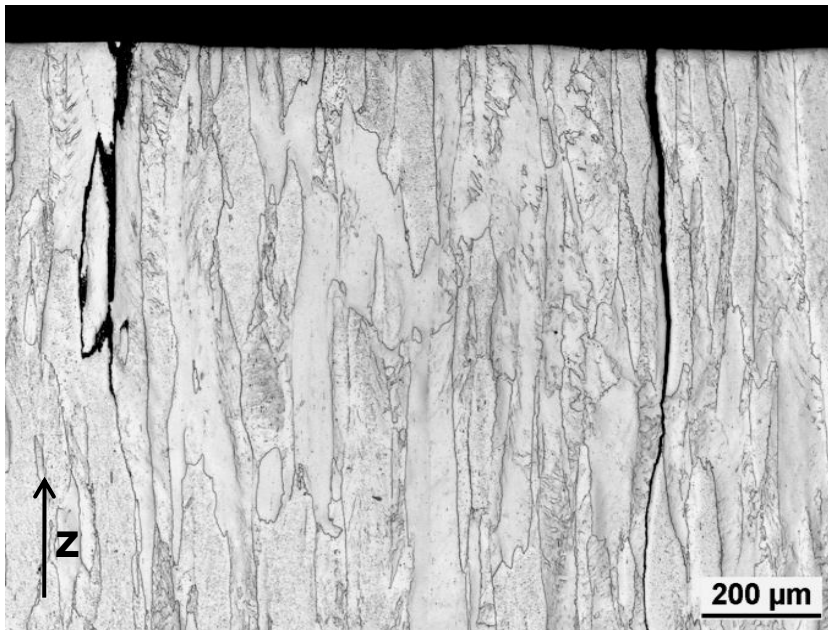
Main problem of tungsten

BRITTLENESS (of grain boundaries)

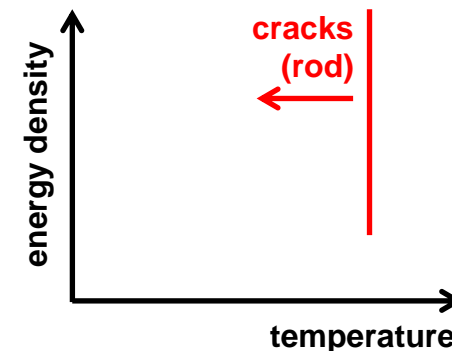


Industrially available grades - ANISOTROPY

ROD

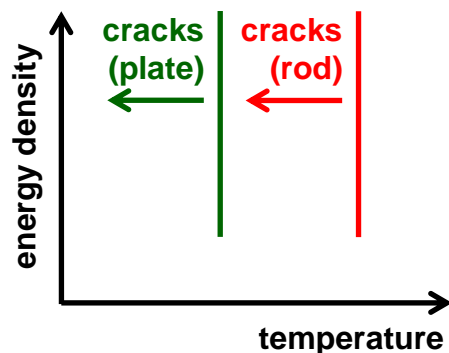


- good mechanical properties in z-direction
 - weak mechanical properties in the surface plane
- ⇒ brittle crack formation up to higher temperatures

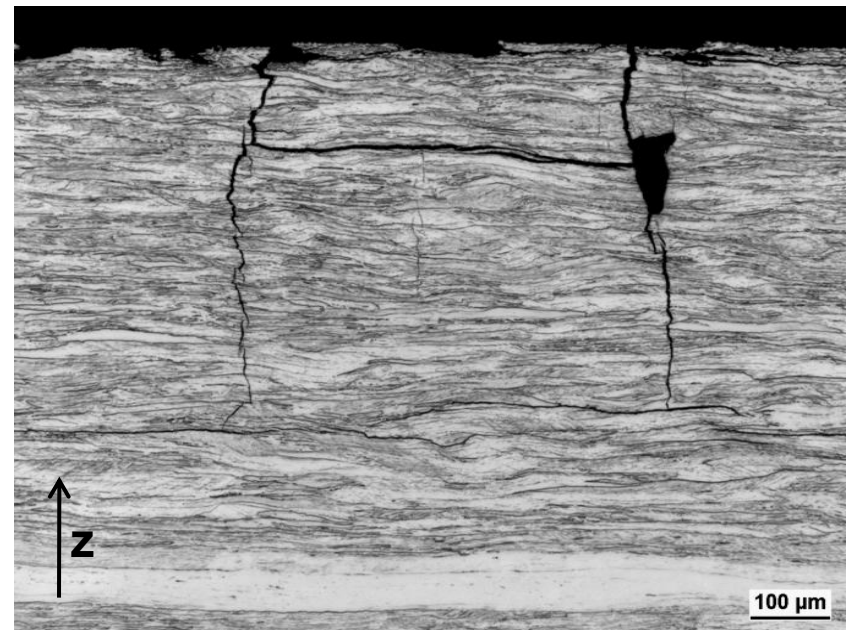


Industrially available grades - ANISOTROPY

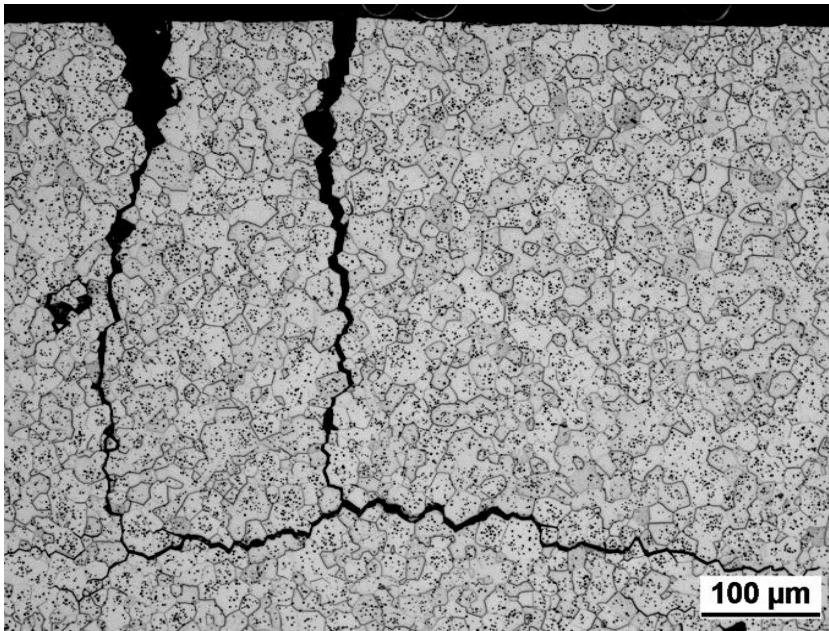
- weak mechanical properties in z-direction
 - good mechanical properties in the surface plane
- ⇒ brittle crack formation limited to lower temperatures **BUT** crack formation parallel to the surface



PLATE



ISOTROPIC material, e.g. PIM- W



J. Opschoor et al., Poster P29, PFMC-12, Jülich

- good mechanical properties in all directions

⇒ brittle crack formation limited to lower temperatures **BUT** crack formation parallel to the surface

crack formation parallel to the surface determined by

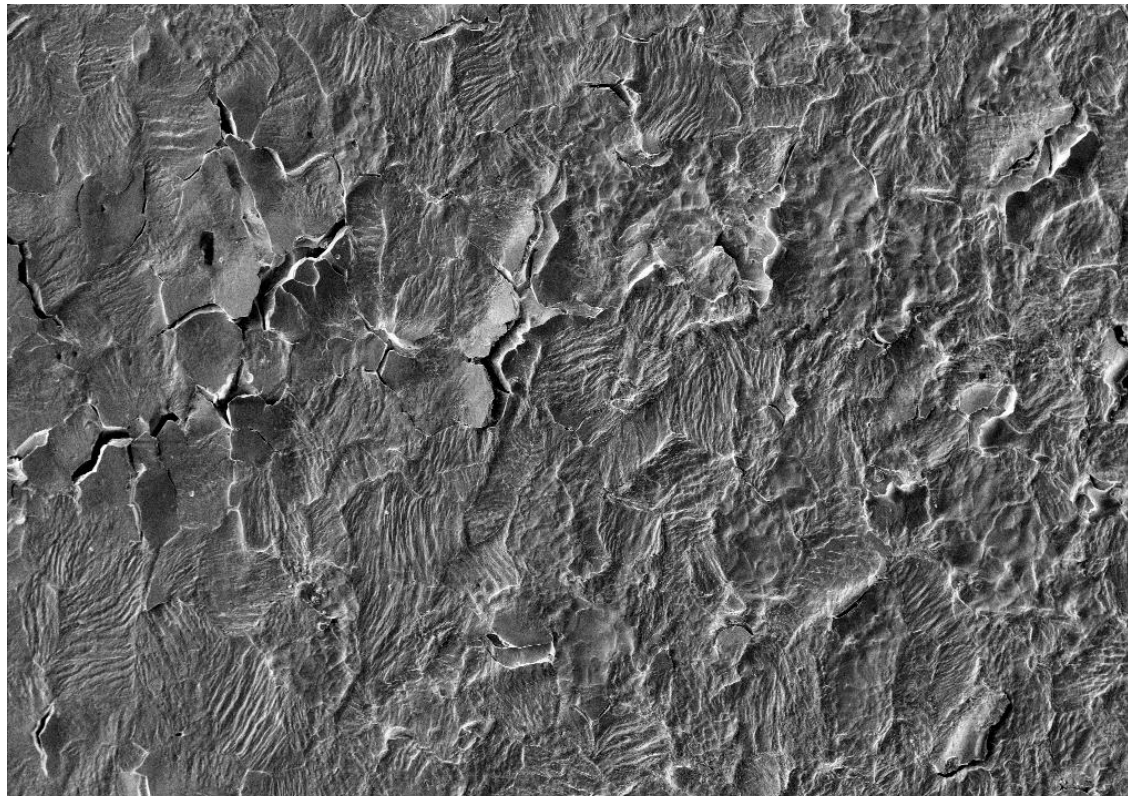
- temperature gradient (pulse duration, power density)
- resulting thermal stresses

