

25th Topical Conference on Radio-Frequency Power in Plasmas

40 Years of ICRF Operation on JET: Challenges and Achievements

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UK Atomic Energy Authority



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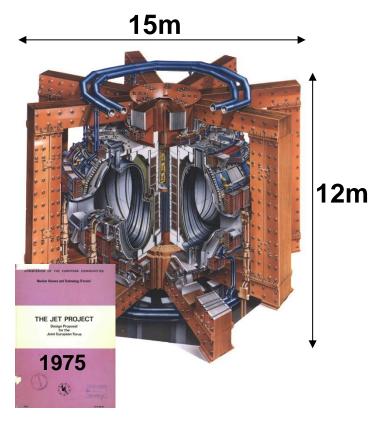
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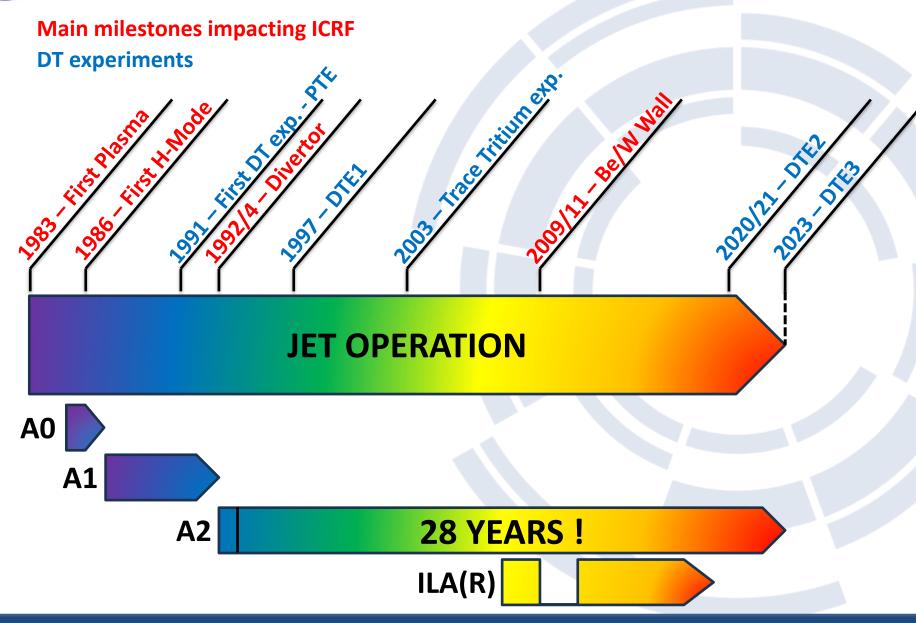


- JET started as an extremely ambitious project with many novelties such as:
 - **D-shaped** plasmas
 - Designed as a nuclear machine for D-T operation and full remote handling capability
 - Designed to confine alpha particles
 - Plasma volume and heating power two orders of magnitude larger than existing machines





JET Operation Timeline & ICRF Antennas





The JET ICRF Project

- Everything was a challenge ! To cite a few:
 - Maximize coupling
 - Minimize impurity production
 - Coupling unprecedented levels of power and energy into the plasma ! 1.5MW/antenna for 10 s i.e. 15MJ (compared to 0.1MJ in TFR and 0.8MJ in PLT)
- Some elements of the design philosophy:
 - Use of existing and proven technology as much as possible
 - Extensive testing of antenna, prototypes and components on dedicated test-bed

IMPURIT

THALLENGE,

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MATCHING CHALLENGE.

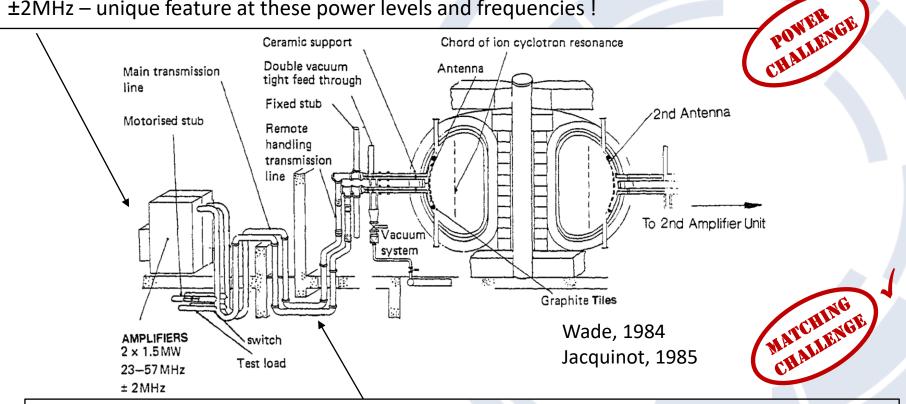
COUPLIN CHALLENGE!

