

Experimental Evidence of Helicon Wave Heating and Current Drive in DIII-D

Jeff Lestz,[†] B.G. Van Compernelle,
R.I. Pinsker, S.X. Tang, A. Dupuy,
A.M. Garofalo, L. McAllister,
C.P. Moeller, M. Porkolab, M.P. Ross,
and the DIII-D Helicon Team

General Atomics

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[†]Contact: lestzj@fusion.gat.com



Motivation and Main Results

- **Motivation:** fast waves in the lower hybrid frequency range (helicon) can provide off-axis current drive needed for non-inductive, steady-state scenarios
- **Goal:** experimentally measure the electron temperature and current profile response to helicon injection in order to assess absorption and current drive
 - Necessary to validate models before using to design future scenarios
- **Main results:**
 - Core electron heating directly observed in both L and H mode plasmas
 - Strong and reproducible experimental evidence of helicon current drive in DIII-D
 - Experimental estimates of absorption and current drive are consistent with GENRAY

Outline

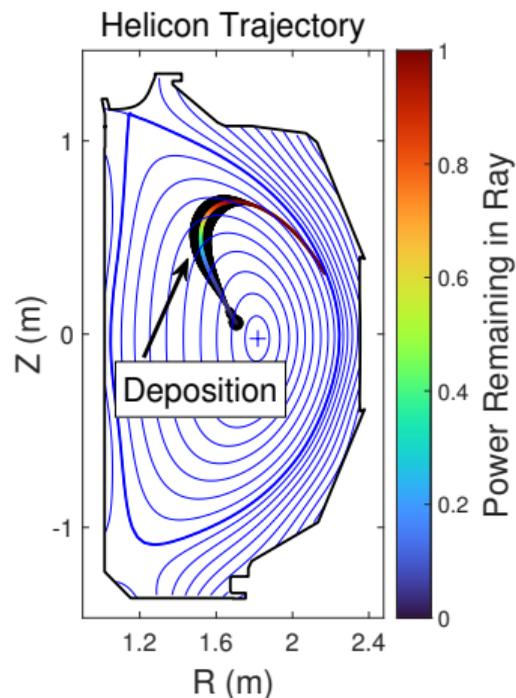
- Introduction
- Evidence of Electron Heating
- Evidence of Current Drive

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Helicon Wave Can Provide Off-Axis Current Drive

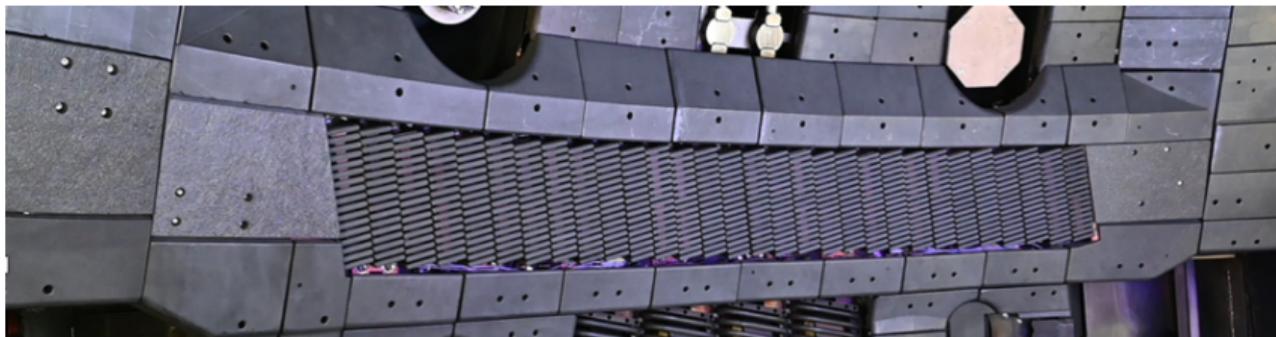
- **Helicon**: fast wave in the lower hybrid range of frequencies ($f_{ci} \ll f \ll f_{ce}$)
 - DIII-D traveling wave antenna: 476 MHz, $n_{\parallel} = 3$
- Absorption via Landau damping, scales with β_e
 - Current drive efficiency scales with T_e/n_e and $\omega/k_{\parallel} v_{th,e}$
- Off-axis absorption can drive non-inductive current necessary to help sustain advanced scenarios¹
- Physics goal: demonstrate helicon heating and current drive in DIII-D plasmas and validate against modeling



¹R. Prater *et al.* Nucl. Fusion **54**, 083024 (2014)

MW-level DIII-D Helicon System Has Been Used for Physics Experiments

- 30 module comb-line traveling wave antenna, 1.5 m in total length
 - Robust load resilience to ELMs consistently observed
- Designed to inject power from either end to drive current in either toroidal direction
- 1.2 MW maximum klystron power, reliably operated around 700 – 800 kW
 - Routinely coupled 300 – 400 kW to plasma for up to 2 s
- No influx of impurities was measured during helicon injection

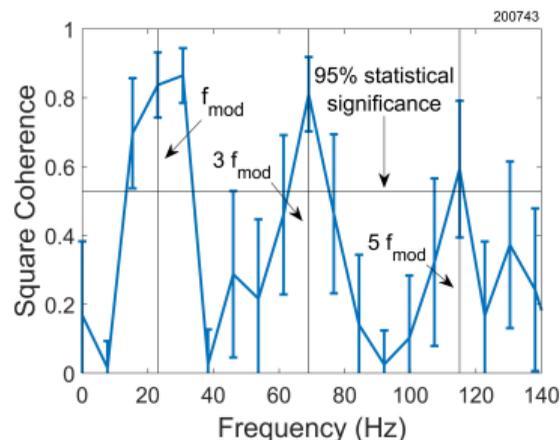
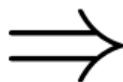
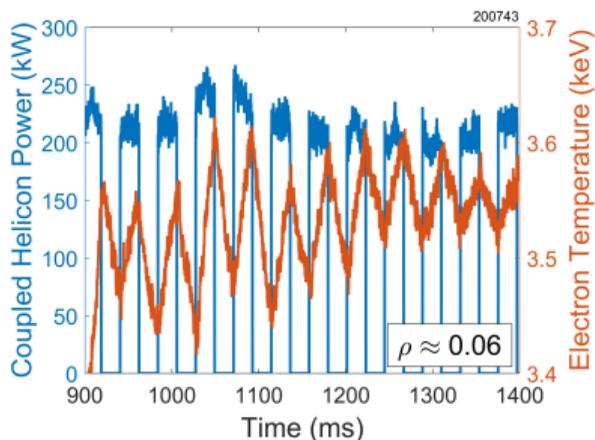


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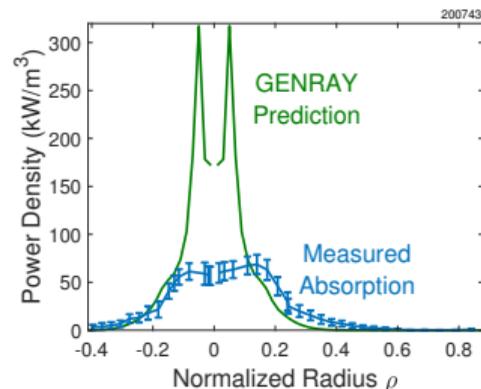
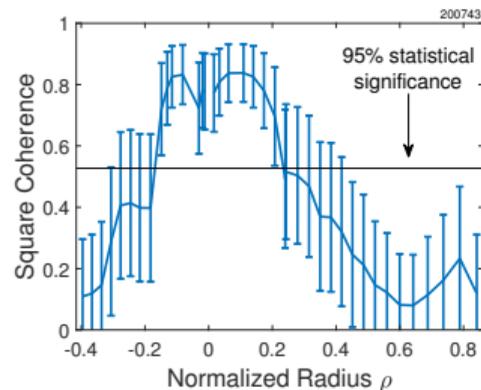
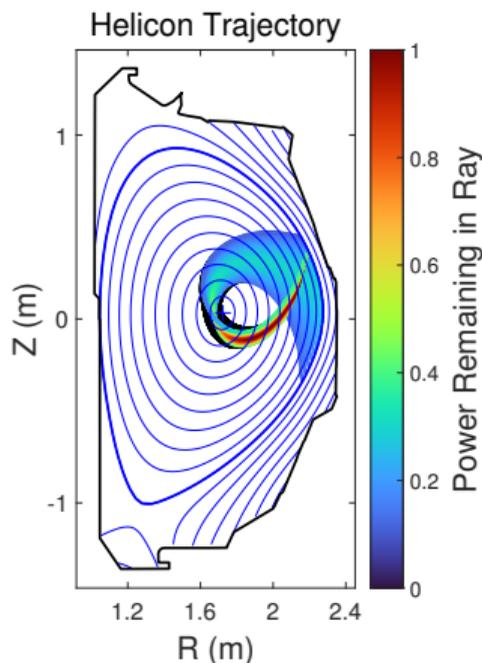
Definitive Observation of Electron Heating Due to Helicon