recrystallization / grain growth ⇒ isotropy

BUT: weakening of grain boundaries & reduction of mechanical strength

Additional problem of tungsten

THERMAL FATIGUE



FZJ - IEF 2009

EHT = 20.00 kV

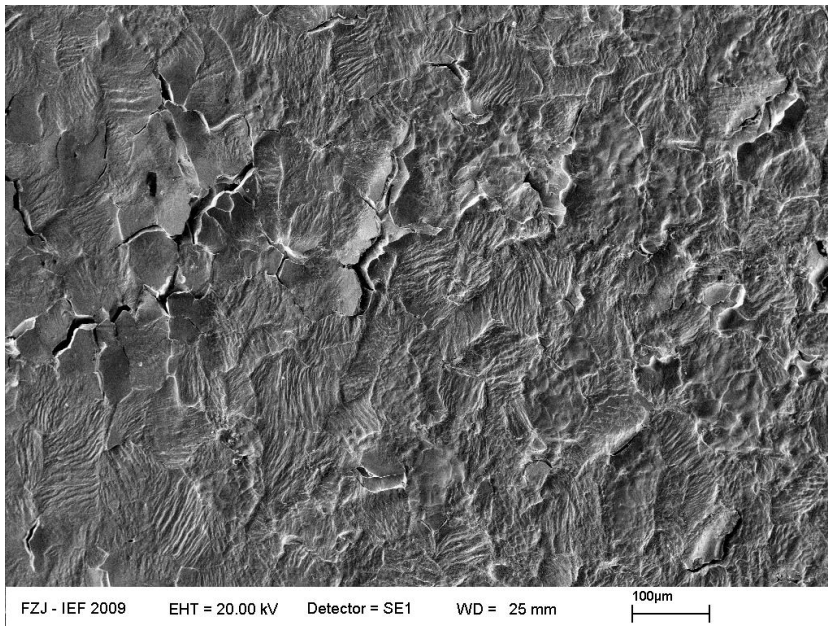
Detector = SE1

WD = 25 mm

100µm

Additional problem of tungsten

THERMAL FATIGUE



depending on

- strength and ductility
- base temperature
- grain size

⇒ plastic deformation leads (sooner or later) to crack formation

(see poster P69A, Th. Loewenhoff et al.)

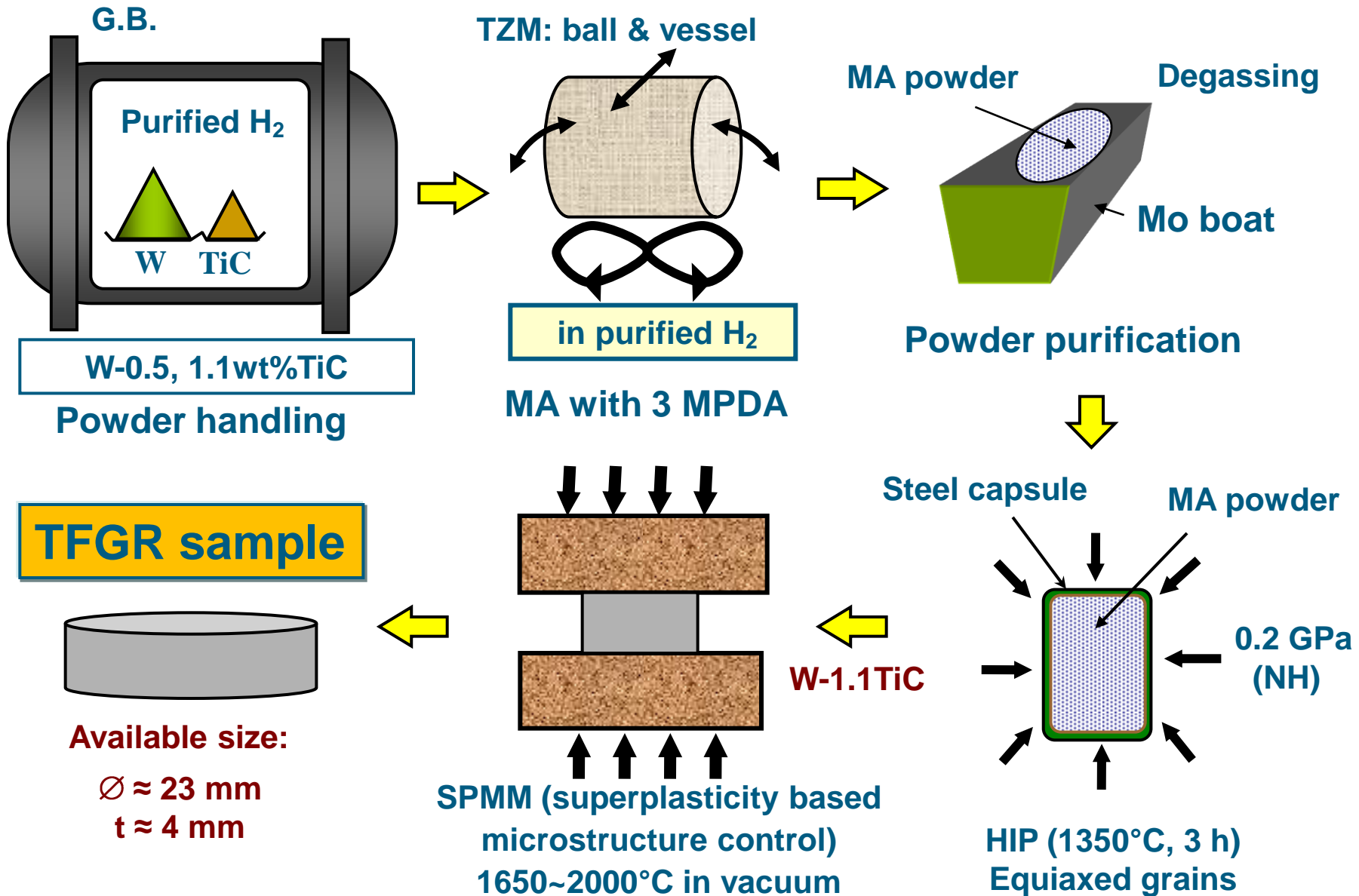
A material with good thermal shock resistance needs

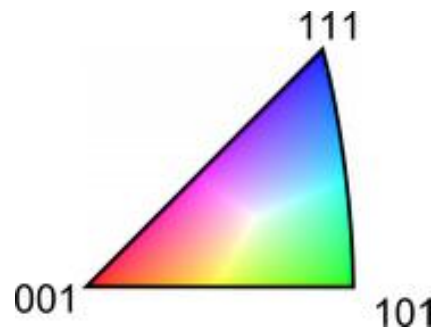
- high strength in all directions
⇒ **isotropy**
- high strength of grain boundaries
⇒ **alloying, particle reinforcement**
- high recrystallization resistance
⇒ **alloying, particle reinforcement, low degree of deformation**
- high thermal fatigue resistance
⇒ **fine grained materials**

Other needs

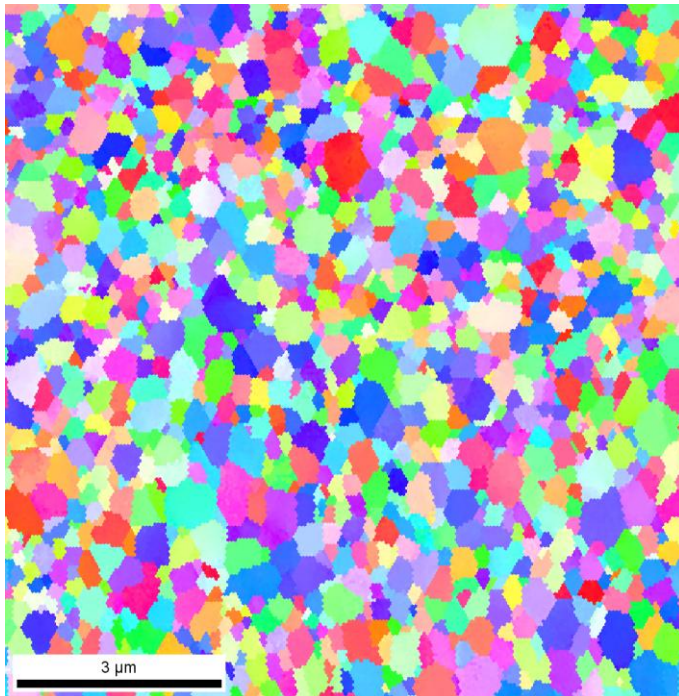
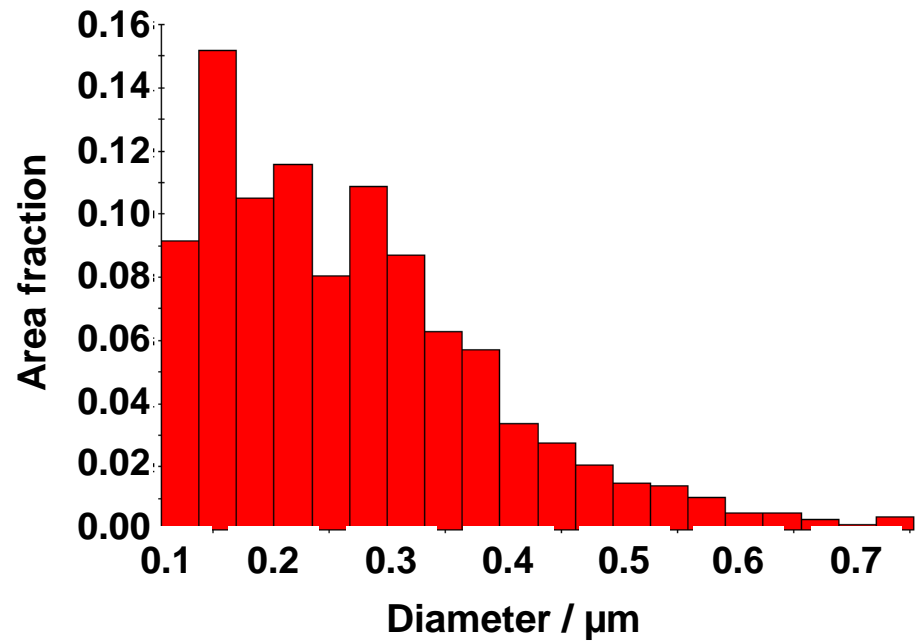
- resistance to H, He and neutrons