- Compatibility with D-T plasmas, remote installation and maintenance
- Heating of JET plasmas in a range of ion species (H, D, He3, T), plasma parameters and B₊
 - → Large operating frequency range required : 23-57MHz

Development of a highly flexible and versatile high power ICRF tool

The ICRF Plant & Matching System

- High power: 16 x 1.5MW amplifiers (Herfurth) upgraded to 16 x 2MW in 1989
- Large operating frequency range: 23-57MHz (except 39-41MHz) in eight bands of 4MHz
- Amplifiers designed to be broad-band and allow 'instantaneous' frequency shifts of ±2MHz – unique feature at these power levels and frequencies !



- 84m long 30Ω TL (Spinner) special design for JET, 3 bar pressurized, 50kV rating
- Matching realised by tuning stubs at generator end and frequency variation (≤100kHz)
- Prematching stub can be installed close to the antenna used in certain conditions

The early days of antenna design for JET ICRF

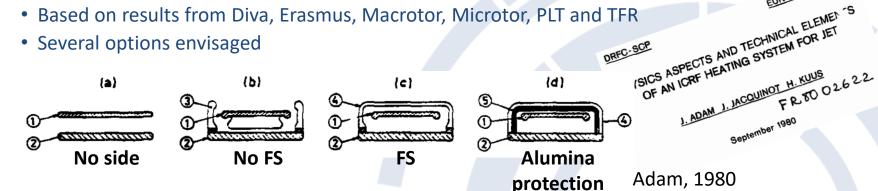
Antenna design work started at Fontenay-aux-Roses (CEA) in 1980

EUR-CEA-FC-1065

COUPLING

CHALLENGE

Based on results from Diva, Erasmus, Macrotor, Microtor, PLT and TFR



- Option C retained
- 6 MW coupled in one port with 4 launching elements (LFS mount)

Three new design features

- Enhance coupling by moving the antenna closer to the plasma -> antenna-limiter concept
- Active cooling of the 15° tilted Faraday screen bars
- New shapes of radiated wavelength spectra : from usual (at the time) monopole to so-called quadrupole antenna
- Main concern : high level of impurity
 - Incentive to investigate other phasings than monopole (exclusion of long wavelengths) generating edge modes) IMPUBIL CHALLENGE,
 - Increased coupling requires antenna close to plasma edge -> low-Z side protections
 - Tilted FS bars to reduce surface modes