- Helicon power modulated at fixed frequency to isolate coherent electron heating
- **Square coherence** measures synchronization of T_e with helicon power over time
 - Clear peaks at $f_{\text{mod}} = 23$ Hz, $3f_{\text{mod}} = 69$ Hz, and $5f_{\text{mod}} = 115$ Hz on core ECE
 - Square coherence far exceeds 95% statistical significance level



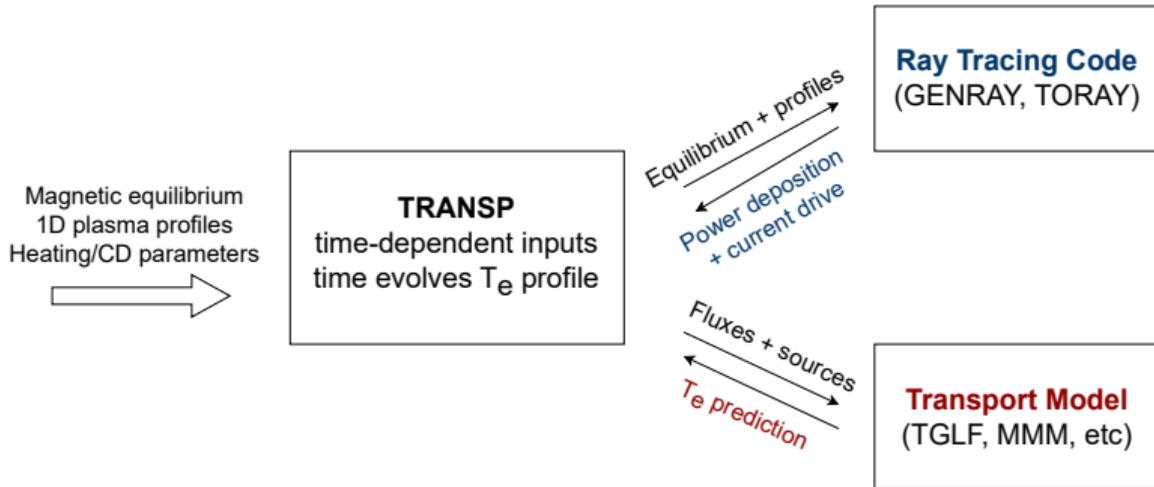
Measured δT_e Profiles Show Core Heating

- GENRAY predicts core deposition with $\approx 40\%$ first pass absorption in L mode
 - 210 kW power measured leaving the antenna
- Square coherence and δT_e peak in core, agreeing with ray tracing predictions
- Preliminary estimate of 90 ± 20 kW of heating
 - Need transport modeling to improve accuracy



Time-Dependent Integrated Modeling With TRANSP

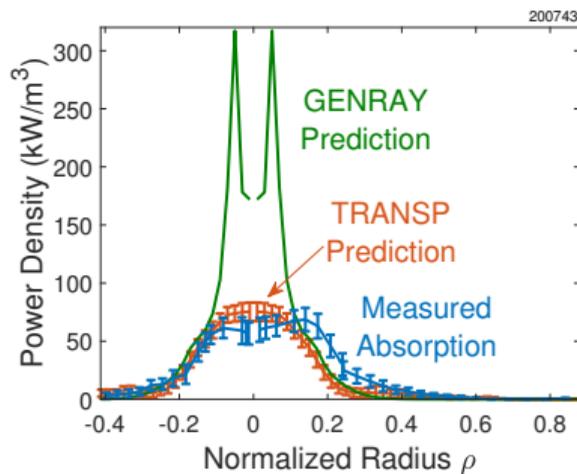
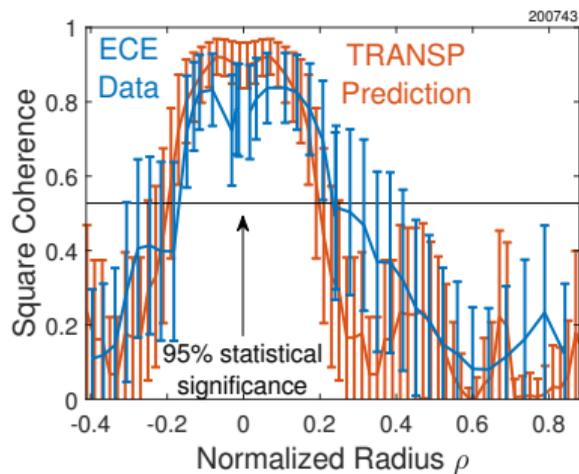
- TRANSP loops over the **GENRAY** ray tracing code and **MMM²** turbulent transport model in order to predict the **helicon deposition** and **δT_e response** over time
- Comparing predicted δT_e to ECE measurements aids experimental interpretation



²T. Rafiq *et al.* Plasma **6**, 435 (2023)

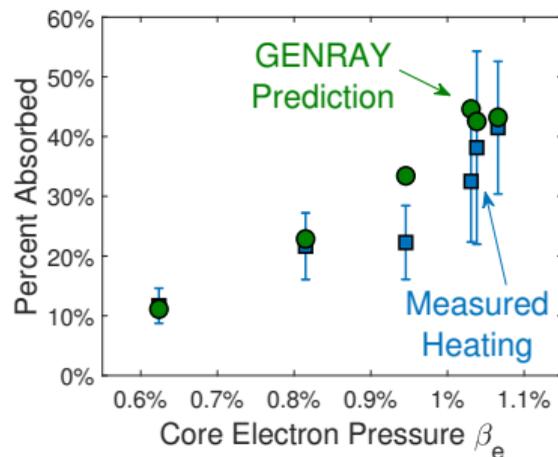
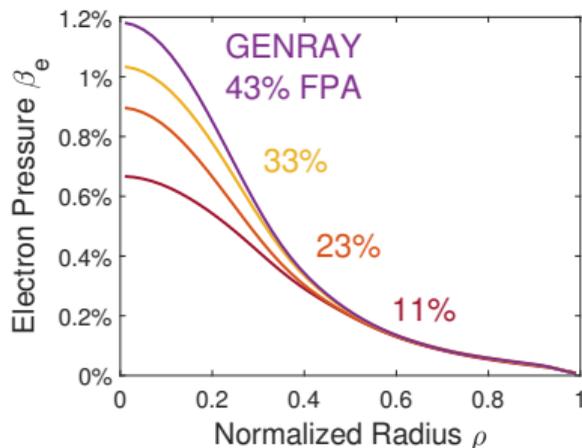
δT_e Measurements Consistent With Time-Dependent TRANSP Simulations

- Coherence is slightly higher in TRANSP, with very similar peaked profile
- δT_e response predicted by TRANSP reproduces broad measured deposition
 - Explains difference between GENRAY vs ECE measurements via transport effects



Observed Power Absorption Scales With Predicted First Pass Absorption

- Core β_e scanned across shots with varying ECH to scan predicted absorption
- Observed electron heating tracks first pass absorption predicted by GENRAY
 - Measurements shown without transport corrections
- Clear heating also observed in H mode, absorption more difficult to quantify

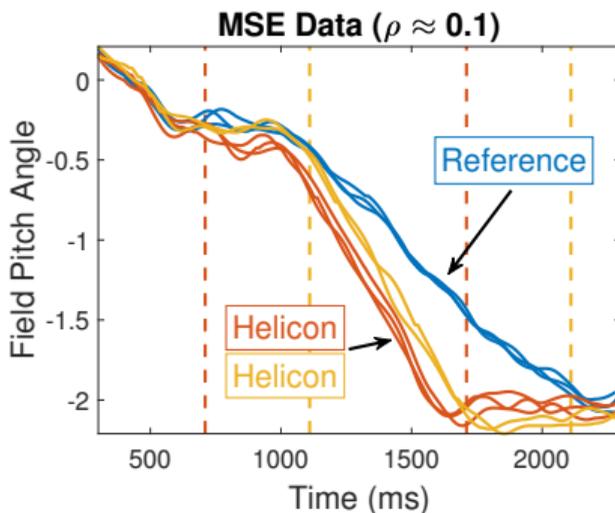
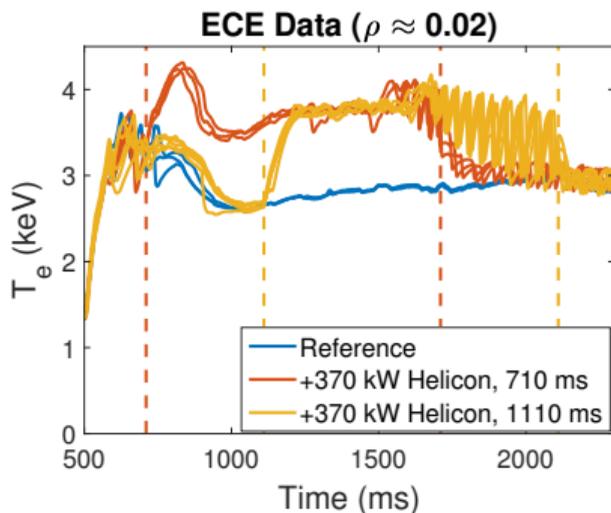