⇒ **W-TiC**

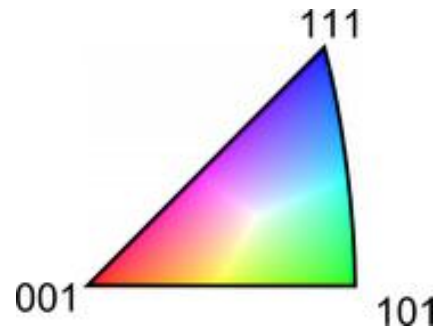




As-HIPed

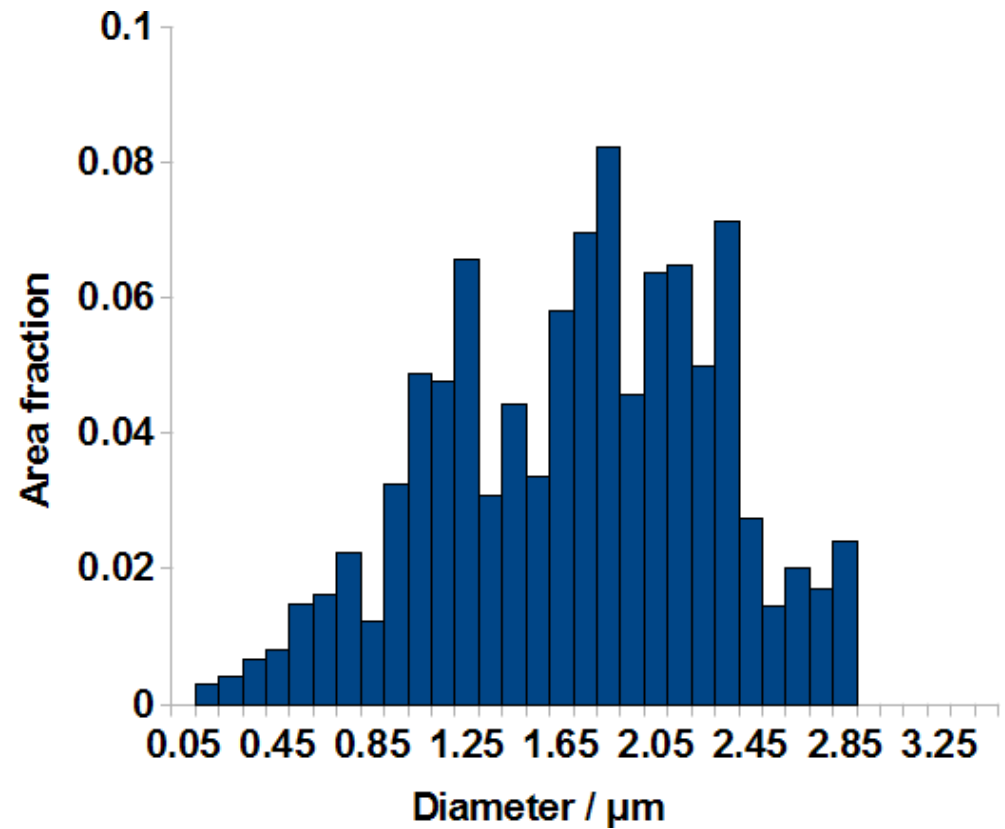


Equiaxed grains



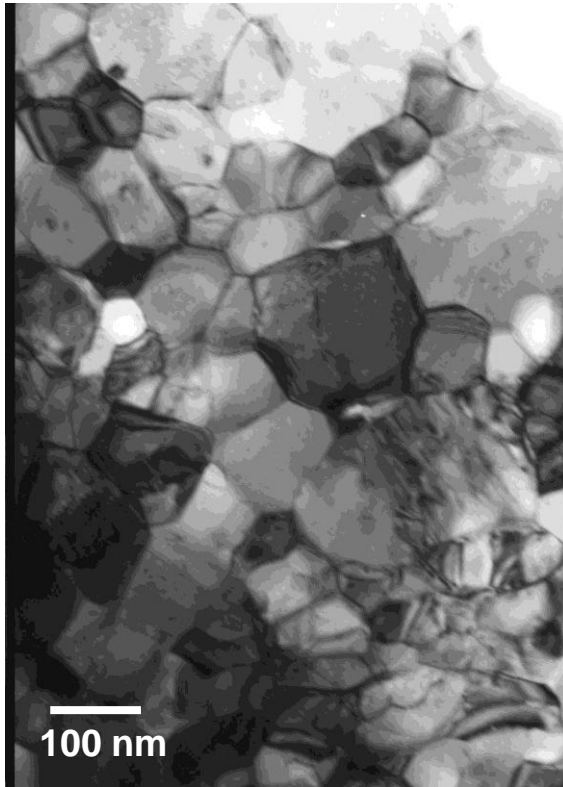
Equiaxed grains

SPMM: 1600 C x 3 h

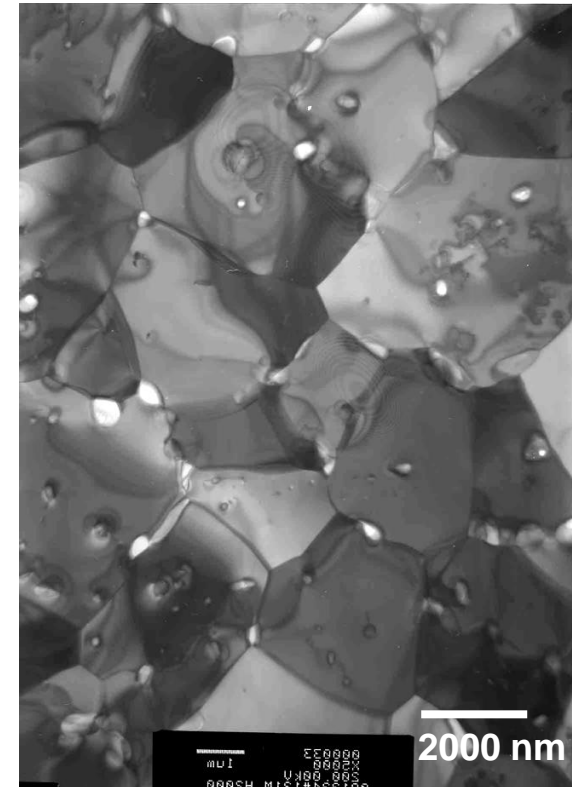
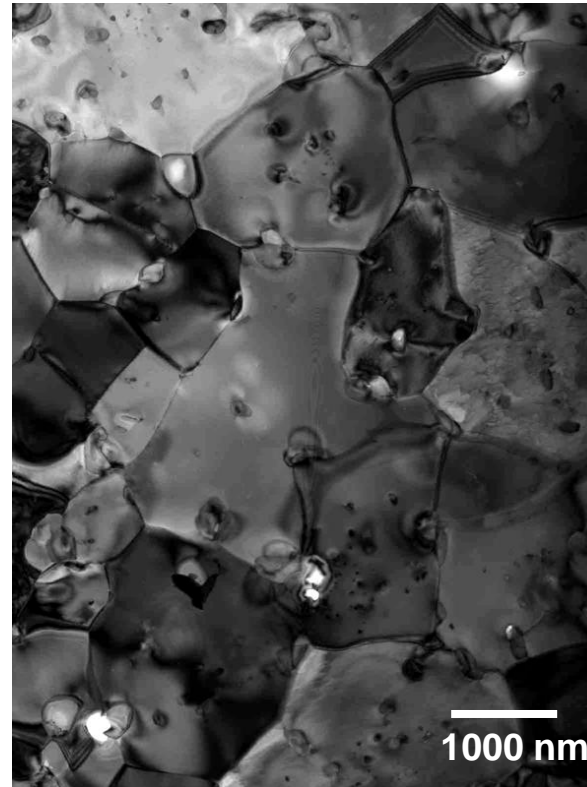