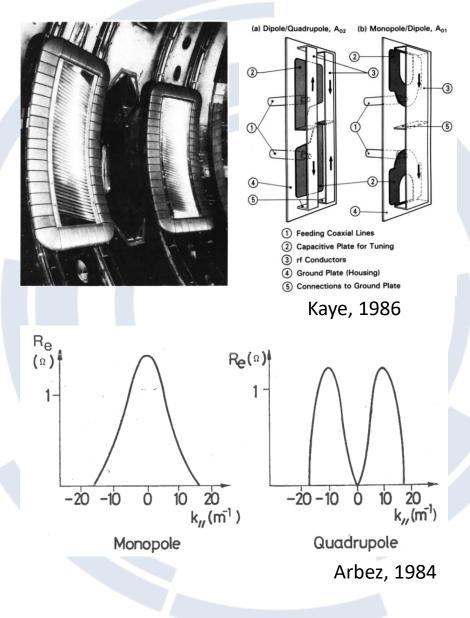
First generation of antennas – A0

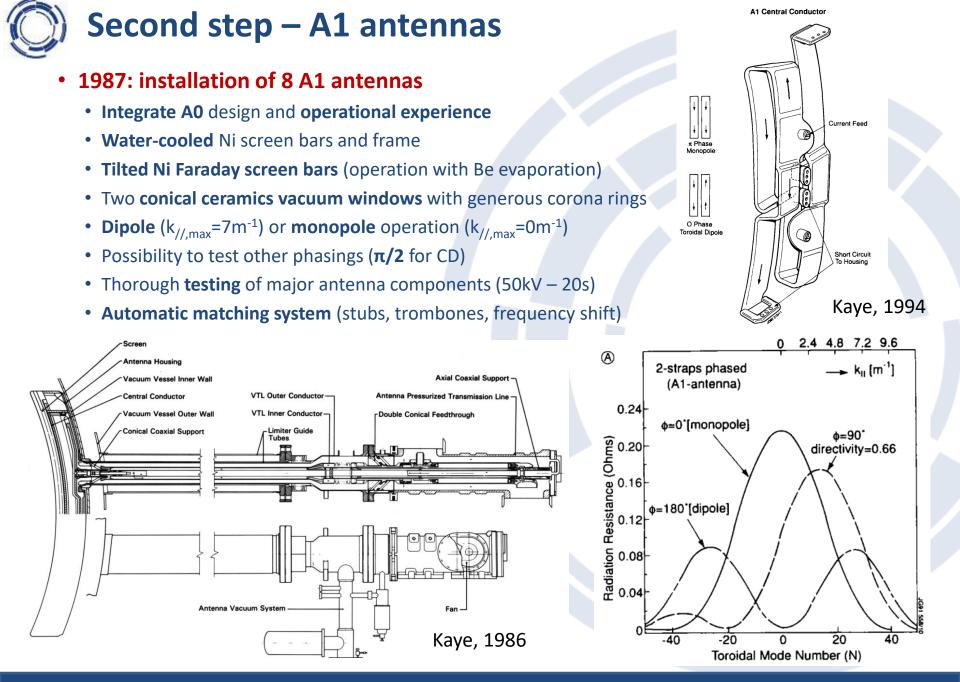
1984: installation of 2 A0 antennas

- Designed for short pulse (uncooled)
- **Give operational experience** for optimisation of future antennas
- Two types of central conductor: monopole and quadrupole; quadrupole expected to reduce impurity produce at the cost of lower coupling
- Antenna-limiter protected by graphite tiles to reduce impurity production
- **15° tilted Faraday screen bars** to minimise excitation of surface modes
- Tested on the TFR testbed
- All components tested up to 45kVp and 1.5kAp @ 60MHz, multipactor region [50,2500] V

• 1985-1986: Start of operations

- Two 3MW units installed
- Third A0 connected
- 5MW and 10MJ coupled to the plasma
- 1987
 - Up to 17 MW coupled in limiter plasmas
 - Impurity levels decreased with tilted Faraday screen bars and dipole operation





Meeting the impurity reduction challenge

Overcoming the RF-specific impurity production

- Progress in the understanding and modelling of the role of RF rectified sheath effects
- 1989: Be Faraday screen bars instead of Ni
 - Lower the Ni impurity release (low Z and self-sputtering coefficient < 1)
 - No active cooling required (simplified design)
 - Open screen design to reduce further RF losses in screen
- Impurity levels further reduced by
 - Aligning the Faraday screen bars to the static magnetic field
 - Lowering the density at the Faraday screen by the use of side limiters
 - Preferably operate in dipole phasing
- Use of carbonization and Be evaporation

Achievements

- Coupled 22MW on plasma (26.3MW generated)
- Coupled 200MJ into single plasma
- Long pulse operation up to 60s
- RF-only H-mode achieved (up to 12MW coupled)
- Operation with $\pi/2$ phasing
- Reliable operation on plasma up to 30kV, electric fields of 2.2kV/mm parallel to Bt, pressure in VTL < 10⁻⁴mbar
- Arc damage at conical ceramic (support of inner conductor) unexplained and failure of arc protection (needs improvement)
- Constant R_c real time control developed for H-mode by feedback of the plasma position