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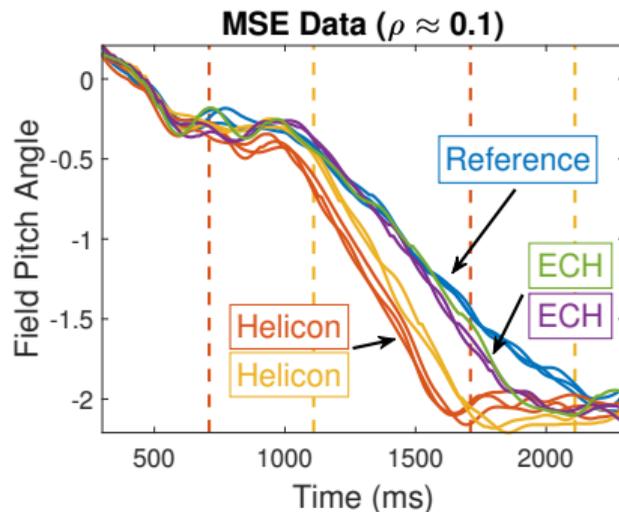
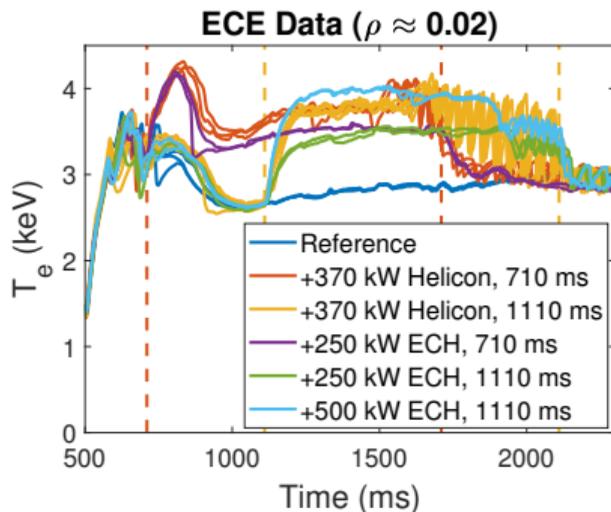
Helicon Injection Changes MSE Evolution

- Only one side of antenna available, unable to compare co- vs cntr-current drive
 - Use ECH comparison shots to separate heating vs current drive effects instead
 - Inject helicon power continuously to drive co- I_p current, without any modulation
- MSE drops faster in shots with helicon than with comparable EC heating



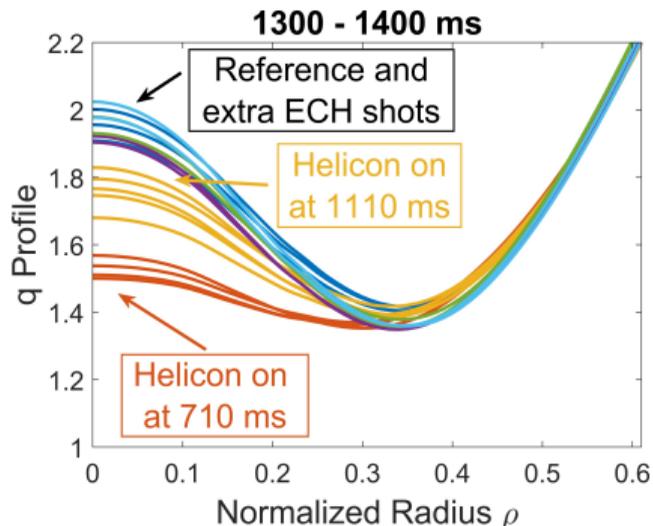
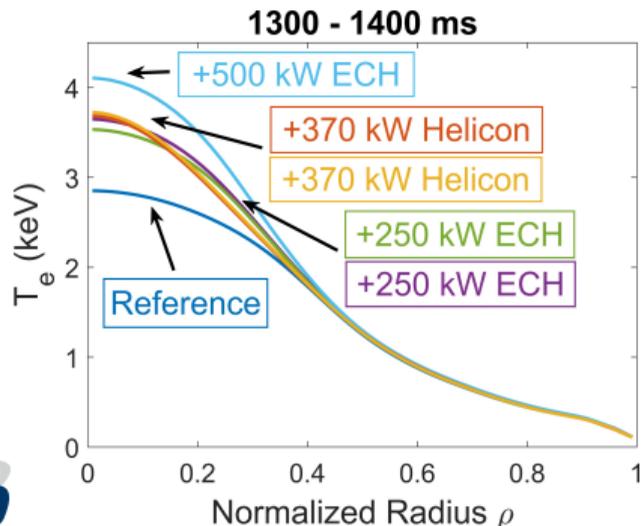
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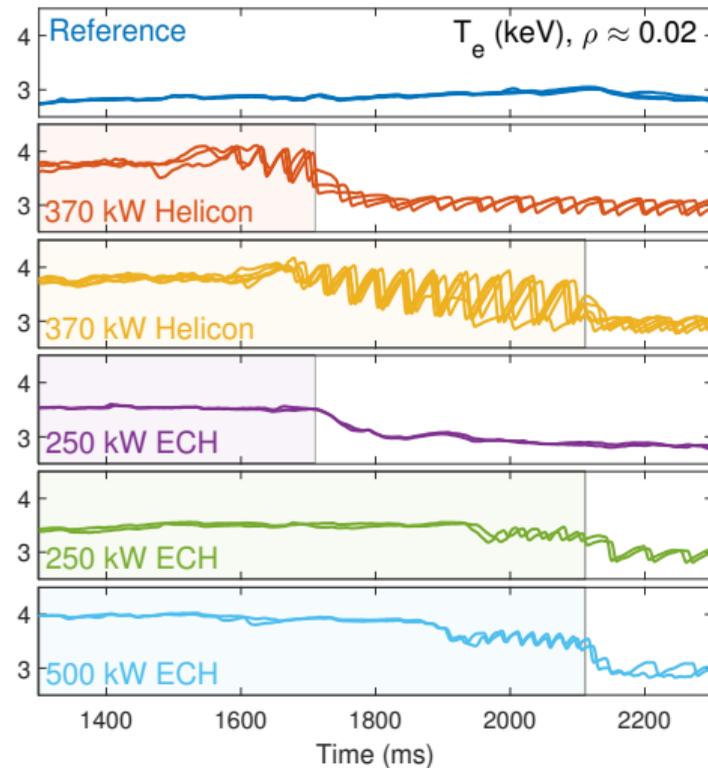
T_e and q Profiles Indicate Helicon Heating and Current Drive

- 370 kW coupled helicon power increases T_e by ~ 1 keV relative to the reference
 - Similar T_e profile to 250 kW of ECH deposited at $\rho = 0.1$
 - Somewhat larger than the $\approx 47\%$ FPA predicted by GENRAY (175 kW)
- MSE-constrained reconstruction shows q profile flattening due to helicon current



Sawteeth Start Earlier in Helicon Shots

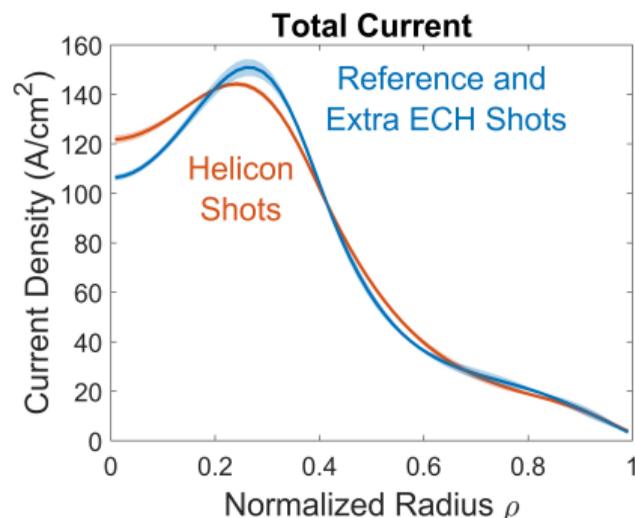
- Sawteeth onset when $q = 1$, providing independent measure of current evolution
- Helicon shots begin sawtoothing long before shots with comparable amount of ECH
- Interpretation: co- I_p helicon current drives q down faster, triggering sawteeth earlier
 - Consistent with MSE and EFIT reconstruction