Effect of SPMM temp. on microstructure

UFG W-1.1TiC



TFGR W-1.1TiC



As-HIPed: 1350 C x 3h

Grain size: 90 nm

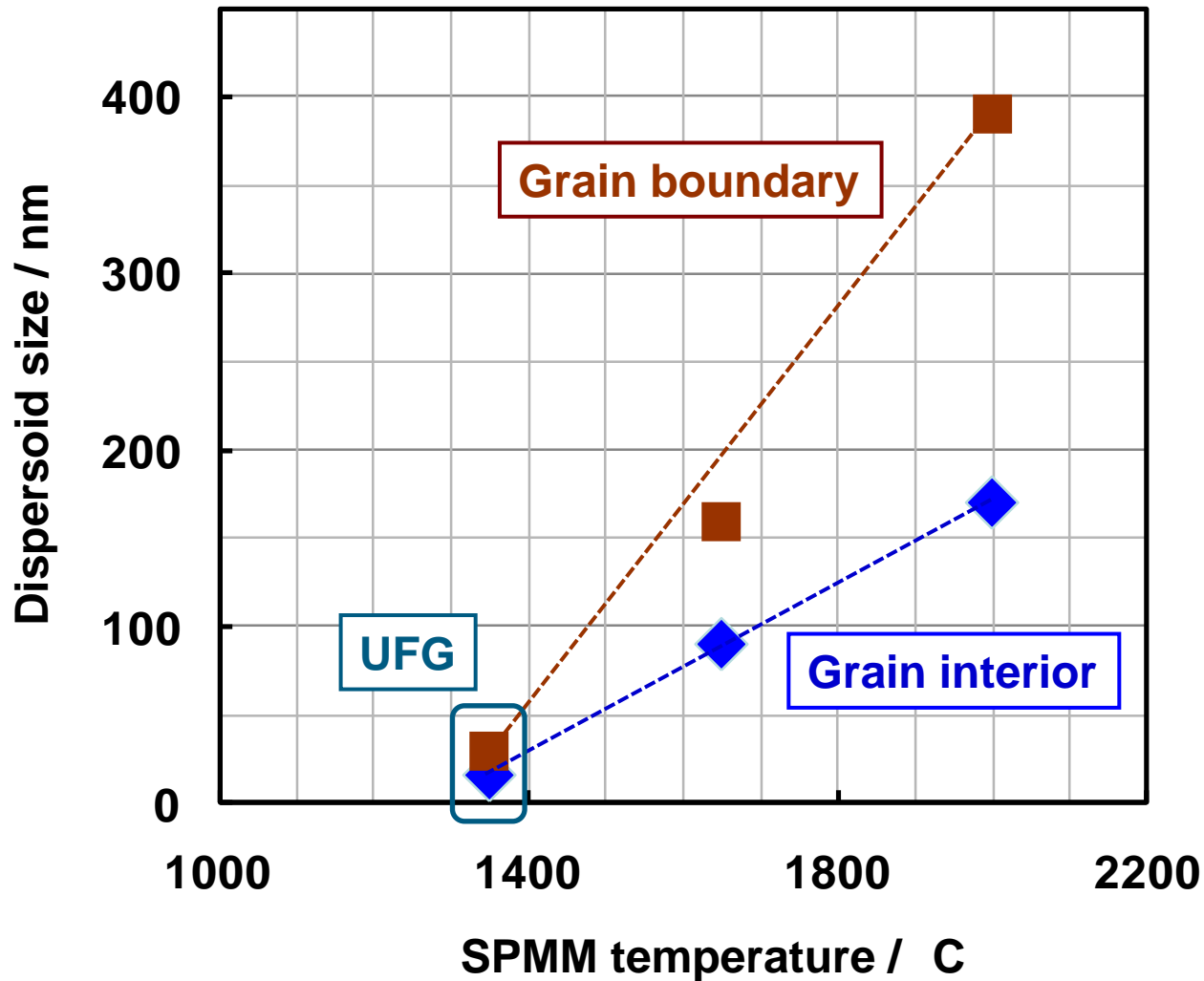
SPMM: 1650 C x 3h

Grain size: 1480 nm

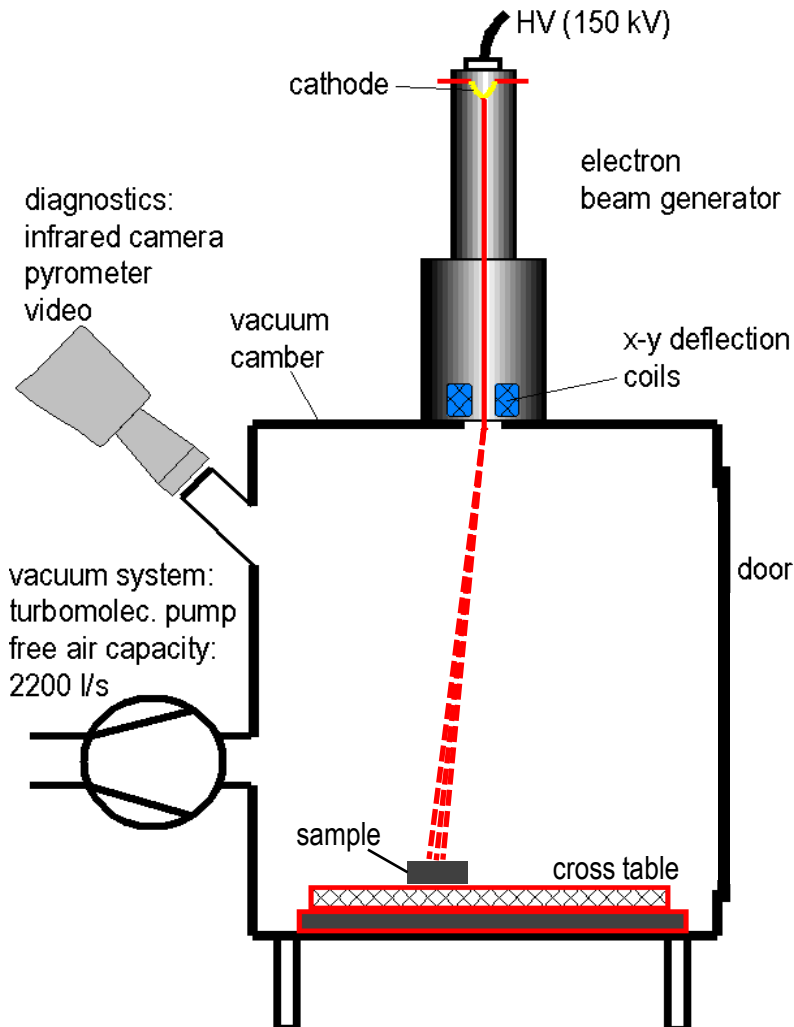
SPMM: 1650-2000 C x 3h

Grain size: 2900 nm

UFG & TFGR W-1.1TiC



JUDITH 1



Materials

UFG

- W-0.5TiC / H₂

TFGR

- W-1.1TiC / H₂, 1650 °C, ~800 ppm O
- W-1.1TiC / H₂, 1850 °C, ~800 ppm O
- W-1.1TiC / H₂, 1650 °C, ~200 ppm O