COUPLING

CHALLENGE

MATCHING

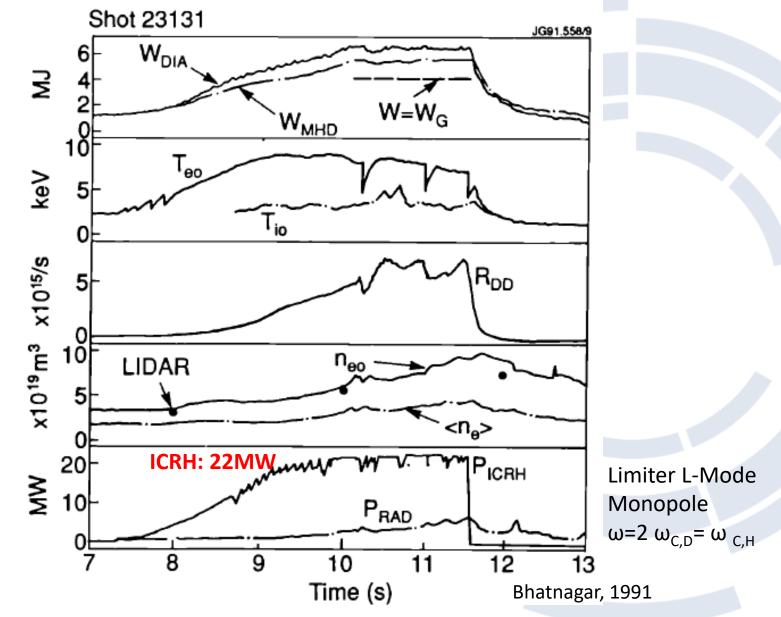
CHALLENGE

POWER

CHALLENGE



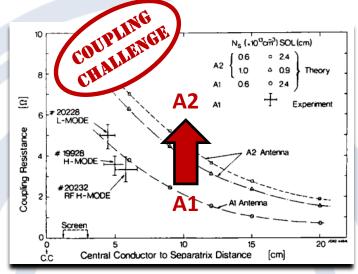
Record ICRH coupled : 22MW H minority heating in D

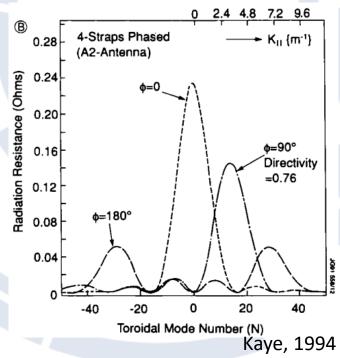


And then came the divertor... and the A2s

- 1992-1994: installation of A2 antennas during pumped divertor installation shutdown
 - Distance plasma-wall larger -> needs improved coupling
 - Changed plasma shape (curvature)
- Design changes driven by installation of pumped divertor and ROX of A1 operation
 - Four 4-straps antennas enabling fast wave current drive
 - 1.5 x wider and 2 x deeper than A1 to **improve coupling**
 - Septum and sidewalls slotted to minimise the spectrum degradation by return currents
 - Increased disruption forces → Minimisation of induced loop currents on antenna by lightweight antenna box design (corrugated sheets) and FS bars fitted with 0.1Ω resistors
 - Antenna tested at 42kV 20s on test-bed (limited to 30kV for ops)
 - Tilted FS (varying on height 13° to 18° to match B_t changes)
 - Antenna protected by new poloidal limiters
 - Double conical feedthrough ceramic window
 - Upgraded control system (arc detection, power and phase control, matching) to **optimise power handling**
 - 1995: refurbishment to cure arcing and coupling issues
 - 1996: RFLM real time control & monitoring of the ICRH plant

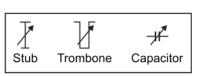
28 years operation without any major issue !!!







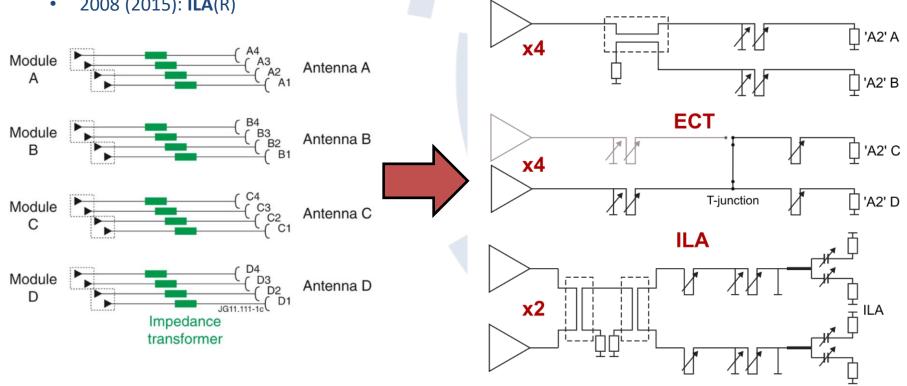
- Operation in **ELMy H-mode**
 - Matching system too slow to cope with fast load variations
 - → Insufficient load tolerance of matching scheme (generator protection VSWR trips)
- Implementation of new load-resilient matching solutions
 - 2004/5: 3dB hybrid couplers
 - 2008/9: External Conjugate-T (ECT) ۲
 - 2008 (2015): ILA(R)