Helicon Current Determined by Comparing Non-Inductive Current With Reference Shots

- Changes in J_{\parallel} profiles are insufficient to quantify helicon current drive
 - $\int \Delta J_{\parallel} dA = 0$ since I_p is unchanged
- Determine change in non-inductive current by subtracting off Ohmic current and “known” non-inductive current sources³
- Calculate ΔJ_{NI} between shots with and without helicon to mitigate systematic uncertainties

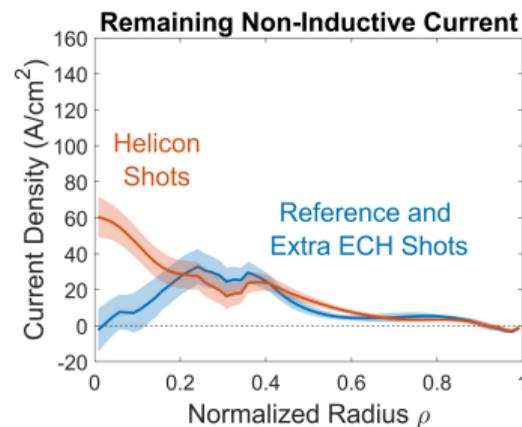
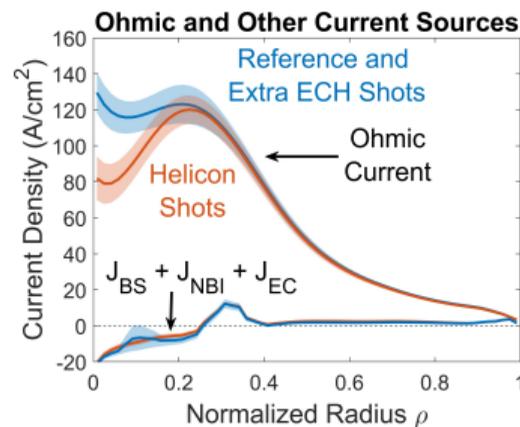
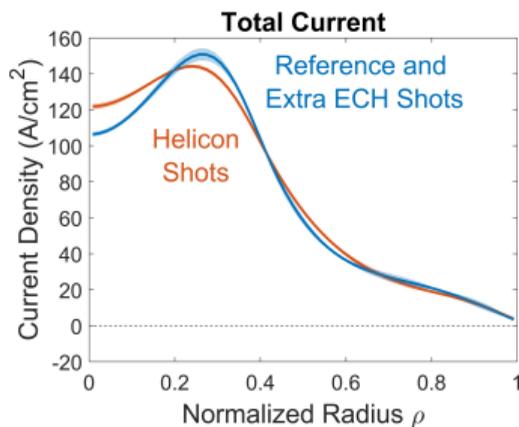
$$J_H = \Delta J_{\parallel} - \Delta J_{Ohm} - \Delta (J_{BS} + J_{NB} + J_{EC})$$



- Average over repeat shots **with helicon** vs **no helicon** to reduce uncertainty

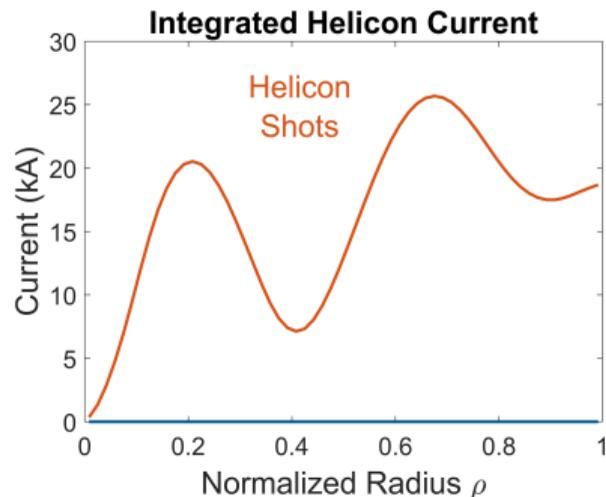
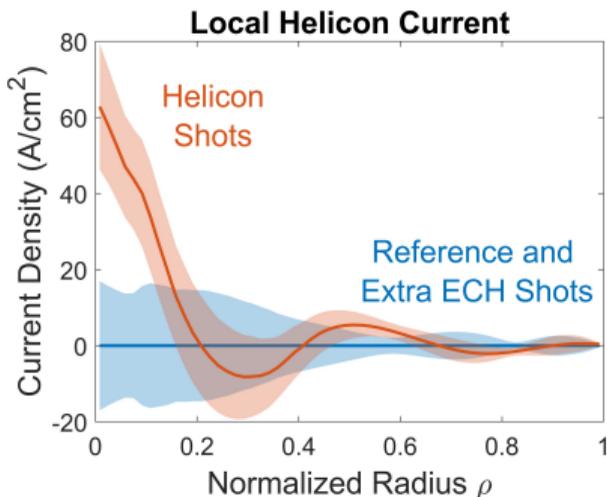
Subtract Ohmic and Other Current Sources To Get Remaining Non-Inductive Current

- E_{\parallel} calculated from MSE-constrained equilibrium reconstruction, neoclassical conductivity from kinetic profile data: $J_{Ohm} = \sigma E_{\parallel} \propto \frac{T_e^{3/2}}{Z_{eff}} \frac{\partial \psi}{\partial t}$
- Other non-inductive current sources calculated by standard models in TRANSP
- Systematic errors lead to unexplained current near $\rho \approx 0.3$ in reference shots



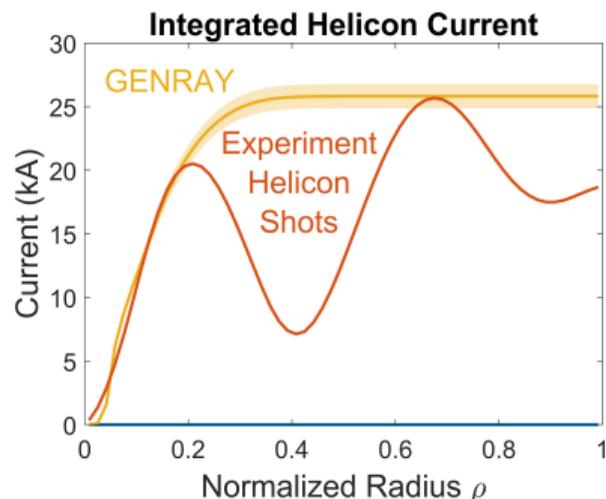
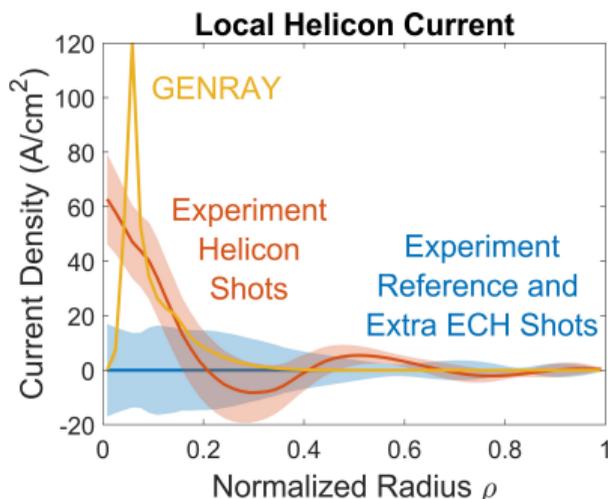
Peaked Helicon Current Profile Within $\rho < 0.2$

- Helicon current profile consistent with measured heating profile in similar L modes
 - Helicon current density far exceeds the spread among reference and ECH shots
- Preliminary estimate of ≈ 20 kA integrated current, at least 10 kA uncertainty
 - Note: shaded regions show average across shots – uncertainties not yet propagated