Loading conditions

$$A = 16 \text{ mm}^2$$

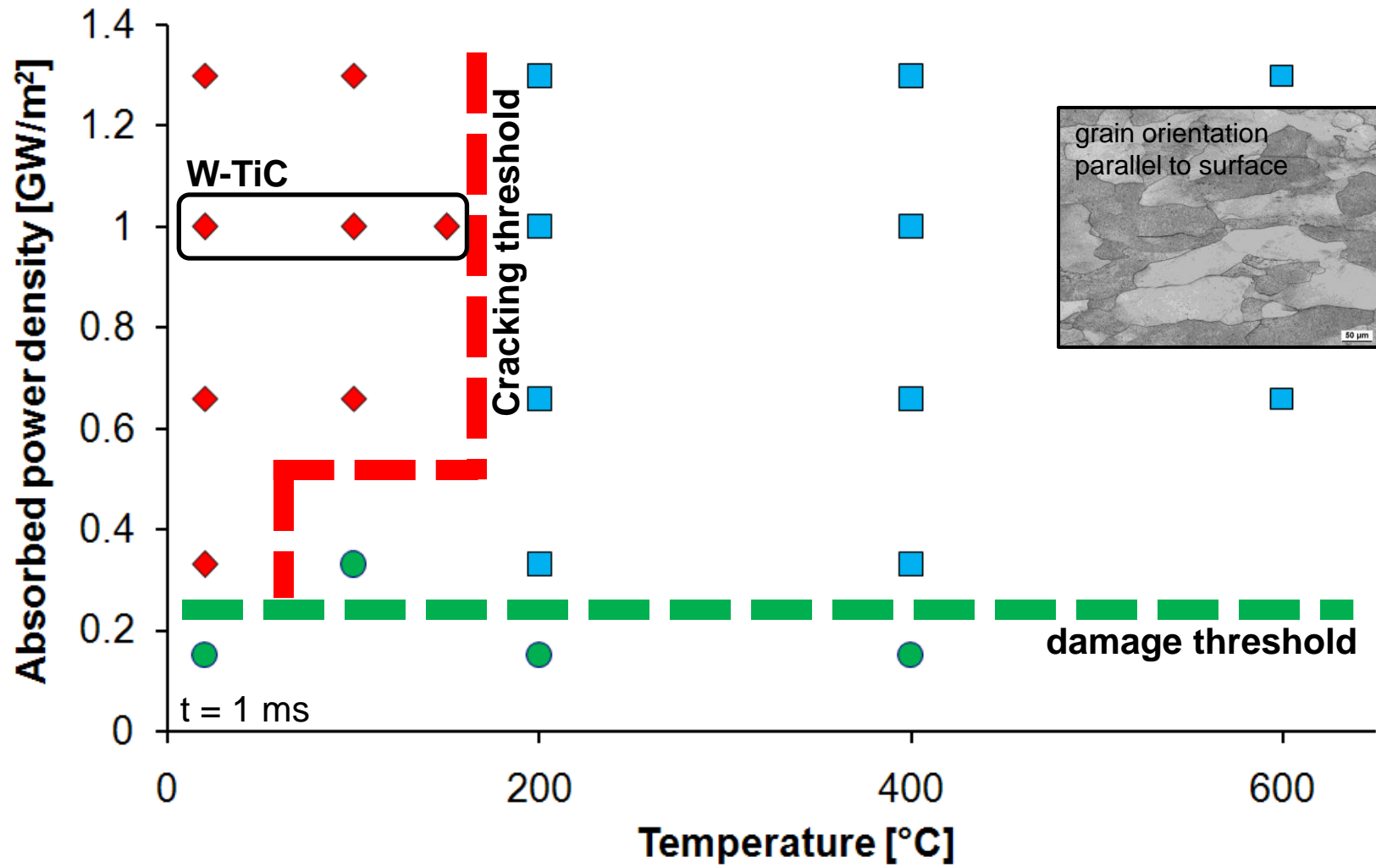
$$t = 1 \text{ ms}$$

$$P = 1.1 \text{ GW/m}^2 \text{ (pure W: } \Delta T \approx 2000 \text{ °C)}$$

$$T_{\text{base}} = \text{RT}, 100 \text{ °C}, 150 \text{ °C}$$

$$n = 100$$

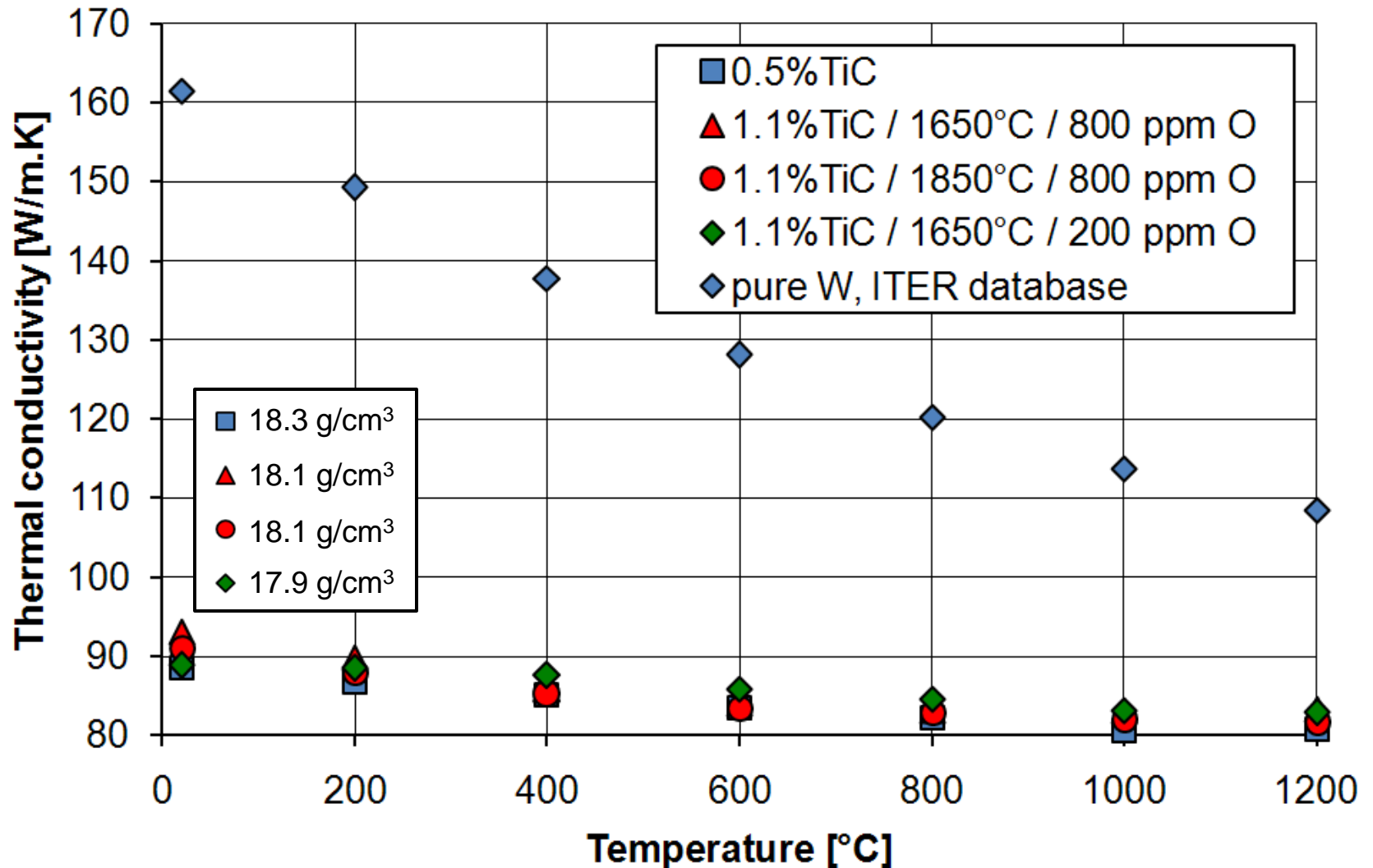
Thermal shock results: double forged tungsten



● no damage

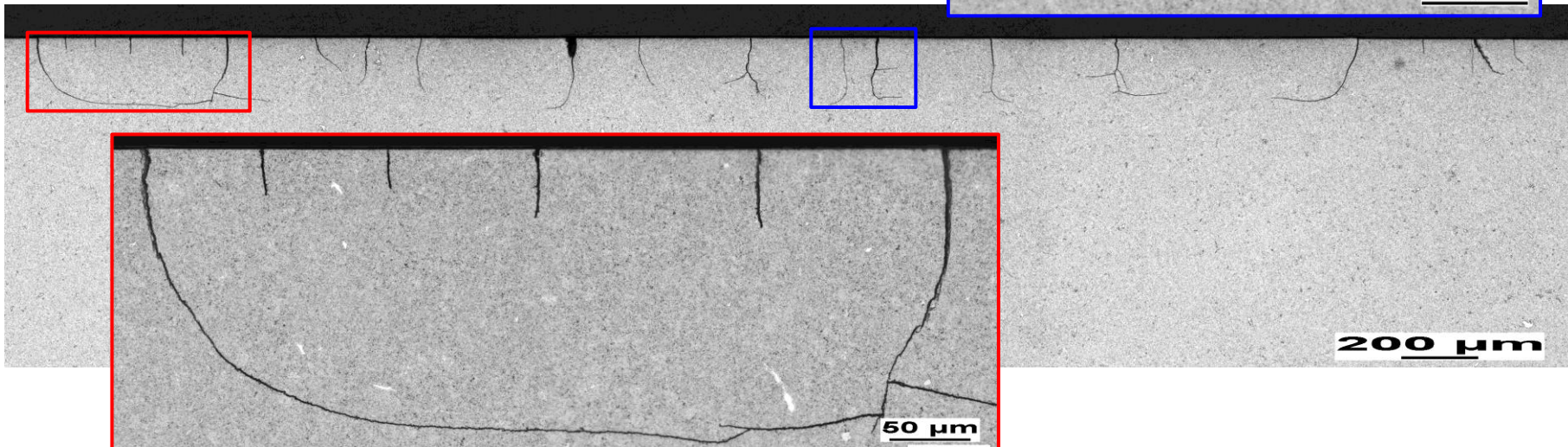
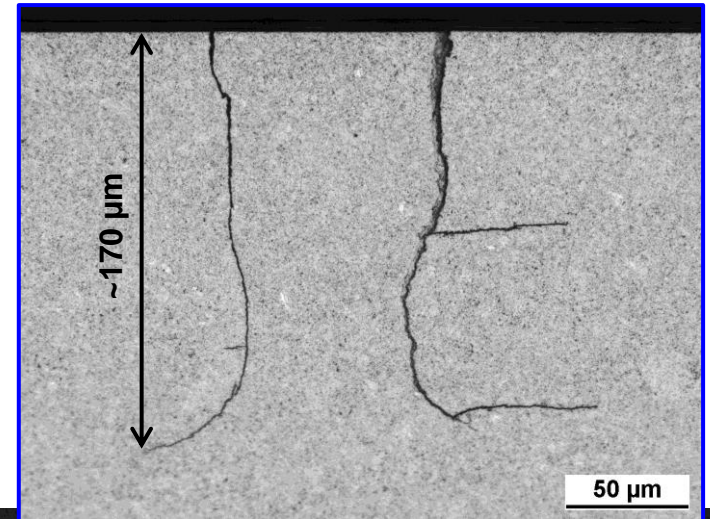
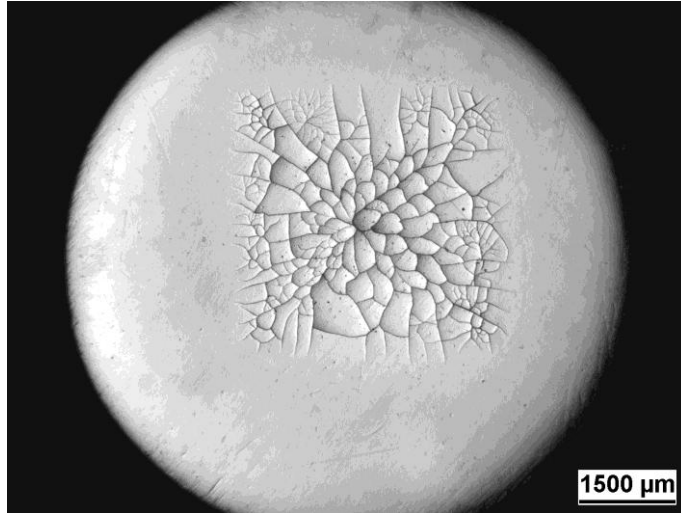
■ surface modification

◆ crack network



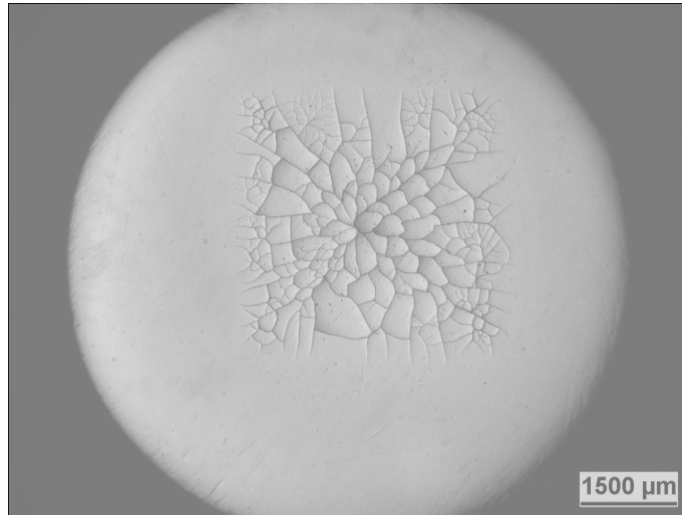
Results at $T_{\text{base}} = 100\text{ }^{\circ}\text{C}$