3dB

MATCHING

THALLENGE



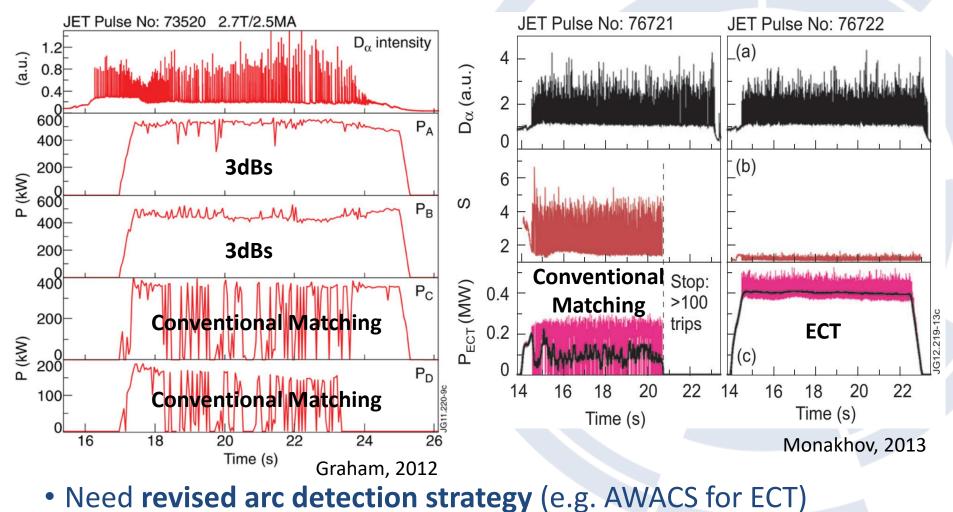


• Load-tolerant schemes successfully implemented

3dB hybrid couplers

External Conjugate-T

MATCHING



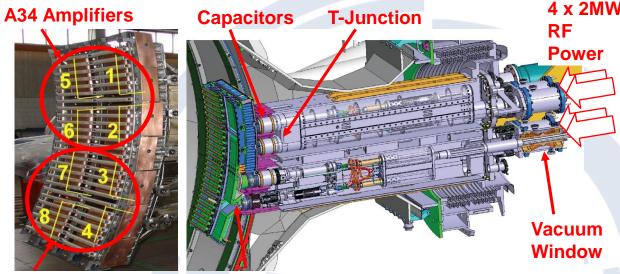
Towards High Power Density – the ILA

KEY FEATURES

- 4 x 2 short low-inductance straps Resonant Double Loops (RDLs) In-vessel matching capacitors
- **Conjugate-T** with typically Re(Z_T)=3...10 Ω and Im(Z_T)=-5...0 Ω
- λ_{42.5MHz/4} Z-transformer + second matching stage
- Port plug antenna
- All components tested up to specs

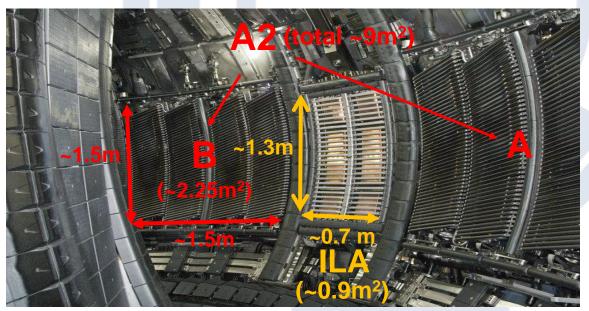
ACHIEVEMENTS

- High power density operation
 ~4MW/m² on ELMy H-mode
 (A2: ~1MW/m²)
- ✓ Similar levels of impurities as A2s
- ✓ Operation at high voltages 40kV
- ✓ Control of close-packed array
- ✓ Load resilience
- ✓ Arc detection : SMAD, SHAD
- ✓ Validation of RF modeling and coupling predictions
- Capacitor failures validate the external matching choice for ITER