Measured Helicon Current Drive in Reasonable Agreement With Modeling

- GENRAY predicted current density profile is more peaked than experiment
 - Sensitive to details of ray trajectory due to rapidly decreasing volume near axis
- Integrated current profile in fair agreement, finding similar amount of current enclosed in $\rho < 0.2$ – oscillations likely an artifact of analysis
 - GENRAY prediction for first pass absorption: 150 kA/MW of absorbed power



Main Results and Ongoing Analysis

Main Results

- Core electron heating observed in both L and H mode DIII-D plasmas
 - Time-dependent integrated modeling in qualitative agreement with measurements
- Strong evidence for first observation of helicon current drive on any device
 - Observed changes in L mode current profile can not be explained by heating alone

Ongoing Analysis

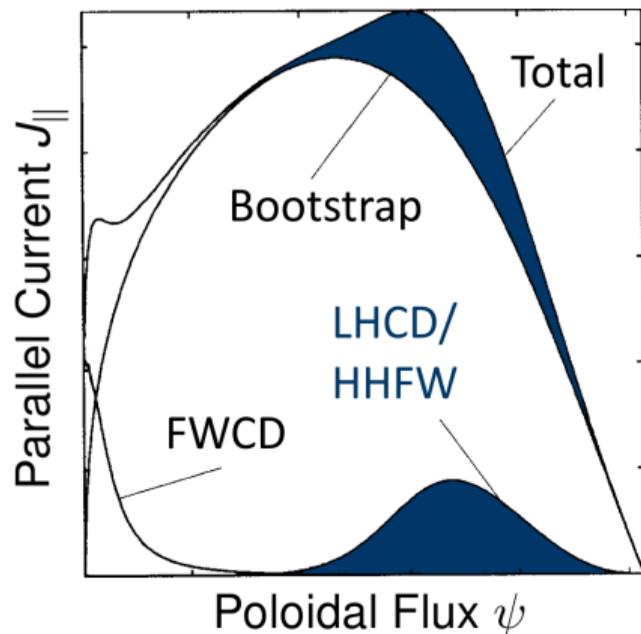
- Calculate H mode power absorption from modulated T_e response
- Refine L mode current drive analysis and quantify experimental efficiency

Work supported by US DOE under DE-FC02-04ER54698. ASIPP and KFE contributed to the manufacturing and procurement of the helicon hardware.

Backup Slides

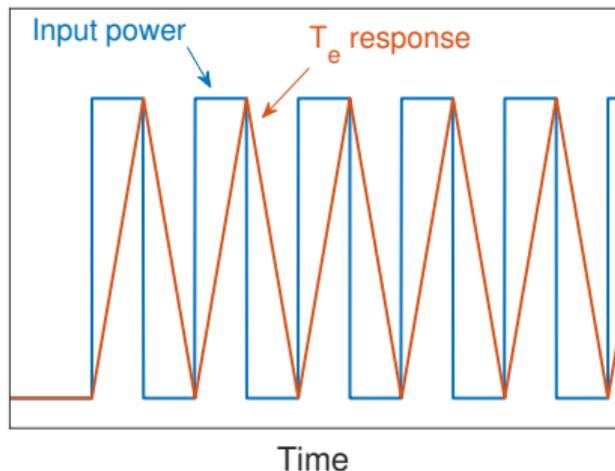
Mid-Radius Current Drive Is Needed for Reactor Scenarios

- Steady state scenarios require efficient, non-inductive off-axis current drive⁴
- DIII-D has been studying methods for off-axis radio frequency current drive
 - Top launch ECCD (since 2019)
 - **Helicon current drive** (2021)
 - HFS lower hybrid current drive (2024)
- Whereas ECCD is localized near $\omega \approx n\omega_{ce}$, helicon and lower hybrid current drive occur due to Landau damping, when $\omega/k_{\parallel} \approx v_{\parallel,e}$
 - Off-axis absorption for sufficiently high β_e



⁴S.C. Jardin *et al.* Fusion Eng. Des. **38**, 27 (1997)

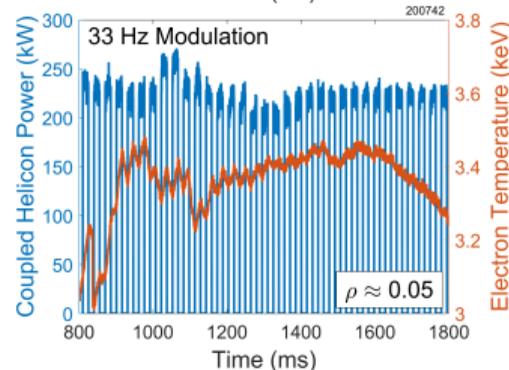
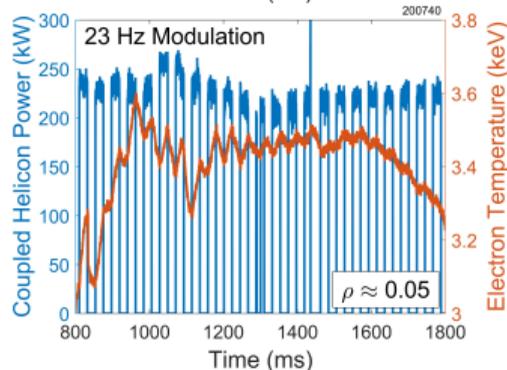
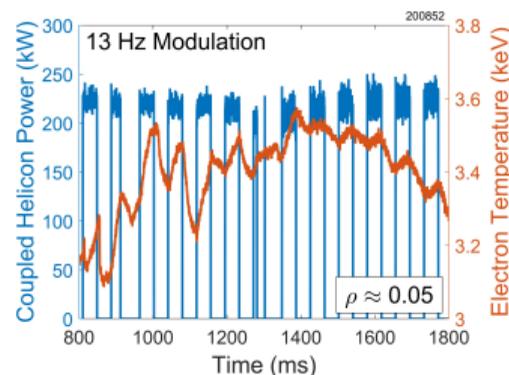
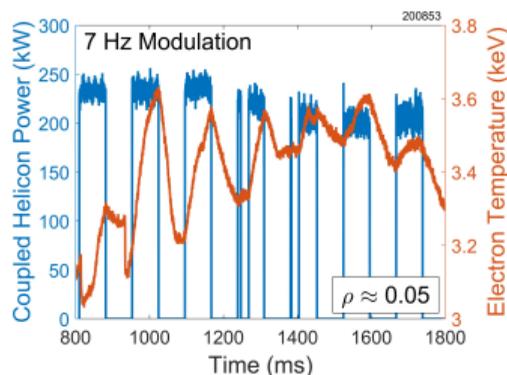
Investigating Helicon Absorption With Power Modulation



- **Direct heating:** modulated helicon power → modulated δT_e response at same frequency, lagging by 90° (ideally)
 - Transport effects distort this picture when modulation is not sufficiently fast
 - However, faster modulation leads to smaller amplitude fluctuations
- Use cross-spectral analysis techniques with Fourier transforms to average over many cycles
- Compare to same analysis with modulated ECH, assumed to be well-understood

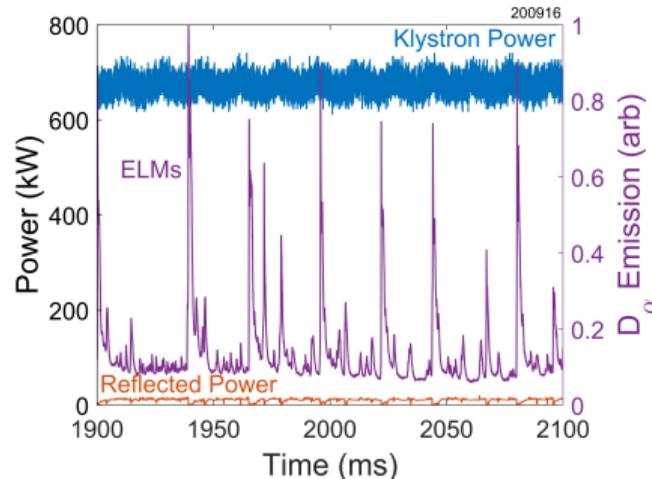
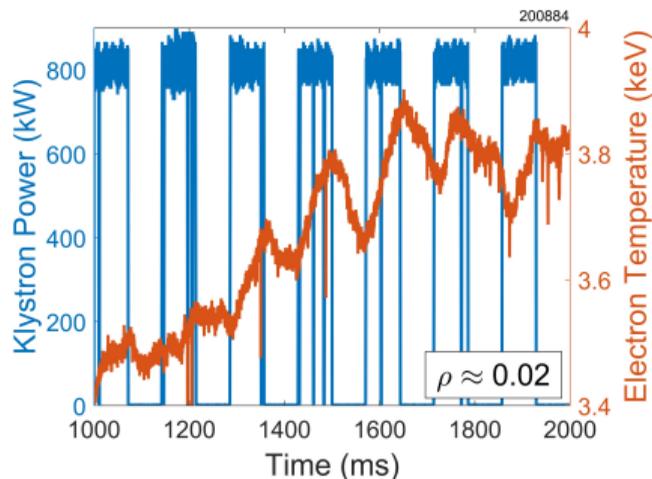
Electron Temperature Responds to Modulation Frequency