● W-0.5TiC

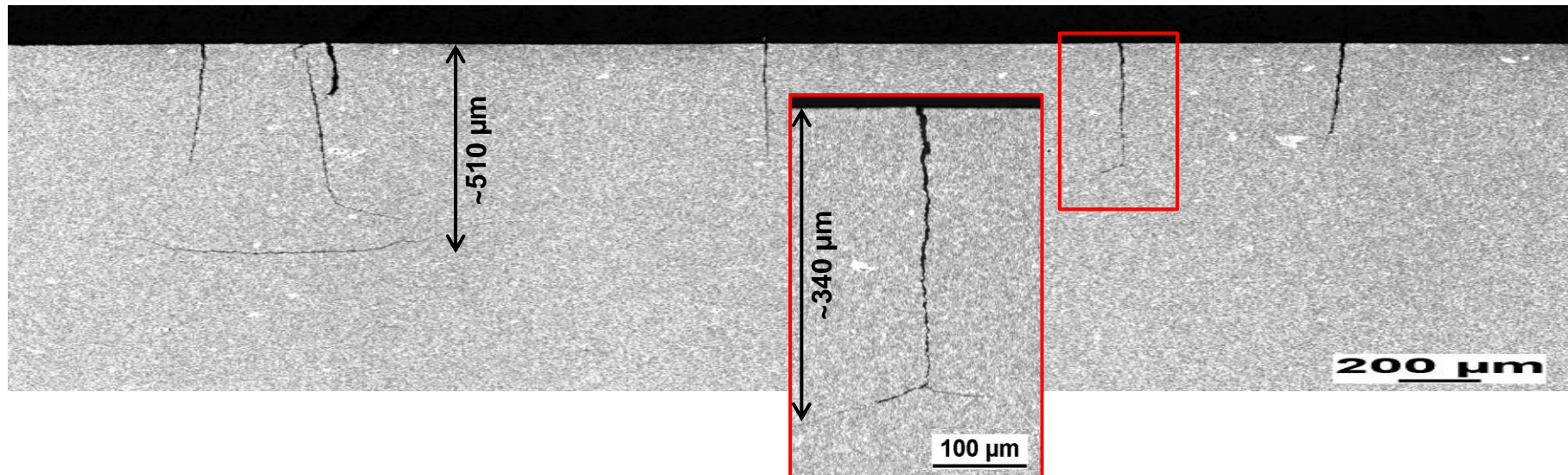
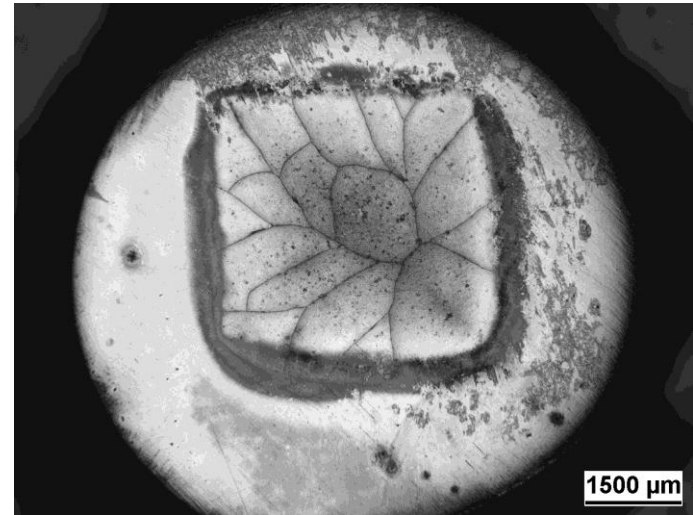