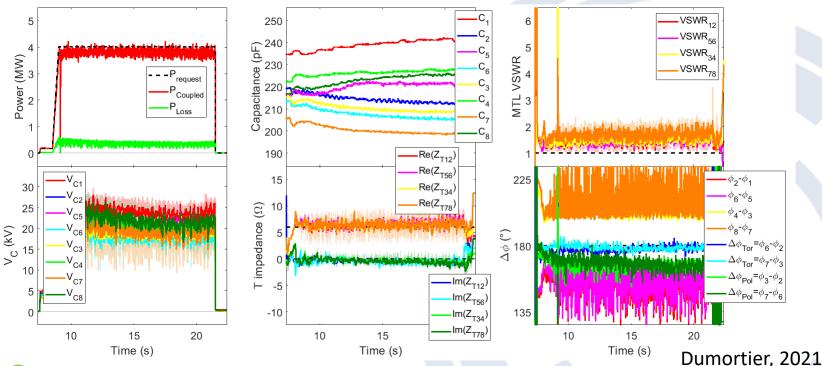
A12 Amplifiers

RDLs





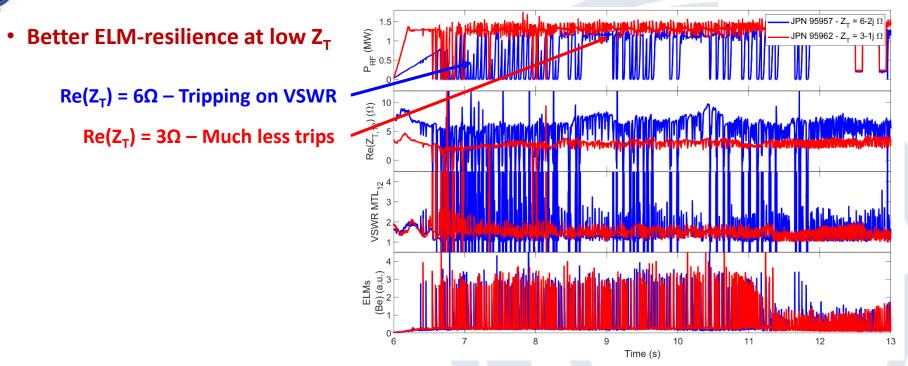
ILA Full Array Control



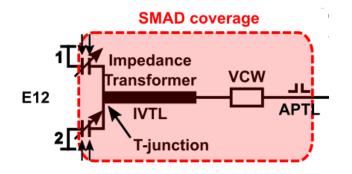
JET Pulse No : 95098 – 33MHz

- Full array control **successful** at 33, 37 and 42MHz
- Up to **4MW** at 33 and 42MHz
- Poloidal phase scan achieved at 37MHz (500kW)
 - Some control instabilities observed during campaigns
 - \rightarrow Test of **polychromatic operation** (Power upper and lower halves of ILA at f₀±250kHz)
 - \bigcirc Decoupling of control \rightarrow **no control instability issues**
 - \bigcirc V_{max} will limit operation (Large cross-talk : $|V_{C,f1}| \sim |V_{C,f2}| \rightarrow |V_{C}| \sim 2 |V_{C,f1}|$)
 - ightarrow lower power than monochromatic full array operation

The ILA : S-Matrix Arc Detection



• Low Z_T section not protected by VSWR against arcs \rightarrow **S-Matrix Arc Detection (SMAD)**

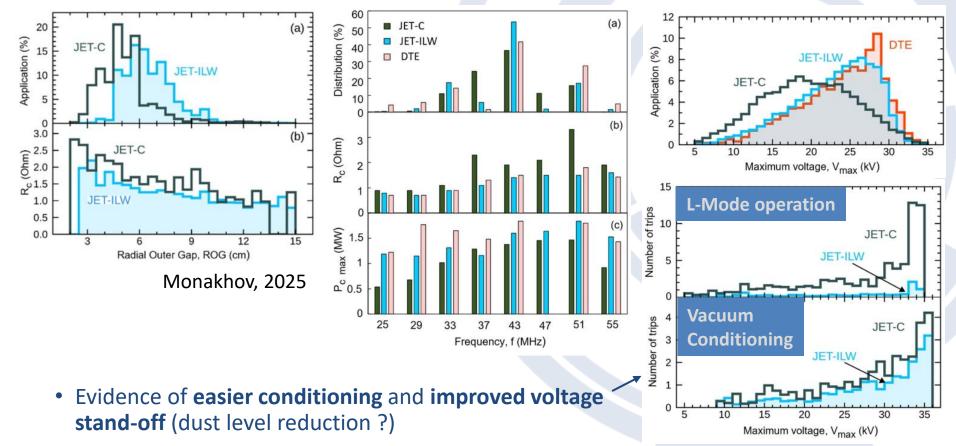


RF consistency check of the section of interest using:

- RF model of the section
- Calibrated RF signals around the section
- SMAD error calculation by FPGA every **2**µs

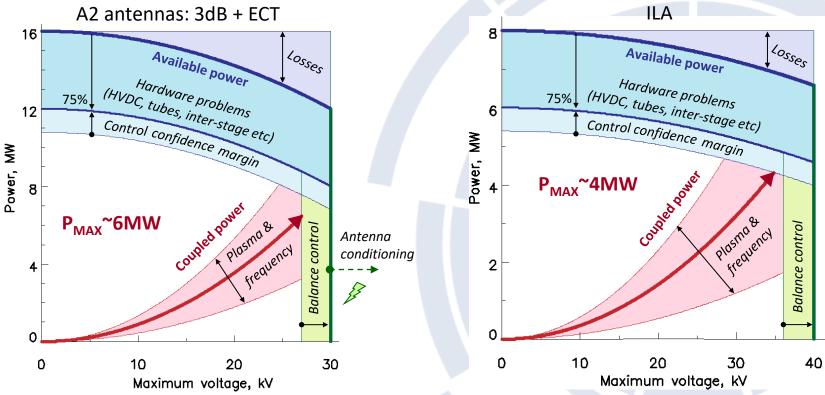
Change from JET-C to JET-ILW (Be/W) metallic wall