- δT_e amplitude increases with longer helicon pulse time
- Frequency scan rules out coincidental δT_e oscillations



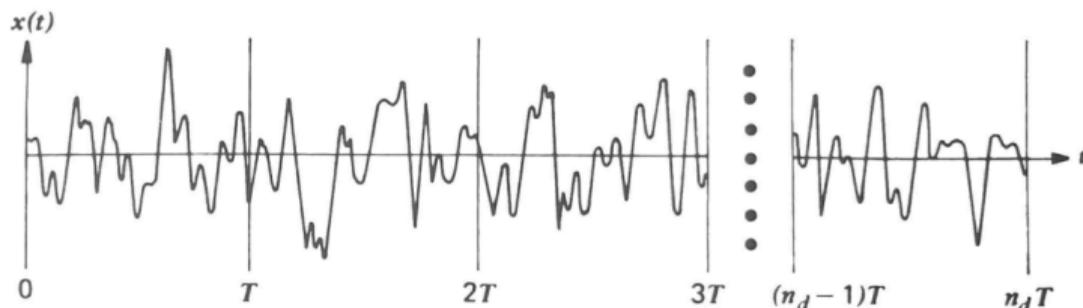
Clear Electron Heating Also Observed in ELMy H mode

- GENRAY predicts over 90% first pass absorption in these H mode plasmas
 - Absorption still predicted near axis – higher density plasmas push absorption off axis
- Robust load resilience – no substantial rise in reflected power during ELMs



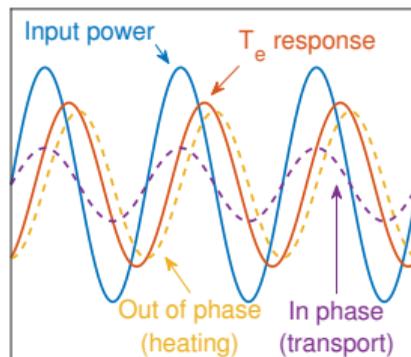
Ensemble Averaging Is Necessary to Quantify Coherence

- Let $P(t)$ be the modulated input power (helicon or ECH) and $T_e(t)$ be the output
 - Then $\hat{P}(f) = F[P(t)]$ and $\hat{T}_e(f) = F[T_e(t)]$ are their Fourier images
- **Square coherence:** $\gamma^2 = \frac{|\langle \hat{T}_e^* \hat{P} \rangle|^2}{\langle \hat{P}^* \hat{P} \rangle \langle \hat{T}_e^* \hat{T}_e \rangle} \approx 1$ only when $\phi_P(t) \approx \phi_{T_e}(t)$
 - $\langle \dots \rangle$ denotes ensemble averaging, by chopping the time series into n_s segments
 - Significance test: $\gamma^2 > 1 - \alpha^{\frac{1}{n_s-1}}$ rejects the null hypothesis with uncertainty α
- Dividing into more segments improves statistics, but reduces frequency resolution

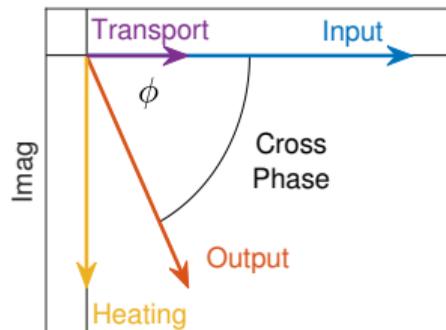


Cross Phase Characterizes Heating vs Transport Response

- Measured T_e response includes both heating and transport effects
- Out of phase component results from heating
$$\text{Im}[\delta T_e(f)] = \frac{\text{Im}[\langle \hat{P}^* \hat{T}_e \rangle]}{\langle \hat{P}^* \hat{P} \rangle} \hat{P}$$
- In phase component $\text{Re}[\delta T_e(f)]$ occurs due to transport or direct diagnostic pickup
- **Cross phase** $\tan \phi(f) = \frac{\text{Im}[\delta T_e]}{\text{Re}[\delta T_e]}$ quantifies this relationship ($\phi \rightarrow -90^\circ$ for zero transport)



Time



Real

Two Quantities for Estimating δT_e Response

- Defining the transfer function \hat{H} via $\hat{T}_e(f) = \hat{H}(f)\hat{P}(f) \Rightarrow \hat{H} = \langle \hat{P}^* \hat{T}_e \rangle / \langle \hat{P}^* \hat{P} \rangle$,
1. **Coherent output spectrum:** $\delta T_e^2(f) = |\hat{H}|^2 \langle \hat{P}^* \hat{P} \rangle = \frac{|\langle \hat{P}^* \hat{T}_e \rangle|^2}{\langle \hat{P}^* \hat{P} \rangle}$
 - Weighting by coherence is built in (equivalently, $|\hat{H}|^2 \langle \hat{P}^* \hat{P} \rangle = \gamma^2 \langle \hat{T}_e^* \hat{T}_e \rangle$)
 - Complementary quantity: incoherent spectrum: $(1 - \gamma^2) \langle \hat{T}_e^* \hat{T}_e \rangle$
 - **Drawback:** no information on phase between \hat{P} and \hat{T}_e
 2. **Out of phase response:** $\delta T_e(f) = \text{Im}[\hat{H}]|\hat{P}| = \frac{\text{Im}[\langle \hat{P}^* \hat{T}_e \rangle]}{\langle \hat{P}^* \hat{P} \rangle} \hat{P}$
 - Cross phase: $\tan \phi(f) = \frac{\text{Im}[\delta T_e]}{\text{Re}[\delta T_e]}$ characterizes heating vs transport response
 - Does not include coherence directly, very noisy away from modulation frequency
 - **Drawback:** overstates Δf resolution due to interpolating $\hat{H}(f)$ onto grid of $\hat{P}(f)$
- Relative error formulas exist for both quantities⁵ (errorbars in plots)

⁵J.S. Bendat *et al.* Journal of Sound and Vibration **59**, 405 (1978)

Electron Transport Effects Complicate Extracting Absorbed Power From δT_e Measurements

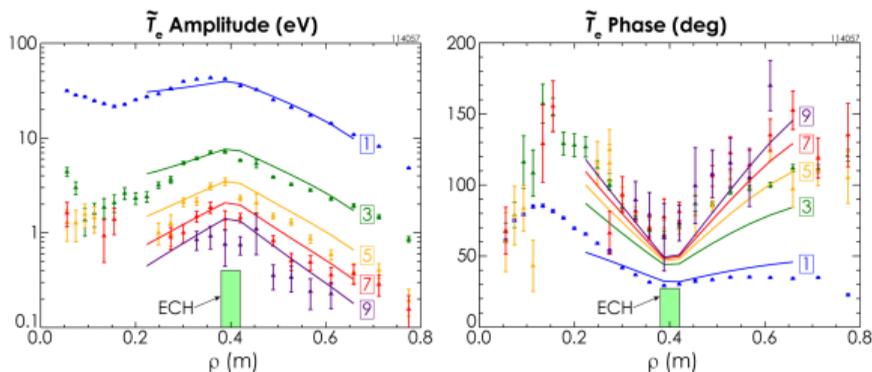
- Electron energy conservation relates source profile $\hat{S}(f, \rho)$ to $\hat{T}_e(f, \rho)$ via transport

$$-D\nabla^2 \hat{T}_e(f, \rho) + V\nabla \hat{T}_e(f, \rho) + \left(\frac{1}{\tau} + i\frac{3}{2}\omega \right) \hat{T}_e(f, \rho) = \frac{\hat{S}(f, \rho)}{n_e}$$

- Diffusion and convection can smear out the fluctuations and alter the cross phase

- Rigorous approach: fit multiple harmonics of \hat{T}_e data to determine values of transport coefficients⁶

- Present helicon data does not have high enough signal to noise to fit multiple harmonics