Results at $T_{\text{base}} = 100\text{ }^{\circ}\text{C}$

● W-0.5TiC

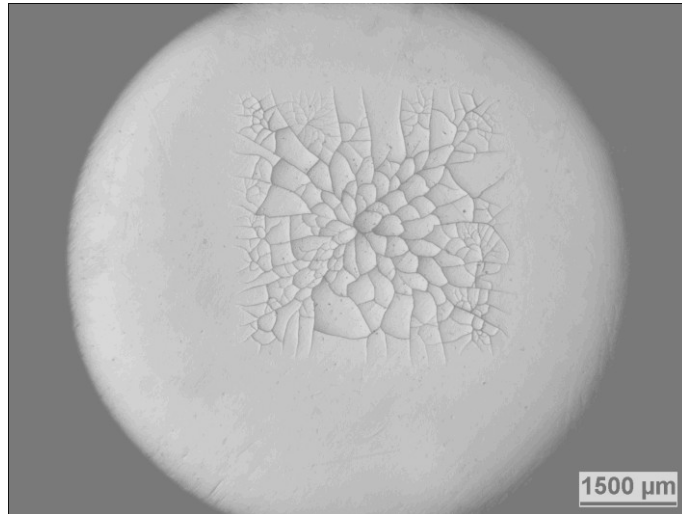


● W-1.1TiC / 1850°C / 800 ppm O

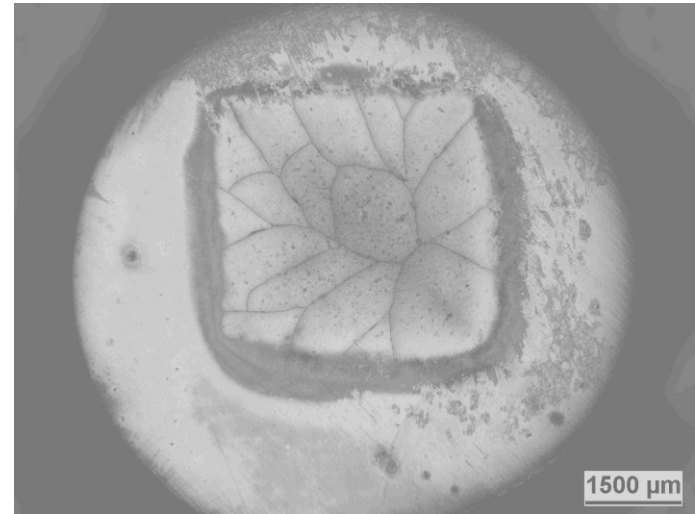


Results at $T_{\text{base}} = 100\text{ }^{\circ}\text{C}$

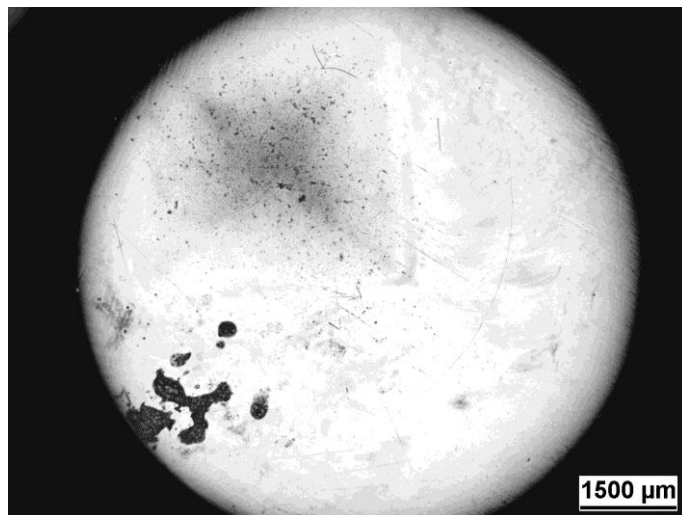
- **W-0.5TiC**



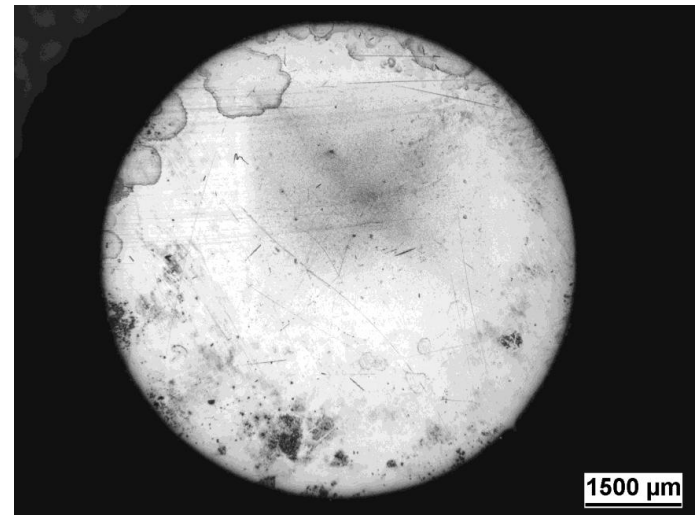
- **W-1.1TiC / 1850°C / 800 ppm O**



- **W-1.1TiC / 1650°C / 800 ppm O**

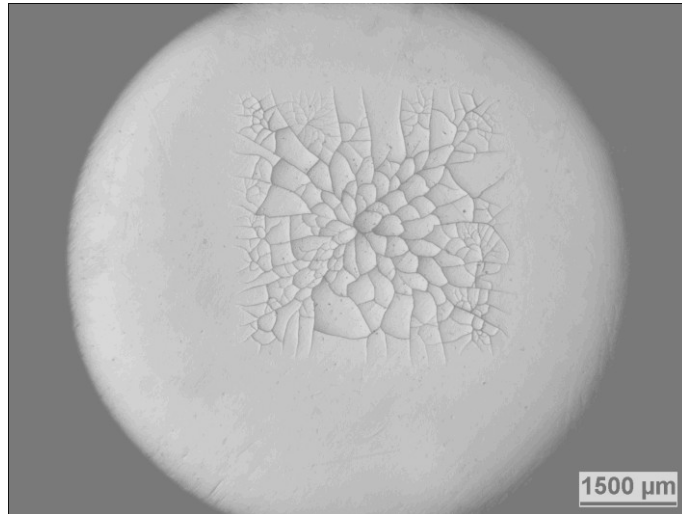


- **W-1.1TiC / 1650°C / 200 ppm O**

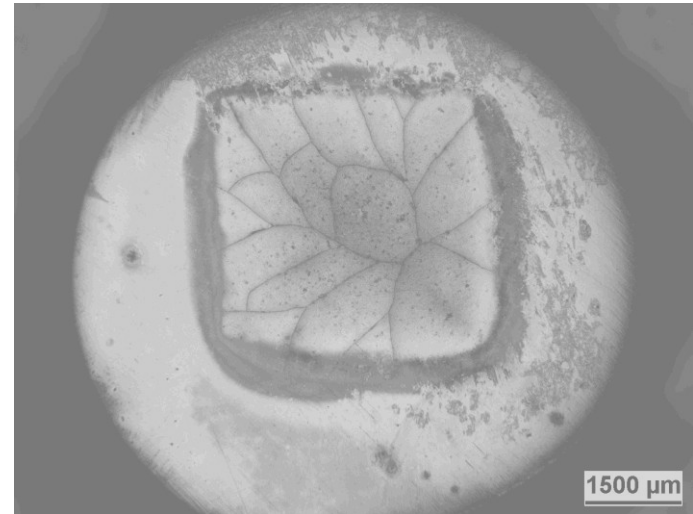


Results at $T_{\text{base}} = 100\text{ }^{\circ}\text{C}$

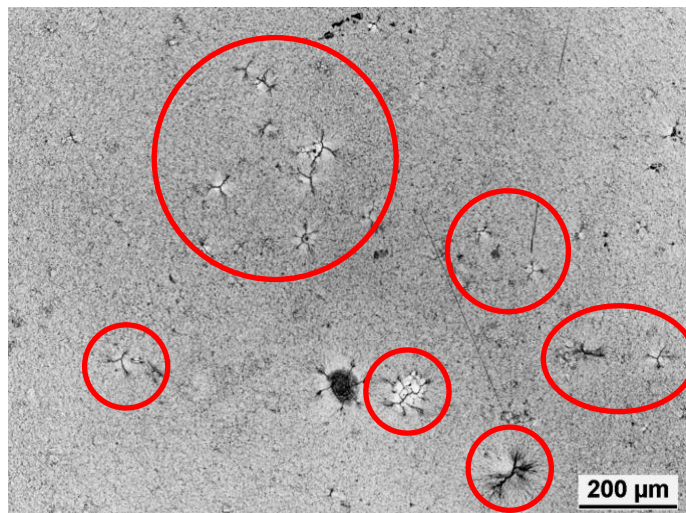
- **W-0.5TiC**



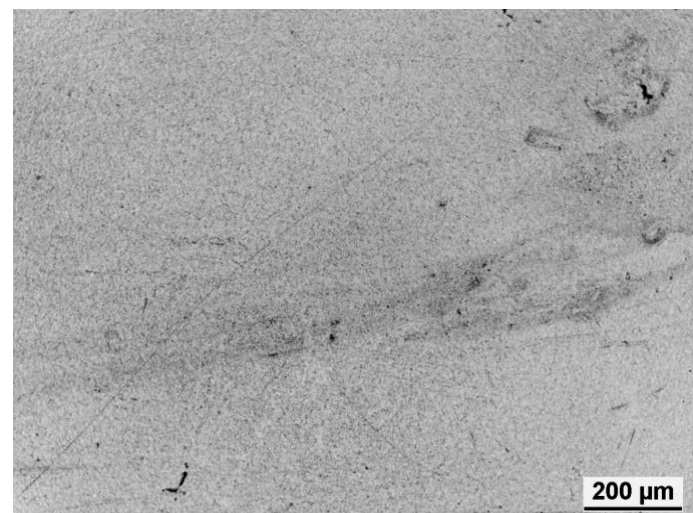
- **W-1.1TiC / 1850°C / 800 ppm O**



- **W-1.1TiC / 1650°C / 800 ppm O**

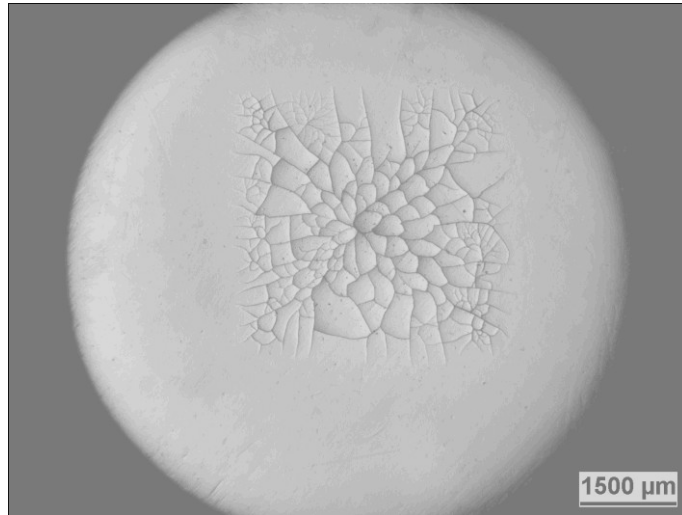


- **W-1.1TiC / 1650°C / 200 ppm O**

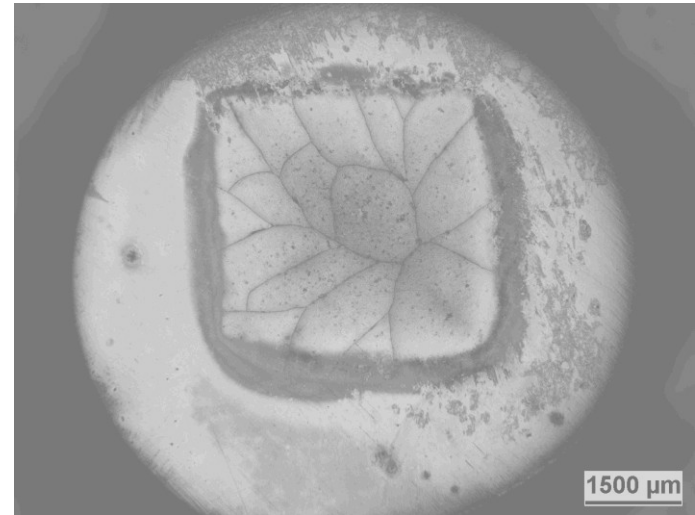


Results at $T_{\text{base}} = 100\text{ }^{\circ}\text{C}$

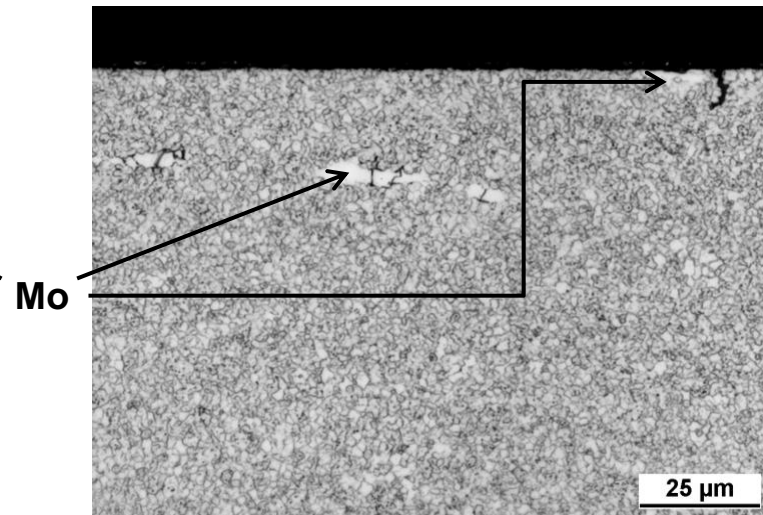
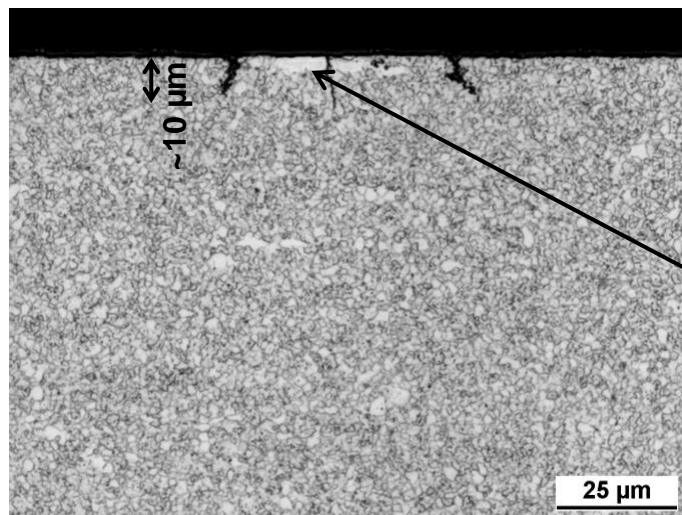
- W-0.5TiC