- 2009/11: installation of the Be wall and W divertor : modified recycling and far-SOL conditions and enhanced wall protection requirements
- Increasingly difficult matching conditions: ROG \uparrow , $R_c \downarrow$ and stronger ELMs ($\delta R_c \uparrow$)
- More operation at band edges in DTE
- System maintenance, diagnostics and optimisation allowed to keep performance up



Maximising Power and Reliability

Expected performance at 42MHz in H-mode plasmas

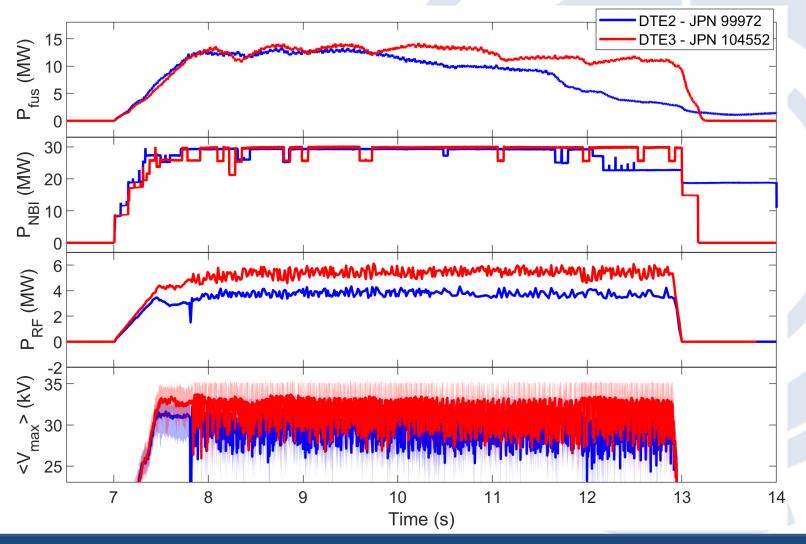


Courtesy I. Monakhov

- Importance of maintenance of the whole system (from HV PS to antenna), accurate diagnostics and high voltage conditioning
- Improve coupling conditions (e.g. ROG, gas puff optimisation)
- Strategy to improve balance control (RFLM upgrade)

) How to improve your record

- Antennas conditioned further for DTE3 : V_{max} set to 35kV (vs 33kV for DTE2)
- ~1.5MW increase in coupled RF power and more stationary conditions !



Some key ingredients for success

- Design phase :
 - Go for a flexible and versatile system for key physics (see talk by M. Mantsinen)
 - Take DT operation and remote handling on board from start of design
 - Test extensively all components and antenna assemblies before installation
 - Avoid movable/critical parts inside the torus vacuum
 - Minimise the RF-induced impurity release
 - Develop and simulate the control (including cross-talk) and the arc detection systems
 - Build the system to be able to quickly identify and safely isolate any fault
 - Accessibility for maintenance and repairs
 - Take some safety margin (nominal installed power)

• Operation phase :

- Plan for accurate RF measurements and extensive **calibration** of all measurement points
- Have a proper maintenance and test schedule of the whole system (amplifiers, HVDC, TL...)
- Allow for amplifier tests and optimisation during shutdowns (HVDC not available on JET during shutdowns)
- Condition as much as possible (even during breaks in ops pulses if possible)
- Coupling is the most important parameter for system performance → improve coupling by all possible means (design, gas puff, plasma conditions...)