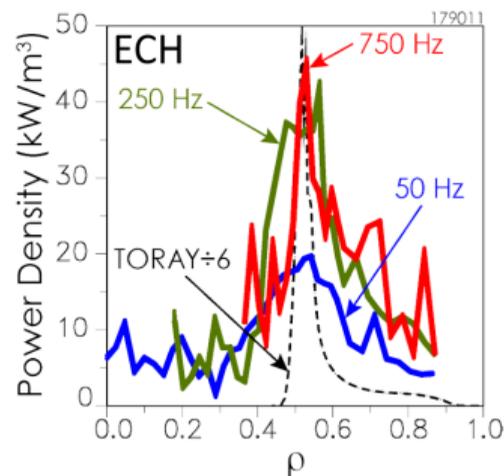
⁶C.C. Petty *et al.* 23rd RFPPC, Hefei, China (2019)

Zero Transport Approximation Yields an Oversimplified Estimation of Power Deposition

- If modulation is much faster than transport, can assume direct heating response
- Then summing over all frequencies in a square wave of height S_{\max} gives the total absorption as a function of δT_e measured only at the modulation frequency f_0

$$P_{\text{abs}} = \int S_{\max}(\rho) dV \approx \frac{3\pi}{4} \omega_0 \int n_e(\rho) \text{Im}[\hat{T}_e(f_0, \rho)] dV$$

- ECH modulation experiments indicate $f_0 = 23$ Hz is not within this zero transport regime⁷
- **Compromise:** adjust this approximation via calibrated ECH measurements and modeling

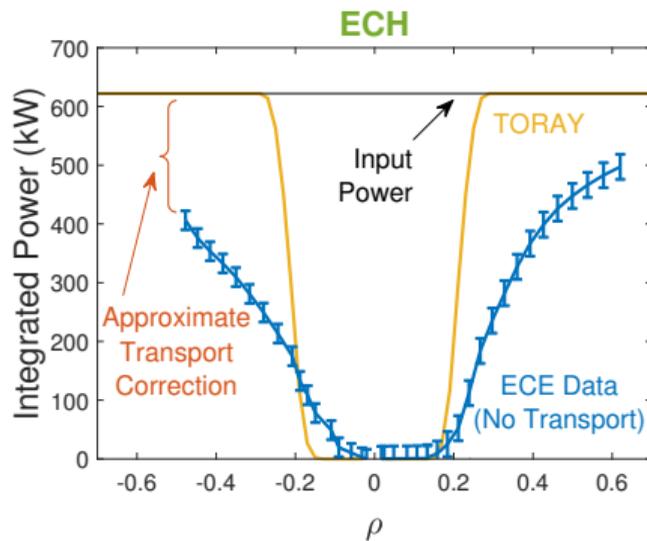


⁷C.C. Petty *et al.* 61st APS DPP, Fort Lauderdale, FL (2019)

ECH Experiments Used to Adjust for Transport in Helicon Experiments

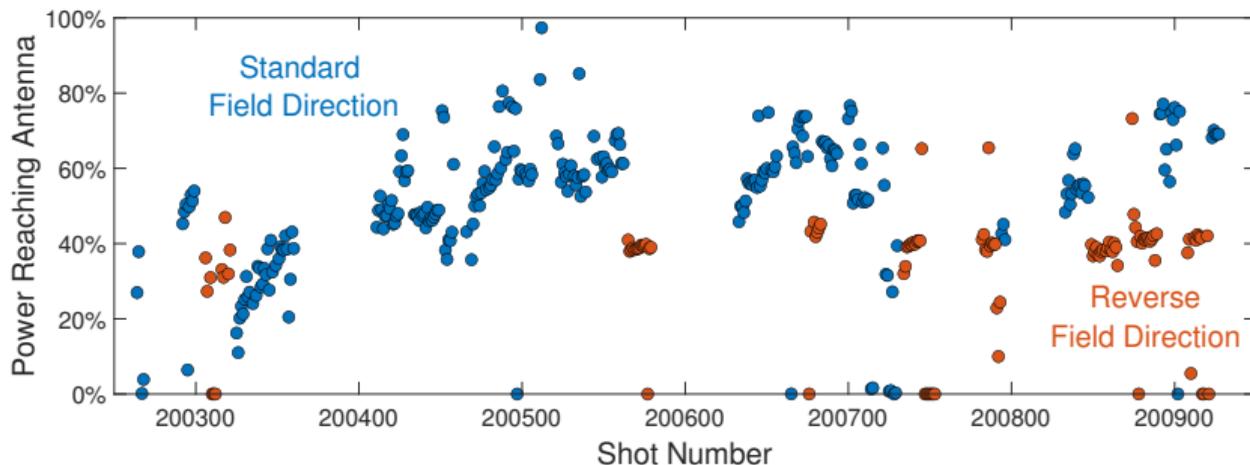
- Significant shortfall exists when calculating P_{abs} from δT_e data without transport for ECH modulation shot
- **Leap of faith:** assume the ECH transport correction is the same for helicon
 - Note: ECH deposition is much more narrow than helicon, localized at $\rho \approx 0.2$
 - Crude approximation, not a precise accounting of transport effects

$$P_{\text{abs}}^{\text{HK}} \approx P_{\text{meas}}^{\text{HK}}(\text{ECE}) \frac{P_{\text{abs}}^{\text{ECH}}(\text{TORAY})}{P_{\text{meas}}^{\text{ECH}}(\text{ECE})}$$



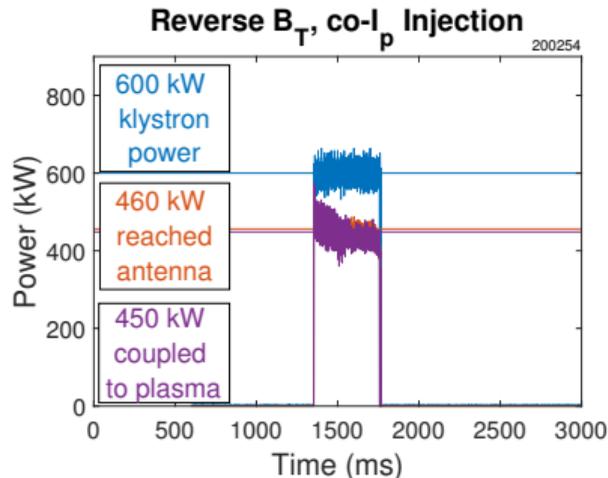
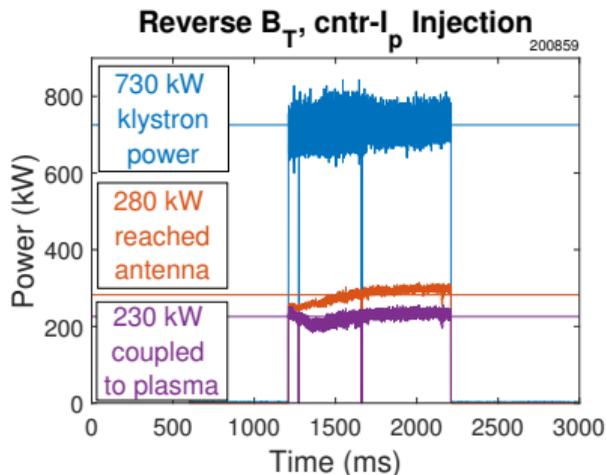
Vacuum Transmission Losses Improve With Conditioning

- Antenna designed for “reverse” B_T direction for advanced scenario experiments
 - Antenna conditioning is sensitive to direction of magnetic field
 - Majority of time available for conditioning was in “standard” B_T direction



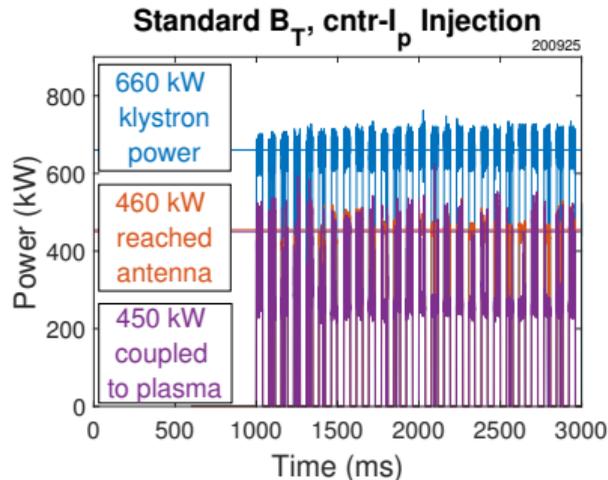
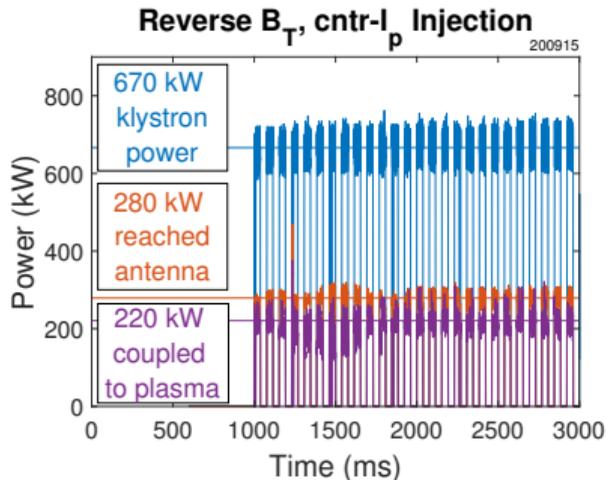
Vacuum Transmission Losses Depend on Which Side of Antenna is Fed Power