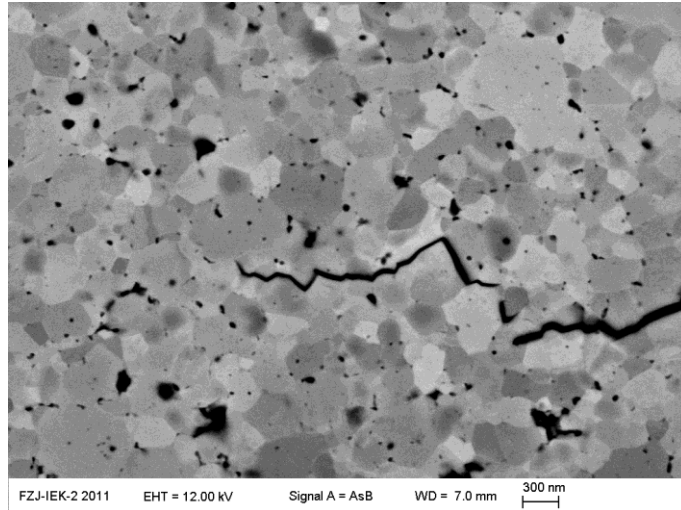
- W-1.1TiC / 1850°C / 800 ppm O



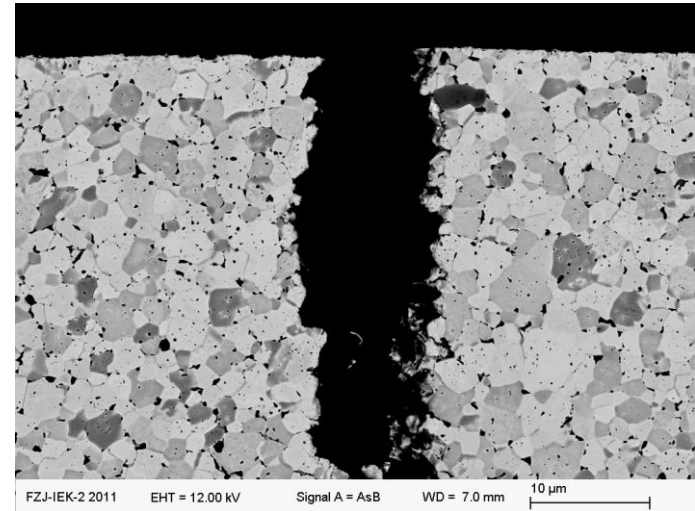
- W-1.1TiC / 1650°C / 800 ppm O



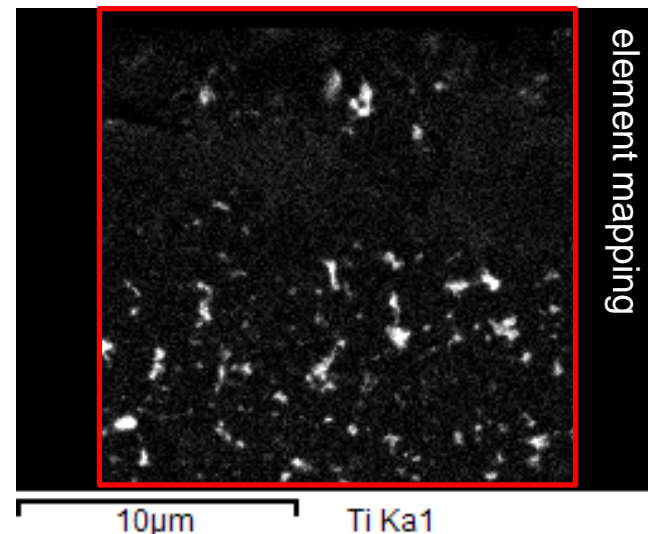
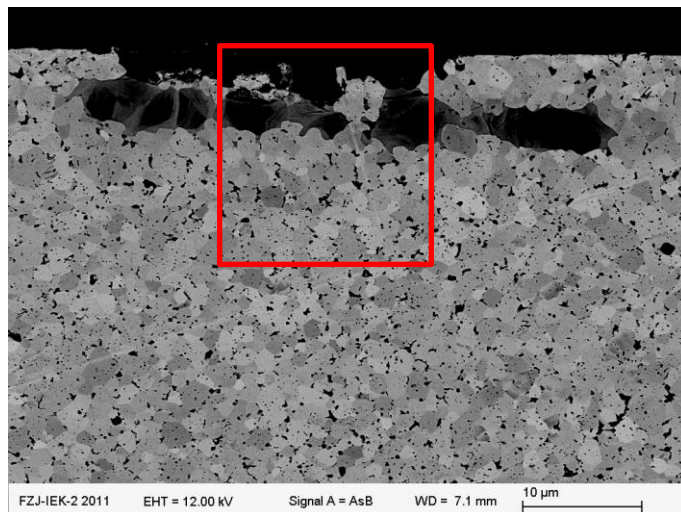
- **W-0.5TiC**



- **W-1.1TiC / 1850°C / 800 ppm O**

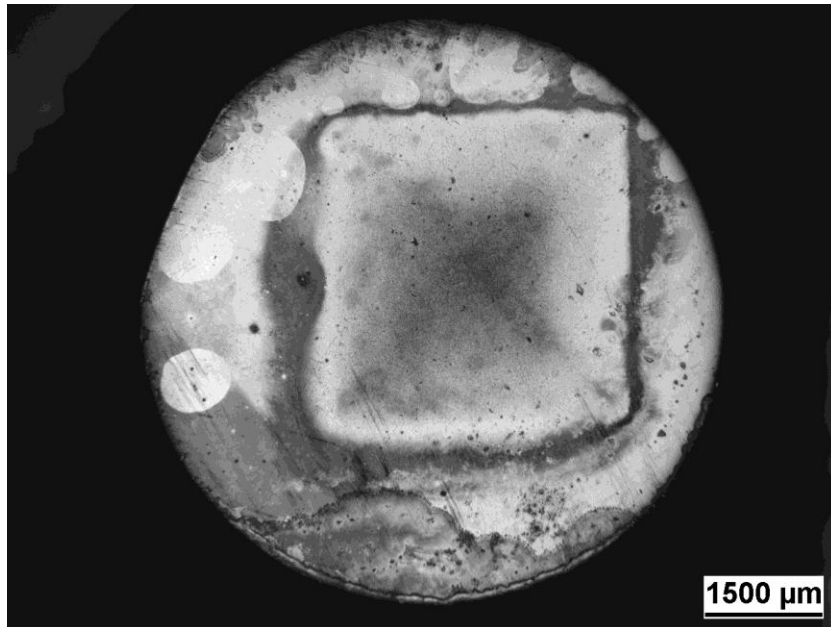


- **W-1.1TiC / 1650°C / 800 ppm O ⇒ optimized grain size / TiC distribution**

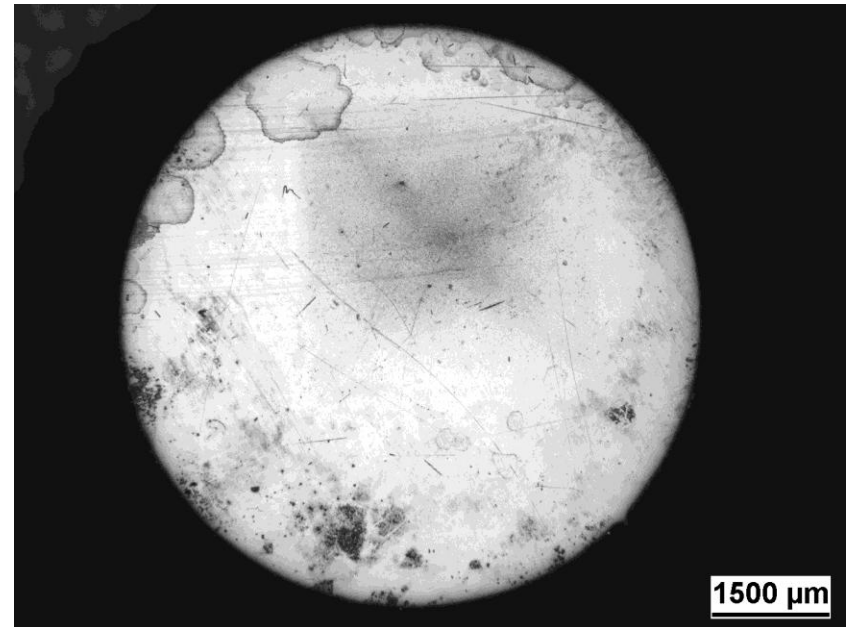


Results: W-1.1TiC / H₂, 1650 °C, ~200 ppm O

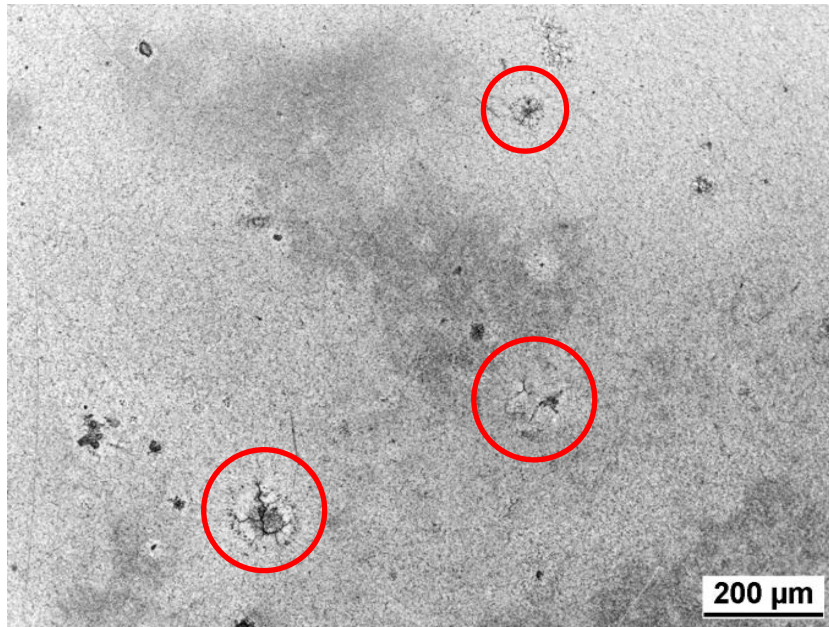
● $T_{\text{base}} = \text{RT}$



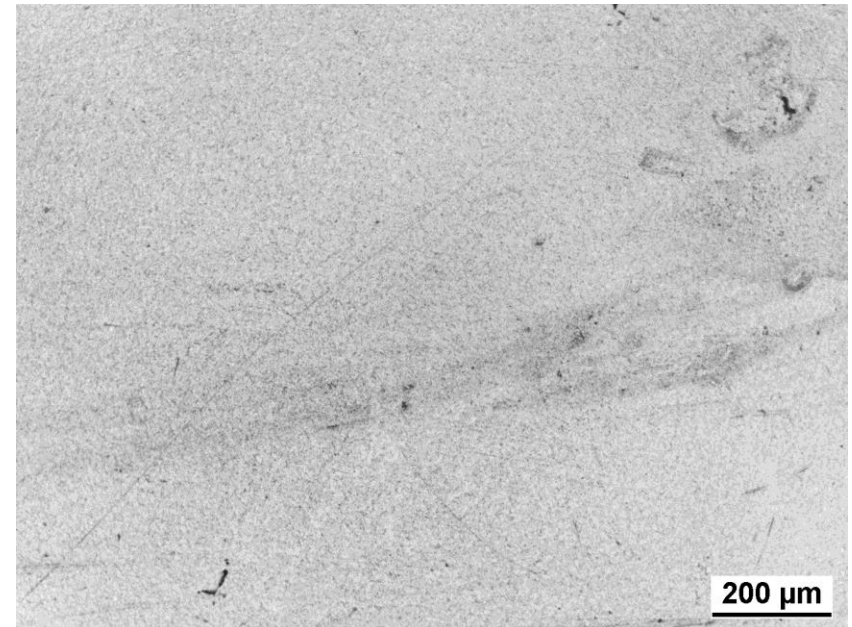
● $T_{\text{base}} = 100\text{ °C}$



● $T_{\text{base}} = \text{RT}$



● $T_{\text{base}} = 100\text{ °C}$



● via laser profilometry no detectable surface roughening after 100 pulses

Improvement of

- **cracking threshold** (T_{base} ↓ **to RT**)

of **W-TiC** due to

- **TiC-content: 0.5 % \Rightarrow 1.1 % (UFG \Rightarrow TFGR)**
- **manufacturing temperature: 1850°C \Rightarrow 1650°C**
- **oxygen content: 800 ppm \Rightarrow 200 ppm**

Future work

- reduction of impurities (large Mo-grains) acting as crack initiation points
- investigation of thermal fatigue resistance as function of temperature
- H^* , $He^{*,**}$, neutrons ** in combination with thermal shock / thermal fatigue
- **industrial upscale???**

* H. Kurishita et al., JNM 398, 2010, 87

** H. Kurishita et al., JNM 377, 2008, 34