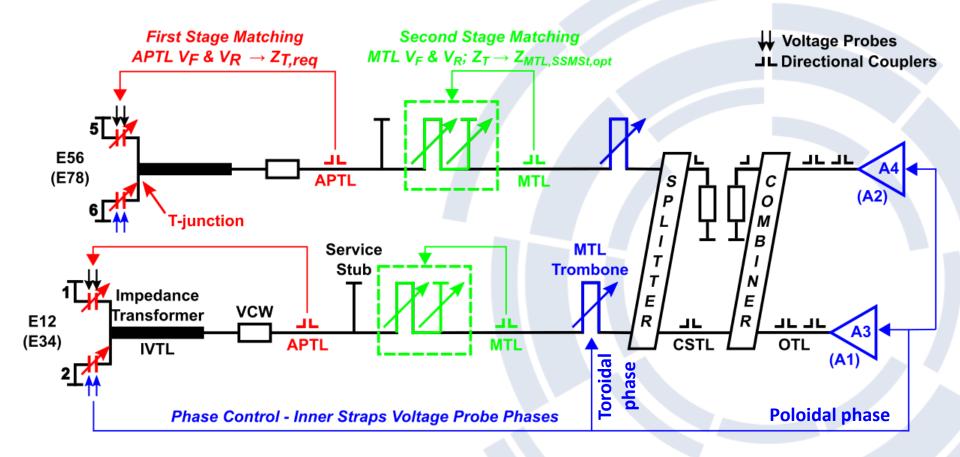
Nothing could be done without them !

Importance of team work towards a common goal !



Thank you for your attention





Full array: 12 feedback loops controlling 22 actuators Half array: 5 feedback loops controlling 10 actuators

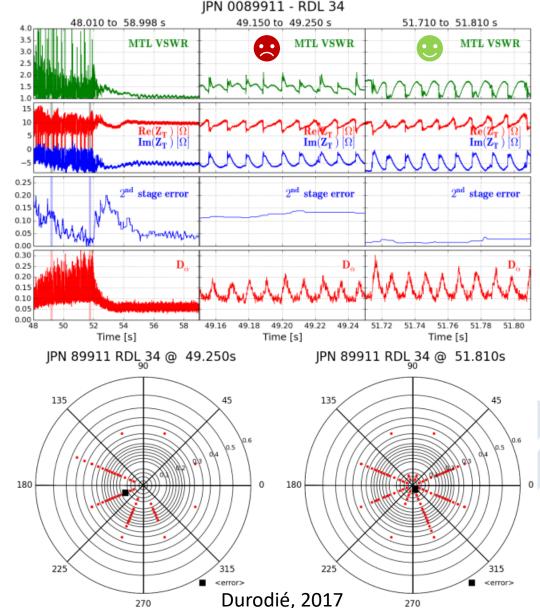


The ILA : Second Stage Offset Matching

Asymmetric RDL straps

 (antenna geometry) restricts
 the load resilience
 → need to offset match in
 presence of ELMs to improve
 ELM tolerance

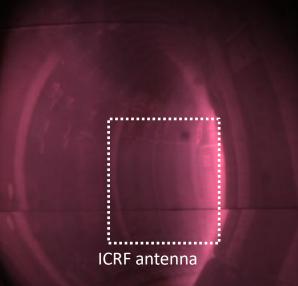
- Γ_{MTL} estimated on fast enough time scale to resolve ELM load variations (2µs) and stored in polar map bins (8 phase + 15-20 amplitude bins) during a chosen tracking time
- Γ_{MTL} averaged on slow time scale (2000 points/pulse) → error signals to drive SSM components (move, direction, slow/fast)



ICWC and RF-assisted start-up

- Dedicated protection set-up for ICWC and RFassisted breakdown experiments
 - Frequency < 33MHz to prevent VTL voltage node (multipactoring)
 - ✓ Install more restrictive **3:1 VSWR cards**
 - \checkmark Trip counters set to **10 trips** maximum (\leftrightarrow 25-100 trips)
 - ✓ VTL trip soft limit set to **5** 10⁻⁵ mbar (\leftrightarrow 1x10-4 mbar)
 - ✓ PEWS interlocks overridden for zero kA
 - ✓ Set Local MTL limits to 20kV (↔ 30kV)
 - ✓ Fast data acquisition enabled
 - ✓ Check trips after each pulse
- Mostly monopole operation
- RF power generally applied before gas injection to avoid arcing in the antenna box
- Requires to establish vacuum reference pulses

ICWC in JET



250kW ICRF 29MHz

Wauters, 2021

DT Operation

- **D-T** operation **planned from start** (remote handling, double vacuum window, etc)
- Containment of Tritium (air flow in transmission lines handled by Active Handling Gas System, reduce extent of 3-bar pressurized transmission line air leaks, monitoring of the DCF interspace, check isolation valves...)
- 'Expensive' pulses → need careful preparation, no spare pulses
 - Improve system reliability, availability and repairability
 - Conditioning as much as possible prior to the experiment
 - Test load pulses to identify issues and know the plant limit
 - Target is to deliver full power on first pulse
 - Reference pulses for every scenario in same coupling conditions
 - RFLM upgrade to equalize voltages taking the plant limits into account