- Magnetic field and plasma current directions unchanged in two shots below
- Vacuum transmission losses were much higher when injecting in $\text{cntr-}I_p$ direction



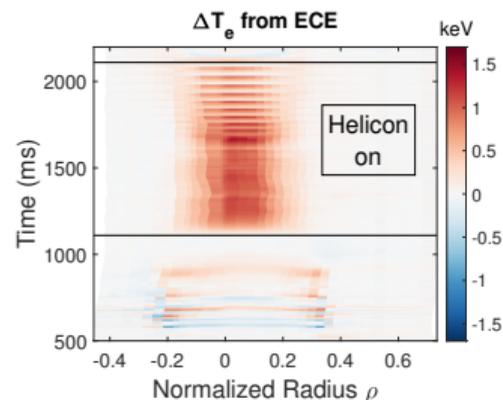
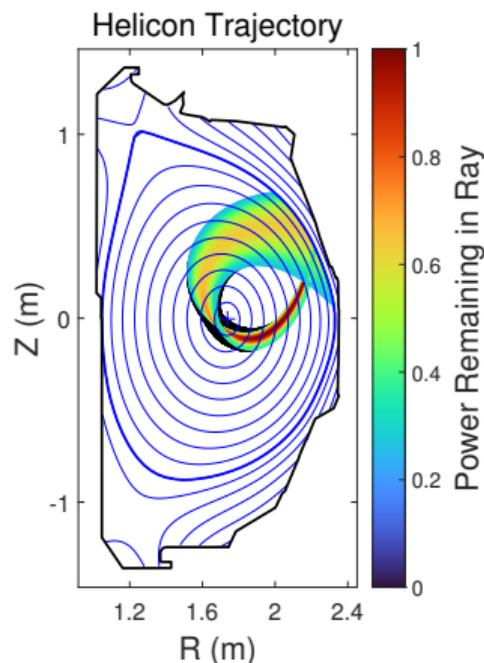
Vacuum Transmission Losses Depend on Field Direction

- Magnetic field direction flipped between two shots below
- Vacuum transmission losses were much higher in the reverse B_T direction



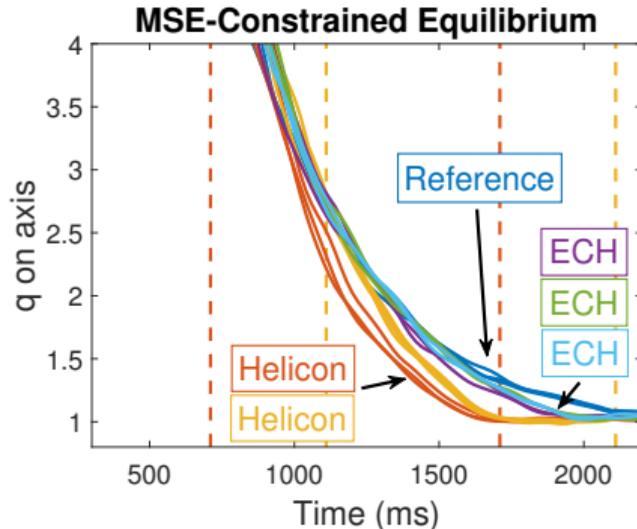
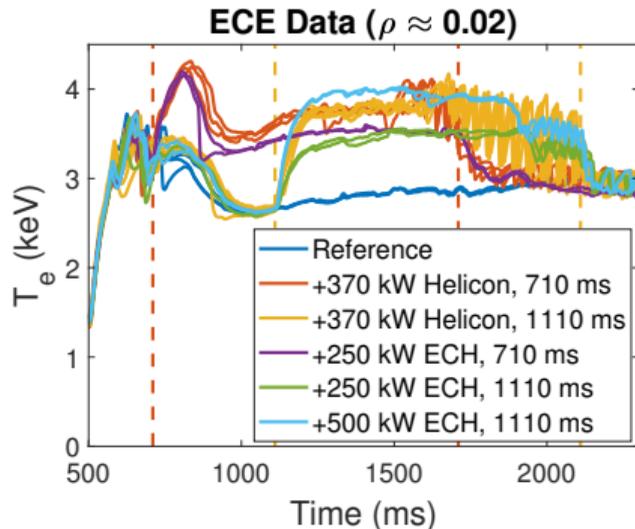
GENRAY Predicts Core Absorption in L Mode Plasma

- GENRAY predicts core deposition with $\approx 47\%$ first pass absorption in L mode
 - 370 kW power measured leaving the antenna
- GENRAY predicts ≈ 26 kA helicon current drive
- Unambiguous core heating measured by comparing T_e in shots with and without helicon

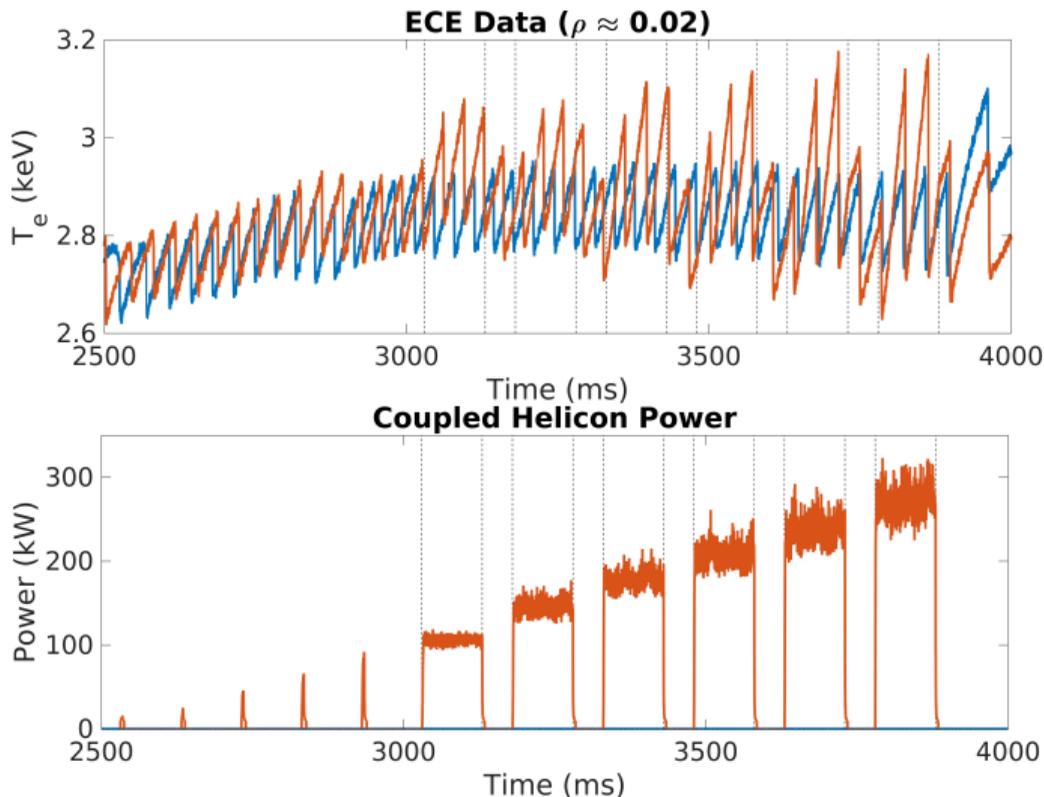


MSE-Constrained EFITs Show Drop in q On-Axis

- q drops faster on-axis in helicon shots than ECH references that had higher T_e
 - Changes in q can not be fully explained by heating – likely helicon current drive



Helicon Power Increases Sawtooth Amplitude



Direct Pickup Has Different Signature From Heating

- ECE channel 28 is polluted when helicon operates
- Signatures of direct pickup:
 - Rapid rise of T_e response
 - Very high coherence
 - Wrong cross phase
- Signal is in phase
- Other ECE channels do not have these dramatic features
 - Helps to rule out pickup

